

IntechOpen

## Fourier Transform Signal Processing and Physical Sciences

Edited by Salih Mohammed Salih





# FOURIER TRANSFORM -SIGNAL PROCESSING AND PHYSICAL SCIENCES

Edited by Salih Mohammed Salih

#### Fourier Transform - Signal Processing and Physical Sciences

http://dx.doi.org/10.5772/58658 Edited by Salih Mohammed Salih

#### Contributors

Massoud Amini, Nafya Hameed Mohammed, Daechul Park, Moon Ho Lee, Andrej Prošek, Matjaž Leskovar, Erica Mejia, Juan Ospina, Laura Osorno, Marco Marquez, Alvaro Morales, Nicolae Aldea, Francisco Javier Mendoza Torres, Maria Guadalupe Morales-Macías, Salvador Sánchez-Perales, Juan Alberto Escamilla Reyna, Takashi Nitta, Renbiao Wu, Qiongqiong Jia, Wenyi Wang, Jie Li

#### © The Editor(s) and the Author(s) 2015

The moral rights of the and the author(s) have been asserted.

All rights to the book as a whole are reserved by INTECH. The book as a whole (compilation) cannot be reproduced, distributed or used for commercial or non-commercial purposes without INTECH's written permission. Enquiries concerning the use of the book should be directed to INTECH rights and permissions department (permissions@intechopen.com).

Violations are liable to prosecution under the governing Copyright Law.

#### CCC) BY

Individual chapters of this publication are distributed under the terms of the Creative Commons Attribution 3.0 Unported License which permits commercial use, distribution and reproduction of the individual chapters, provided the original author(s) and source publication are appropriately acknowledged. If so indicated, certain images may not be included under the Creative Commons license. In such cases users will need to obtain permission from the license holder to reproduce the material. More details and guidelines concerning content reuse and adaptation can be foundat http://www.intechopen.com/copyright-policy.html.

#### Notice

Statements and opinions expressed in the chapters are these of the individual contributors and not necessarily those of the editors or publisher. No responsibility is accepted for the accuracy of information contained in the published chapters. The publisher assumes no responsibility for any damage or injury to persons or property arising out of the use of any materials, instructions, methods or ideas contained in the book.

First published in Croatia, 2015 by INTECH d.o.o. eBook (PDF) Published by IN TECH d.o.o. Place and year of publication of eBook (PDF): Rijeka, 2019. IntechOpen is the global imprint of IN TECH d.o.o. Printed in Croatia

Legal deposit, Croatia: National and University Library in Zagreb

Additional hard and PDF copies can be obtained from orders@intechopen.com

Fourier Transform - Signal Processing and Physical Sciences Edited by Salih Mohammed Salih p. cm. ISBN 978-953-51-2127-5 eBook (PDF) ISBN 978-953-51-5761-8

# We are IntechOpen, the world's leading publisher of Open Access books Built by scientists, for scientists

3,800+

116,000+

International authors and editors

120M+

151 Countries delivered to Our authors are among the

most cited scientists

12.2%

Contributors from top 500 universities



WEB OF SCIENCE

Selection of our books indexed in the Book Citation Index in Web of Science™ Core Collection (BKCI)

## Interested in publishing with us? Contact book.department@intechopen.com

Numbers displayed above are based on latest data collected. For more information visit www.intechopen.com



## Meet the editor



Salih Mohammed Salih (SMIEEE) received his B.Sc. degree in Electrical Engineering from the University of Baghdad, Iraq in 1999, his M.Sc. and Ph.D. degrees in Communication Engineering from the University of Technology, Iraq in 2003 and 2008, respectively. Since 2005 he has worked with the University of Anbar, Iraq as a lecturer in the Electrical Engineering Department.

He is currently the director of the Renewable Energy Research Centre (RERC). His research interests include OFDM, space time coding, modulation techniques, security, wireless communications, optical communications, radar, computer networks, digital signal processing, and renewable energy resources. He has published more than 50 papers in local and international journals and conferences.

### Contents

#### Preface XI

Section 1	Signal Processing 1
Chapter 1	Jacket Matrix Based Recursive Fourier Analysis and Its Applications 3 Daechul Park and Moon Ho Lee
Chapter 2	Efficient FFT-based Algorithms for Multipath Interference Mitigation in GNSS 25 Renbiao Wu, Qiongqiong Jia, Wenyi Wang and Jie Li
Chapter 3	<b>Use of Fast Fourier Transform for Sensitivity Analysis 51</b> Andrej Prošek and Matjaž Leskovar
Chapter 4	Henstock-Kurzweil Integral Transforms and the Riemann-Lebesgue Lemma 79 Francisco J. Mendoza-Torres, Ma. Guadalupe Morales-Macías, Salvador Sánchez-Perales and Juan Alberto Escamilla-Reyna
Chapter 5	Double Infinitesimal Fourier Transform 107 Takashi Gyoshin Nitta
Section 2	Physical Sciences 139
Chapter 6	Experimental Data Deconvolution Based on Fourier Trans

- Chapter 6 Experimental Data Deconvolution Based on Fourier Transform Applied in Nanomaterial Structure 141 Adrian Bot, Nicolae Aldea and Florica Matei
- Chapter 7 Gabor-Fourier Analysis 169 Nafya Hameed Mohammad and Massoud Amini

#### Mineralogical Characterization of Chalcopyrite Chapter 8 **Bioleaching 197** E.R. Mejía, J.D. Ospina, L. Osorno, M.A. Márquez and A.L. Morales

### Preface

The Fourier transform is important in engineering, mathematics, and physical sciences. Its discrete counterpart, the discrete Fourier transform (DFT), which is typically computed using the fast Fourier transform (FFT), has revolutionized modern society, as it is ubiquitous in digital electronics and signal processing. This book focuses on Fourier transform applications in signal processing techniques and physical sciences. The field of signal processing has seen an explosive growth during the past decades, as phenomenal advances both in research and applications have been made. During the preparation of this book, we found that almost all the textbooks on signal processing and physics have a section devoted to the Fourier transform theory. The basic idea is that *it is possible to form any function as a summa*tion of a series of sine and cosine terms of increasing frequency. In other words, any space or timevarying data can be transformed into a different domain called the *frequency space*. Joseph Fourier first proposed the idea of Fourier transform in the 19th century, and it had proven to be useful for various applications, mainly in signal processing for many applications. It can be said that Gauss was the first scientist who proposed the techniques that we now call the FFT for calculating the coefficients in a trigonometric expansion of an asteroid's orbit in 1805. However, it was the seminal paper by Cooley and Tukey in 1965 that caught the attention of the science and engineering community and, in a way, proposed the discipline of digital signal processing. The FFT may be the most important numerical algorithm in science, engineering, and applied mathematics. New theoretical results are still appearing, advances in computers and hardware continually restate the basic questions, and new applications open new areas for research. It is hoped that this book will provide the background, references, and incentive to encourage further research and results in this field as well as provide tools for practical applications. One of the features of this book is that the inclusion is simple, and practical examples that expose the reader to real-life signal processing have been given. The whole book contains eight chapters, and it divided into two sections. The first section consists of five chapters that deal with signal processing while the last three chapters deal with physical sciences.

In the first chapter, a unified fast hybrid recursive Fourier transform based on Jacket matrix has been derived. The proposed analysis proves that discrete cosine transform-II (DCT-II), discrete sine transform-II (DST-II), and DFT can be unified by using the diagonal sparse matrix based on the Jacket matrix and recursive structure based on some modifications. In chapter two, a new acquisition algorithm for global navigation satellite system has been introduced. Two multipath interference mitigation algorithms based on the decoupled parameter estimation algorithms are presented in this chapter. The FFT based approach is used to determine the sensitivity of output parameters in chapter three. The signal influenced by sensitive parameter variation is compared with a reference signal. In chapter 4, theorems

about convergence of integrals of products, based on a version of Riemann-Lebesgue Lemma function are presented. Fourier transform using Henstock-Kurzweil Integral is used in this chapter. The real and the complex number fields are extended for treating the Fourier transform for functional in chapter five. Two kinds of Fourier transform theories to the propagator for fields harmonic oscillator are applied.

In chapter six, section two, it is shown that XRD analysis provides more information for understanding the physical properties of nanomaterial structure. In chapter seven, a new approach is introduced for studying the irregular Gabor transform, and proved some non harmonic sets of Fourier expansions for Gabor systems instead of sets of complex exponentials. In chapter eight, the mineral phases formed during chalcopyrite bioleaching are studied using *Acidithiobacillusferrooxidans* bacteria in the absence of ferrous sulfate and elemental sulfur based on Fourier transform infrared spectroscopy, scanning electron microscopy with energy dispersive X-ray spectroscopy, and X-ray diffraction.

Finally, I would like to thank all the authors who have participated in this book for their valuable contributions. Also, I would like to thank all the reviewers for their valuable notes. While there is no doubt that this book may have omitted some significant findings in the Fourier transform field, we hope the information included will be useful for electrical engineers, communication engineers, signal processing engineers, physicians and mathematicians, in addition to the academic researchers working in this field.

Asst. Prof. Salih Mohammed Salih, SMIEEE

Renewable Energy Research Center University of Anbar, Iraq

Section 1

**Signal Processing** 

#### **Chapter 1**

## Jacket Matrix Based Recursive Fourier Analysis and Its Applications

Daechul Park and Moon Ho Lee

Additional information is available at the end of the chapter

http://dx.doi.org/10.5772/59353

#### 1. Introduction

The last decade based on orthogonal transform has been seen a quiet revolution in digital video technology as in Moving Picture Experts Group (MPEG)-4, H.264, and high efficiency video coding (HEVC) [1–7]. The discrete cosine transform (DCT)-II is popular compression structures for MPEG-4, H.264, and HEVC, and is accepted as the best suboptimal transformation since its performance is very close to that of the statistically optimal Karhunen-Loeve transform (KLT) [1-5].

The discrete signal processing based on the discrete Fourier transform (DFT) is popular in wide range of applications depending on specific targets: orthogonal frequency division multiplexing (OFDM) wireless mobile communication systems in 3GPP-LTE [3], mobile worldwide interoperability for microwave access (WiMAX), international mobile telecommunications-advanced (IMT-Advanced), broadcasting related applications such as digital audio broad-casting (DAB), digital video broadcasting (DVB), digital multimedia broadcasting (DMB)) based on DFT. Furthermore, the Haar-based wavelet transform (HWT) is also very useful in the joint photographic experts group committee in 2000 (JPEG-2000) standard [2], [8]. Thus, different applications require different types of unitary matrices and their decompositions. From this reason, in this book chapter we will propose a unified hybrid algorithm which can be used in the mentioned several applications in different purposes.

Compared with the conventional individual matrix decompositions, our main contributions are summarized as follows:



© 2015 The Author(s). Licensee InTech. This chapter is distributed under the terms of the Creative Commons Attribution License (http://creativecommons.org/licenses/by/3.0), which permits unrestricted use, distribution, and eproduction in any medium, provided the original work is properly cited.

- We propose the diagonal sparse matrix factorization for a unified hybrid algorithm based on the properties of the Jacket matrix [9], [10] and the recursive decomposition of the sparse matrix. It has been shown that this matrix decomposition is useful in developing the fast algorithms [11]. Individual DCT-II [1–3], [6], [7], [12], DST-II [4], [6], [7], [13], DFT [3], [5], [14], and HWT [8] matrices can be decomposed to one orthogonal character matrix and a corresponding special sparse matrix. The inverse of the sparse matrix can be easily obtained from the property of the block (element)-wise inverse Jacket matrix. However, there have been no previous works in the development of the common matrix decomposition supporting these transforms.
- We propose a new unified hybrid algorithm which can be used in the multimedia applications, wireless communication systems, and broadcasting systems at almost the same computational complexity as those of the conventional unitary matrix decompositions as summarized in Table 1 and 2. Compared with the existing unitary matrix decompositions, the proposed hybrid algorithm can be even used to the heterogeneous systems with hybrid multimedia terminals being serviced with different applications. The block (element)-wise diagonal decompositions of DCT-II, DST-II, DFT and DWT have a similar pattern as Cooley-Tukey's regular butterfly structures. Moreover, this unified hybrid algorithm can be also applied to the wireless communication terminals requiring a multiuser multiple input-multiple output (MIMO) SVD block diagonalization systems [15], [11,19], [22] and diagonal channels interference alignment management in macro/femto cell coexisting networks [16]. In [15-16, 19, 22-23], a block-diagonalized matrix can be applied to wireless communications MIMO downlink channel.

In Section 2, we present recursive factorization algorithms of DCT-II, DST-II, and DFT matrix for fast computation. In Section 3, hybrid architecture is proposed for fast computations of DCT-II, DST-II, and DFT matrices. Also numerical simulations follow. The conclusion is given in Section 4.

*Notation:* The superscript  $(\cdot)^T$  denotes transposition;  $I_N$  denotes the  $N \times N$  identity matrix; 0 denotes an all-zero matrix of appropriate dimensions;  $C_l^i = \cos(i\pi/l)$ ;  $S_l^i = \sin(i\pi/l)$ ;  $W = e^{-\frac{j2\pi}{N}}$ ;  $\otimes$  and  $\oplus$ , respectively, denote the Kronecker product and the direct sum.

#### 2. Jacket matrix based recursive decompositions of Fourier matrix

#### 2.1. Recursive decomposition of DCT-II

Definition 1: Let  $J_N = \{a_{i,j}\}$  be a matrix, then it is called the Jacket matrix when  $J_N^{-1} = \frac{1}{N} \{(a_{i,j})^{-1}\}^T$ .

That is, the inverse of the Jacket matrix can be determined by its element-wise inverse [9-11]. The row permutation matrix,  $P_N$  is defined by

#### Jacket Matrix Based Recursive Fourier Analysis and Its Applications 5 http://dx.doi.org/10.5772/59353

$$\boldsymbol{P}_{2} = \boldsymbol{I}_{2} \text{ and } \boldsymbol{P}_{N} = \begin{bmatrix} 1 & 0 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ 0 & 0 & 0 & \cdots & 1 & 0 & \cdots & 0 \\ 0 & 1 & 0 & \cdots & 0 & 0 & \cdots & 0 \\ 0 & 0 & 0 & \cdots & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \cdots & 0 & 0 & \cdots & 1 \end{bmatrix}.$$
(1)

where  $\boldsymbol{P}_N$  elements are determined by the following relation:

$$\begin{cases} p_{i,j}=1, & if \quad i=2j, \quad 0 \le j \le \frac{N}{2} - 1, \\ p_{i,j}=1, & if \quad i=(2j+1) \mod N, \quad \frac{N}{2} \le j \le N - 1, \\ p_{i,j}=0, & others. \end{cases}$$

The block column permutation matrix,  $Q_N$  is defined by

$$\boldsymbol{Q}_{N} = \boldsymbol{I}_{2} \text{ and } \boldsymbol{Q}_{N} = \begin{bmatrix} \boldsymbol{I}_{N/4} & \boldsymbol{0}_{N/2} \\ \boldsymbol{0}_{N/2} & \boldsymbol{\overline{I}}_{N/4} \end{bmatrix}, N \ge 4.$$
 (2)

where  $\bar{I}_{N/2}$  denotes reversed identity matrix. Note that  $Q_N^{-1} = Q_N$  and  $P_N^{-1} \neq P_N$ , whereas  $Q_N^{-1} = Q_N^T$  and  $P_N^{-1} = P_N^T$ .

**Proposition 1**: With the use of the Kronecker product and Hadamard matrices, a higher order blockwise inverse Jacket matrix (BIJM) can be recursively obtained by

$$\boldsymbol{J}_{2N} = \boldsymbol{J}_N \otimes \boldsymbol{H}_2, \, N \ge 2 \tag{3}$$

then

$$J_{2N}^{-1} = \frac{1}{N} J_{2N}^{T}$$
(4)

where the lowest order Hadamard matrix is defined by  $H_2 = \begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix}$ 

**Proof**: A proof of this proposition is given in Appendix 6.A.

Note that since the BIJM requires a matrix transposition and then normalization by its size, a class of transforms can be easily inverted as follows:

$$Y_{2N} = J_{2N} X_{2N}$$
, and  $X_{2N} = J_{2N}^{-1} Y_{2N} = \frac{1}{N} J_{2N}^T Y_{2N}$ . (5)

Due to a simple operation of the BIJM, we can reduce the complexity order as the matrix size increases. In the following, we shall use this property of the BIJM in developing a hybrid diagonal block-wise transform.

According to [1-4] and [7], the DCT-II matrix is defined as follows:

$$\boldsymbol{C}_{N} = \sqrt{\frac{2}{N}} \begin{bmatrix} \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & \cdots & \frac{1}{\sqrt{2}} \\ C_{4N}^{2k_{0}\Phi_{0}} & C_{4N}^{2k_{0}\Phi_{1}} & \cdots & C_{4N}^{2k_{0}\Phi_{N-1}} \\ \vdots & \vdots & \ddots & \vdots \\ C_{4N}^{2k_{N-2}\Phi_{0}} & C_{4N}^{2k_{N-2}\Phi_{1}} & \cdots & C_{4N}^{2k_{N-2}\Phi_{N-1}} \end{bmatrix} = \sqrt{\frac{2}{N}} \boldsymbol{X}_{N}$$
(6)

where  $\Phi_i = 2i + 1$  and  $k_i = i + 1$ . We first define a permuted DCT-II matrix  $\tilde{C}_N = P_N^{-1} C_N Q_N^{-1} = \sqrt{\frac{2}{N}} P_N^{-1} X_N Q_N^{-1}$ . We can readily show that the matrix  $X_N$  can be constructed recursively as follows:

$$\boldsymbol{X}_{N} = \boldsymbol{P}_{N} \begin{bmatrix} \boldsymbol{X}_{N/2} & \boldsymbol{X}_{N/2} \\ \boldsymbol{B}_{N/2} & -\boldsymbol{B}_{N/2} \end{bmatrix} \boldsymbol{Q}_{N} = \boldsymbol{P}_{N} \begin{bmatrix} \boldsymbol{X}_{N/2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{B}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & -\boldsymbol{I}_{N/2} \end{bmatrix} \boldsymbol{Q}_{N}.$$
(7)

Here, the matrix  $B_N$  in (7) is given as:

$$\boldsymbol{B}_{N} = \left\{ B_{N}\left(m,n\right) = C_{4N}^{f\left(m,n\right)} \right\}$$
(8)

where f(m, 1) = 2m - 1 and f(m, n + 1) = f(m, n) + 2f(m, 1) for  $m, n \in \{1, 2, ..., N/2\}$ . For example, the matrix  $B_4$  is given by

$$\boldsymbol{B}_{4} = \begin{bmatrix} C_{16}^{1} & C_{16}^{3} & C_{16}^{5} & C_{16}^{7} \\ C_{16}^{3} & -C_{16}^{7} & -C_{16}^{1} & -C_{16}^{5} \\ C_{16}^{5} & -C_{16}^{1} & C_{16}^{7} & C_{16}^{3} \\ C_{16}^{7} & -C_{16}^{5} & C_{16}^{3} & -C_{16}^{1} \end{bmatrix}.$$
(9)

Since  $X_{N/2}^{-1} = \frac{4}{N} X_{N/2}^{T}$  and  $B_{N/2}^{-1} = \frac{4}{N} B_{N/2'}^{T}$  the matrix decomposition in (7) is the form of the matrix product of diagonal block-wise inverse Jacket and Hadamard matrices. The matrix  $B_{N/2}$  is recursively factorized using Lemma 1.

**Lemma 1**: *The matrix*  $B_N$  *can be decomposed as:* 

$$\boldsymbol{B}_N = \boldsymbol{L}_N \boldsymbol{X}_N \boldsymbol{D}_N \tag{10}$$

where a lower triangular matrix  $L_N$  is defined by  $L_N = \{L_N(m, n)\}$  with elements

$$L_{N}(m,n) = \begin{cases} \sqrt{2} (-1)^{m-1}, \forall m \text{ and } n = 1\\ 2(-1)^{m-1} (-1)^{n-1}, m \le n\\ 0, m > n \end{cases}$$
(11)

and a diagonal matrix  $\mathbf{D}_N$  is defined by  $\mathbf{D}_N = diag\{C_{4N'}^{\Phi_0}, C_{4N'}^{\Phi_1}, \dots, C_{4N}^{\Phi_{N-1}}\}$ .

**Proof:***A proof of this Lemma is provided in Appendix 6.B.* 

Using (10), we first rewrite (7) as

$$\boldsymbol{X}_{N} = \boldsymbol{P}_{N} \begin{bmatrix} \boldsymbol{X}_{N/2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{L}_{N/2} \boldsymbol{X}_{N/2} \boldsymbol{D}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & \boldsymbol{-I}_{N/2} \end{bmatrix} \boldsymbol{Q}_{N}$$

$$= \boldsymbol{P}_{N} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{L}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{2} \otimes \boldsymbol{X}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{D}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & \boldsymbol{-I}_{N/2} \end{bmatrix} \boldsymbol{Q}_{N}$$
(12)

which can be evaluated recursively as follows:

$$\boldsymbol{X}_{N} = \boldsymbol{P}_{N} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{L}_{N/2} \end{bmatrix} \times \begin{bmatrix} \boldsymbol{I}_{2} \otimes \begin{bmatrix} \cdots \begin{bmatrix} \boldsymbol{I}_{2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{L}_{2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{2} \otimes \boldsymbol{X}_{2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{L}_{2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{2} \otimes \boldsymbol{X}_{2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{D}_{2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{2} & \boldsymbol{I}_{2} \end{bmatrix} \boldsymbol{Q}_{4} \end{bmatrix} \end{bmatrix} \cdots \end{bmatrix}$$

$$\times \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{D}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & \boldsymbol{-} \boldsymbol{I}_{N/2} \end{bmatrix} \boldsymbol{Q}_{N}.$$

$$(13)$$

Note that in (13) a 2×2 Hadamard matrix is defined by  $X_2 = \begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix}$ . Also, applying the Kronecker product of  $I_2$  and  $X_4$ ,  $X_8$  can be obtained. Keep applying the Kronecker product of  $I_2$  and  $X_{N/2}$ , the final equivalent form of  $X_N$  is obtained. Thus, the proposed systematic decomposition is based on the Jacket and Hadamard matrices.

In [17], the author proposed a recursive decimation-in-frequency algorithm, where the same decomposition specified in (10) was used. However, due to using a different permutation matrix, a different recursive form was obtained. Different recursive decomposition was proposed in [18]. Four different matrices, such as the first matrix, the last matrix, the odd numbered matrix, and the even number matrix, were proposed. Compared to the decomposition in [18], the proposed decomposition is seen to be more systematic and requires less numbers of additions and multiplications. We show a complexity comparison among the proposed decomposition and other methods in Table 1-2.

Potoron co numbo	Conven	tional methods	Proposed				
Kererence number	Addition	Multiplication	Addition	Multiplication			
W. H. Chen at el							
[18]	$3N/2(\log_2 N - 1) + 2$	$N\log_2 N - (3N/2) + 4$	$N \log_2 N$	$N/2(\log_2 N+1)$			
DCT-II							
<b>Z. Wang[13]</b> DST-	$N\left(\frac{7}{4}\log_2(N)-2\right)+3$	$N\left(\frac{3}{4}\log_2(N)-1\right)+3$	$N\log_2 N$	$N/2(\log_2 N + 1)$			
Cooley and Tukey [21] DFT	Nlog <sub>2</sub> N	$(N/2)\log_2 N$	$N\log_2 N$	$(N/2)\log_2 N$			

Table 1. The comparison of computation complexity of conventional independent the DCT-II, DST-II, DFT, and hybrid DCT-II/DST-II/DFT

	Matrix Size, N	Conventional		Proposed	
		Addition	Multiplication	Addition	Multiplication
DCT-II	4	8	6	8	6
	8	26	16	24	16
	16	74	44	64	40
	32	194	116	160	96
	64	482	292	384	224
	128	1154	708	896	512
	256	2690	1668	2048	1152
DST-II	4	9	5	8	6
	8	29	13	24	16
	16	83	35	64	40
	32	219	91	160	96
	64	547	227	384	224
	128	1315	547	896	512
	256	3075	1283	2048	1152
DFT	4	8	4	8	4
	8	24	12	24	12
	16	64	32	64	32

	Matrix Size, N	Conventional		Proposed	
		Addition	Multiplication	Addition	Multiplication
	32	160	80	160	80
	64	384	192	384	192
	128	896	448	896	448
	256	2048	1024	2048	1024

Table 2. Computational Complexity: DCT-II/DST-II/DFT

Applying (13), we can readily compute  $C_N = \sqrt{\frac{2}{N}} X_N$ . The inverse of  $C_N$  can be obtained from the properties of the sparse Jacket matrix inverse:

$$(\boldsymbol{C}_{N})^{-1} = \sqrt{\frac{N}{2}} (\boldsymbol{Q}_{N})^{-1} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & \boldsymbol{-I}_{N/2} \end{bmatrix}^{-1} \begin{bmatrix} \boldsymbol{X}_{N/2}^{-1} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{B}_{N/2}^{-1} \end{bmatrix} \boldsymbol{P}_{N}^{-1}$$

$$= \sqrt{\frac{N}{2}} \boldsymbol{Q}_{N} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & \boldsymbol{-I}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{X}_{N/2}^{T} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{B}_{N/2}^{T} \end{bmatrix} \boldsymbol{P}_{N}^{T}.$$

$$(14)$$

The corresponding butterfly data flow diagram of  $C_N$  is given in Fig. 1.



Figure 1. Regular systematic butterfly data flow of DCT-II.

#### 2.2. Recursive decomposition of the DST-II

The DST-II matrix [1-4] and [7] can be expressed as follows:

$$\boldsymbol{S}_{N} = \sqrt{\frac{2}{N}} \begin{bmatrix} S_{4N}^{2k_{0}\Phi_{0}} & S_{4N}^{2k_{0}\Phi_{1}} & \cdots & S_{4N}^{2k_{0}\Phi_{N-1}} \\ S_{4N}^{2k_{1}\Phi_{0}} & S_{4N}^{2k_{1}\Phi_{1}} & \cdots & S_{4N}^{2k_{1}\Phi_{N-1}} \\ \vdots & \vdots & \ddots & \vdots \\ S_{4N}^{2k_{N-2}\Phi_{0}} & S_{4N}^{2k_{N-2}\Phi_{1}} & \cdots & S_{4N}^{2k_{N-2}\Phi_{N-1}} \\ \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & \cdots & -\frac{1}{\sqrt{2}} \end{bmatrix} = \sqrt{\frac{2}{N}} \boldsymbol{Y}_{N}.$$
(15)

Similar to the procedure we have used in the DCT-II matrix, we first define the permuted DST-II matrix,  $\tilde{S}_N$  as follows:

$$\tilde{\boldsymbol{S}}_{N} = \boldsymbol{P}_{N}^{-1} \boldsymbol{S}_{N} \boldsymbol{\mathcal{Q}}_{N}^{-1} = \sqrt{\frac{2}{N}} \boldsymbol{P}_{N}^{-1} \boldsymbol{Y}_{N} \boldsymbol{\mathcal{Q}}_{N}^{-1}.$$
(16)

From (16), we can have a recursive form for  $Y_N$  as

$$\boldsymbol{Y}_{N} = \boldsymbol{P}_{N} \begin{bmatrix} \boldsymbol{A}_{N/2} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{Y}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & \boldsymbol{-I}_{N/2} \end{bmatrix} \boldsymbol{Q}_{N}$$
(17)

where the submatrix  $A_N$  can be calculated by

$$\boldsymbol{A}_{N} = \boldsymbol{U}_{N} \boldsymbol{Y}_{N} \boldsymbol{D}_{N} \tag{18}$$

where  $U_N$  and  $D_N$  are, respectively, upper triangular and diagonal matrices. The upper triangular matrix  $U_N = \{U_N(m, n)\}$  is defined as follows:

$$U_{N}(m,n) = \begin{cases} \sqrt{2} (-1)^{m-1}, \forall m \text{ and } n = N \\ 2(-1)^{m-1} (-1)^{n-1}, m \ge n \\ 0, m < n \end{cases}$$
(19)

whereas the matrix  $D_N$  is defined as before in (10). The derivation of (18) is given in Appendix C. Recursively applying (18) in (17), Recursively applying (18) in (17), we can find that

$$\mathbf{Y}_{N} = \mathbf{P}_{N} \begin{bmatrix} \mathbf{A}_{N/2} & 0 \\ 0 & \mathbf{Y}_{N/2} \end{bmatrix} \begin{bmatrix} \mathbf{I}_{N/2} & \mathbf{I}_{N/2} \\ \mathbf{I}_{N/2} & -\mathbf{I}_{N/2} \end{bmatrix} \mathbf{Q}_{N} = \mathbf{P}_{N} \begin{bmatrix} \mathbf{U}_{N/2} \mathbf{Y}_{N/2} \mathbf{D}_{N/2} & 0 \\ 0 & \mathbf{Y}_{N/2} \end{bmatrix} \begin{bmatrix} \mathbf{I}_{N/2} & -\mathbf{I}_{N/2} \\ \mathbf{I}_{N/2} & -\mathbf{I}_{N/2} \end{bmatrix} \mathbf{Q}_{N}$$

$$= \mathbf{P}_{N} \begin{bmatrix} \mathbf{U}_{N/2} & 0 \\ 0 & \mathbf{I}_{N/2} \end{bmatrix} \begin{bmatrix} \mathbf{I}_{2} \otimes \mathbf{Y}_{N/2} \end{bmatrix} \begin{bmatrix} \mathbf{D}_{N/2} & 0 \\ 0 & \mathbf{I}_{N/2} \end{bmatrix} \begin{bmatrix} \mathbf{I}_{N/2} & -\mathbf{I}_{N/2} \\ \mathbf{I}_{N/2} & -\mathbf{I}_{N/2} \end{bmatrix} \mathbf{Q}_{N}.$$
(20)

Further applying (17) to the Kronecker product  $[I_2 \otimes Y_{N/2}]$ , the following general recursive form for DST-II matrix can be obtained as:

$$\mathbf{Y}_{N} = \sqrt{\frac{2}{N}} \mathbf{P}_{N} \begin{bmatrix} \mathbf{U}_{N/2} & \mathbf{0} \\ \mathbf{0} & \mathbf{I}_{N/2} \end{bmatrix} \times \begin{bmatrix} \mathbf{I}_{2} \otimes \begin{bmatrix} \mathbf{u}_{1} \begin{bmatrix} \mathbf{U}_{2} & \mathbf{0} \\ \mathbf{0} & \mathbf{I}_{2} \end{bmatrix} \begin{bmatrix} \mathbf{I}_{2} \otimes \mathbf{Y}_{2} \end{bmatrix} \begin{bmatrix} \mathbf{D}_{2} & \mathbf{0} \\ \mathbf{0} & \mathbf{I}_{2} \end{bmatrix} \begin{bmatrix} \mathbf{I}_{2} & -\mathbf{I}_{2} \end{bmatrix} \mathbf{Q}_{4} \end{bmatrix} \cdots \end{bmatrix} \\ \times \begin{bmatrix} \mathbf{D}_{N/2} & \mathbf{0} \\ \mathbf{0} & \mathbf{I}_{N/2} \end{bmatrix} \begin{bmatrix} \mathbf{I}_{N/2} & \mathbf{I}_{N/2} \\ \mathbf{I}_{N/2} & -\mathbf{I}_{N/2} \end{bmatrix} \mathbf{Q}_{N}.$$

$$(21)$$

Note that if we compare (21) and (13), a similarity can be found in the proposed matrix decompositions. That is, starting from the common lowest order  $Y_2 = \begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix}$ , the discrete sine kernel matrix is recursively constructed. Especially, applying the relationship of  $U_N = \tilde{I}_N \tilde{L}_N \tilde{I}_N$ , where  $\tilde{I}_N = \begin{bmatrix} 0 & \cdots & 0 & 1 \\ 0 & \cdots & 1 & 0 \\ \vdots & \ddots & \vdots & \vdots \\ 1 & \cdots & 0 & 0 \end{bmatrix}$  denotes the opposite diagonal identity matrix, the

butterfly data flow of the DST-II matrix can be obtained from the corresponding that of the proposed DCT-II decomposition. The butterfly data flow graph of the DST-II matrix is shown in Fig. 2.

Now utilizing the properties of the BIJM, we can first obtain

$$\begin{bmatrix} A_{N/2} & 0\\ 0 & Y_{N/2} \end{bmatrix}^{-1} = \frac{2}{N} \begin{bmatrix} A_{N/2}^{T} & 0\\ 0 & Y_{N/2}^{T} \end{bmatrix}$$
(22)

such that the inverse of the matrix  $S_N$  is given by

$$\boldsymbol{S}_{N}^{-1} = \sqrt{\frac{N}{2}} \boldsymbol{\varrho}_{N} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & -\boldsymbol{I}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{A}_{N/2}^{T} & \boldsymbol{0} \\ \boldsymbol{0} & \boldsymbol{Y}_{N/2}^{T} \end{bmatrix} \boldsymbol{P}_{N}^{T}.$$
(23)

Note that applying again the properties of the BIJM and (18), a recursive form of the inverse DST-II can be easily obtained.



Figure 2. Regular systematic butterfly data flow of DST-II.

#### 2.3. Recursive decomposition of DFT

The DFT is a Fourier representation of a given sequence  $\{x(n)\}$ ,

$$X(n) = \sum_{m=0}^{N-1} x(m) W^{nm}, \ 0 \le n \le N-1.$$
(24)

where  $W = e^{-j2\pi/N}$ . The *N* -point DFT matrix can be denoted by  $F_N = \{W^{nm}\}$ . The *N* × *N* Sylvester Hadamard matrix is denoted by  $H_N$ . The Sylvester Hadamard matrix is generated by the successive Kronecker products:

$$\boldsymbol{H}_{N} = \boldsymbol{H}_{2} \otimes \boldsymbol{H}_{N/2} \tag{25}$$

for N = 4, 8, ... In (25), we define  $H_2 = \begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix}$ . We decompose a sparse matrix  $E_N = P_N \tilde{F}_N W_N$  in the following way:

$$\boldsymbol{F}_{N} = \begin{bmatrix} \boldsymbol{P}_{N} \end{bmatrix}^{T} \tilde{\boldsymbol{F}}_{N}$$

$$\tilde{\boldsymbol{F}}_{N} = \begin{bmatrix} \tilde{\boldsymbol{F}}_{N/2} & \tilde{\boldsymbol{F}}_{N/2} \\ \boldsymbol{E}_{N/2} & -\boldsymbol{E}_{N/2} \end{bmatrix} = \begin{bmatrix} \tilde{\boldsymbol{F}}_{N/2} & 0 \\ 0 & \boldsymbol{E}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & -\boldsymbol{I}_{N/2} \end{bmatrix}$$
(26)

where  $E_{N/2}$  is further decomposed by Lemma 1

$$\boldsymbol{E}_{N/2} = \boldsymbol{P}_{N/2} \tilde{\boldsymbol{F}}_{N/2} \boldsymbol{W}_{N/2} \tag{27}$$

where  $W_N$  is the diagonal complex unit for the N-point DFT matrix. That is, we have  $W_N = diag\{W^0, \dots, W^{N-1}\}$ .



Figure 3. Butterfly data flow of DFT.

Similar to the development for DCT-II and DST-II, we first rewrite (26) using (27) as

$$\tilde{\boldsymbol{F}}_{N} = \begin{bmatrix} \tilde{\boldsymbol{F}}_{N/2} & 0 \\ 0 & \boldsymbol{P}_{N/2} \tilde{\boldsymbol{F}}_{N/2} \boldsymbol{W}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & \boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & -\boldsymbol{I}_{N/2} \end{bmatrix}$$

$$= \begin{bmatrix} \boldsymbol{I}_{N/2} & 0 \\ 0 & \boldsymbol{P}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{2} \otimes \tilde{\boldsymbol{F}}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & 0 \\ 0 & \boldsymbol{W}_{N/2} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_{N/2} & -\boldsymbol{I}_{N/2} \\ \boldsymbol{I}_{N/2} & -\boldsymbol{I}_{N/2} \end{bmatrix}.$$
(28)

 $[I_2 \otimes \tilde{F}_{N/2}]$  in (28) can be recursively decomposed in the following way:

$$\tilde{F}_{N} = \begin{bmatrix} I_{N/2} & 0 \\ 0 & P_{N/2} \end{bmatrix} \times \begin{bmatrix} I_{2} \otimes \begin{bmatrix} \dots \\ 0 & P_{2} \end{bmatrix} \begin{bmatrix} I_{2} \otimes \tilde{F}_{2} \end{bmatrix} \begin{bmatrix} I_{2} & 0 \\ 0 & W_{2} \end{bmatrix} \begin{bmatrix} I_{2} & I_{2} \\ I_{2} & -I_{2} \end{bmatrix} \cdots \\ \vdots \\ \hline \tilde{F}_{4} \\ \hline \tilde{F}_{N/2} \end{bmatrix} \end{bmatrix} \times \begin{bmatrix} I_{N/2} & 0 \\ 0 & W_{N/2} \end{bmatrix} \begin{bmatrix} I_{N/2} & I_{N/2} \\ I_{N/2} & -I_{N/2} \end{bmatrix}.$$
(29)

It is clear that the form of (29) is the same as that of (13), where we only need to change  $L_l$  to  $P_l$  and  $D_l$  to  $W_l$  for  $l \in \{2, 4, 8, ..., N/2\}$  to convert the DCT-II matrix into DFT matrix. Consequently, the butterfly data flow of the DFT matrix can be drawn in Fig. 3 using the baseline architecture of DCT-II.

## 3. Proposed hybrid architecture for fast computations of DCT-II, DST-II, and DFT matrices

We have derived recursive formulas for DCT-II, DST-II, and DFT. The derived results show that DCT-II, DST-II, and DFT matrices can be unified by using a similar sparse matrix decomposition algorithm, which is based on the block-wise Jacket matrix and diagonal recursive architecture with different characters. The conventional method is only converted from DFT to DCT-II, DST-II. But our proposed method can be universally switching from DCT-II to DST-II, and DFT vice versa. Figs. 1-3 exhibit the similar recursive flow diagrams and let us motivate to develop universal hybrid architecture via switching mode selection. Moreover, the butterfly data flow graphs have  $log_2N$  stages. From Fig.1, we can generate Figs. 2-3 according to the following proposed ways:

#### 3.1. From DCT-II to DST-II

The N-point DCT-II of x is given by

$$X_{N}^{DCT}(m) = c_{m} \sqrt{\frac{2}{N}} \sum_{n=0}^{N-1} x(n) \cos \frac{m(2n+1)\pi}{2N} = c_{m} \sqrt{\frac{2}{N}} C_{N} \mathbf{x}$$
  
where  $m, n = 0, 1, ..., N-1, c_{m} = \begin{cases} 1, ..., m \neq 0\\ 1/\sqrt{2}, m = 0 \end{cases}$  (30)

The N-point DST-II of **x** is given by

#### Jacket Matrix Based Recursive Fourier Analysis and Its Applications 15 http://dx.doi.org/10.5772/59353

$$X_{N}^{DST}(m) = s_{m} \sqrt{\frac{2}{N}} \sum_{n=0}^{N-1} x(n) \sin \frac{(m+1)(2n+1)\pi}{2N} = s_{m} \sqrt{\frac{2}{N}} S_{N} \mathbf{x}$$
  
where  $m, n = 0, 1, ..., N-1, s_{m} = \begin{cases} 1, & m \neq N-1 \\ 1/\sqrt{2}, & m = N-1 \end{cases}$  (31)

Let  $C_N$  and  $S_N$  be orthogonal  $N \times N$  DCT-II and DST-II matrices, respectively. Also,  $x = [x(0) \ x(1) \ \dots \ x(N-1)]^T$  denotes the column vector for the data sequence x(n). Substituting m = N - k - 1,  $k = 1, 2, \dots, N$  into (30), we have

$$C_N(N-k-1) = c_{N-k} \sqrt{\frac{2}{N}} \sum_{n=0}^{N-1} x(n) \cos \frac{(2n+1)(N-k-1)\pi}{2N}, \ k = 0, 1, 2, ..., N-1$$
(32)

Using the following trigonometric identity

$$\cos\left(\frac{(2n+1)\pi}{2} - \frac{(2n+1)(k+1)\pi}{2N}\right) = \cos\left(\frac{(2n+1)\pi}{2}\right)\cos\left(\frac{(2n+1)(k+1)\pi}{2N}\right) + \sin\left(\frac{(2n+1)\pi}{2}\right)\sin\left(\frac{(2n+1)(k+1)\pi}{2N}\right)$$
(33)  
=  $(-1)^{n}\sin\left(\frac{(2n+1)(k+1)\pi}{2N}\right)$ 

(32) becomes

$$C_N(N-k-1) = c_{N-k} \sqrt{\frac{2}{N}} \sum_{n=0}^{N-1} (-1)^n x(n) \sin \frac{(2n+1)(k+1)\pi}{2N}$$
(34)

where  $C_N = (N - k - 1)$  represents the reflected version of  $C_N(k)$  and this can be achieved by multiplying the reversed identity matrix  $\overline{I}_N$  to  $C_N$ . (34) can be represented in a more compact matrix multiplication form [13]:

$$\boldsymbol{S}_{N} = \overline{\boldsymbol{I}}_{N} \boldsymbol{C}_{N} \boldsymbol{M}_{N} \Leftrightarrow \boldsymbol{C}_{N} = \overline{\boldsymbol{I}}_{N} \boldsymbol{S}_{N} \boldsymbol{M}_{N}$$
(35)

where,  $M_N = [M_1 \otimes I_{N/2}], M_1 = \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix}$ 

Then, the DST-II matrix is resulted from the DCT-II matrix. Note that compatibility property exists in the DCT-II and DST-II.

#### 3.2. From DFT to DCT-II

The (m,n) elements of the DCT-II kernel matrix is expressed by

$$[C_N]_{m,n} = c_m \sqrt{\frac{2}{N}} \cos \frac{m(2n+1)\pi}{2N}$$
(36)

A new sequence  $x^{(1)}(n)$  is defined by

$$\begin{cases} x^{(1)}(n) = x(2n) & \text{for } 0 \le n \le N/2 - 1\\ x^{(1)}(N-n-1) = x(2n+1) & \text{for } 0 \le n \le N/2 - 1 \end{cases}$$
(37)

For the sequence  $x^{(1)}(n)$ , we see that we can write

$$X_{N}^{DCT}(m) = c_{m} \sqrt{\frac{2}{N}} \sum_{n=0}^{N-1} x^{(1)}(n) \cos \frac{m(4n+1)\pi}{2N} = c_{m} \sqrt{\frac{2}{N}} \sum_{n=0}^{N-1} x^{(1)}(n) \cos 2\pi \frac{m}{2N} \left(2n + \frac{1}{2}\right)$$
$$= c_{m} \sqrt{\frac{2}{N}} \mathsf{R} \left(\sum_{n=0}^{N-1} x^{(1)}(n) e^{-j2\pi m(2n+1/2)/2N}\right) = c_{m} \sqrt{\frac{2}{N}} \mathsf{R} \left(e^{-j\pi m/2N} \sum_{n=0}^{N-1} x^{(1)}(n) e^{-j2\pi mn/N}\right)$$
$$= c_{m} \sqrt{\frac{2}{N}} \mathsf{R} \left(e^{-j\pi m/2N} F_{N} \mathbf{x}^{(1)}\right)$$
(38)

where **R** indicates a real part.

With the result above we have avoided computing a DFT of double size. We have

$$\mathbf{W}_{4N} = diag\left\{W_{4N}^{0}, \dots, W^{N-1}\right\} = diag\left\{1, e^{-j\pi/2N}, e^{-j\pi^{2/2N}}, \dots, e^{-j\pi(N-1)/2N}\right\}$$
(39)

Now, the result can be put in the more compact matrix-vector form

$$C_N = c_m \sqrt{\frac{2}{N}} \mathbf{R} \left( \mathbf{W}_{4N} F_N \right) \tag{40}$$

Then, the DCT-II matrix is resulted from the DFT matrix.

#### 3.3. From DCT-II and DST-II to DFT

We develop a relation between the circular convolution operation in the discrete cosine and sine transform domains. We need to measure half of the total coefficients. The main advantage

of a proposed new relation is that the input sequences to be convolved need not be symmetrical or asymmetrical. Thus, the transform coefficients can be either symmetric or asymmetric [21].

From (30) and (31), it changes to coefficient for circular convolution (C) format. Thus, we have the following equations:

$$\mathbf{X}_{N}^{DCT-IIC}(m) = 2\sum_{n=0}^{N-1} x(n) \cos\left(\frac{m(2n+1)}{2N}\right), \quad m = 0, 1, \dots, N-1$$

$$\mathbf{X}_{N}^{DST-IIC}(m) = 2\sum_{n=0}^{N-1} x(n) \sin\left(\frac{m(2n+1)}{2N}\right), \quad m = 1, \dots, N$$
(41)

We can rewrite the DFT (24)

$$X(m) = \sum_{n=0}^{N-1} x(n) e^{-j2\pi mn/N}, \ m = 0, 1, \dots, N-1.$$
(42)

Multiplying (42) by  $2e^{-j\pi m/N}$ , we can get

$$2e^{-j\pi m/N} X(m) = 2e^{-j\pi m/N} \sum_{n=0}^{N-1} x(n) e^{-j2\pi mn/N} = 2\sum_{n=0}^{N-1} x(n) e^{-j\pi m/N} e^{-j2\pi mn/N}$$

$$= 2\sum_{n=0}^{N-1} x(n) e^{-j\left[\frac{m(2n+1)\pi}{N}\right]} = 2\sum_{n=0}^{N-1} x(n) \left(\cos\left[\frac{m(2n+1)\pi}{N}\right] - j\sin\left[\frac{m(2n+1)\pi}{N}\right]\right).$$
(43)

Comparing the first term of (41) with first one of (43), it can be seen that  $2\sum_{n=0}^{N-1} \mathbf{x}(n) \left( \cos \left[ \frac{m(2n+1)\pi}{N} \right] \right)$  is decimated and asymmetrically extended of (41) with index m=0:N-1. Similarly,  $2\sum_{n=0}^{N-1} \mathbf{x}(n) \left( \sin \left[ \frac{m(2n+1)\pi}{N} \right] \right)$  is decimated and symmetrically extended of (41) with index m=1:N. It is observed that proper zero padding of the sequences, symmetric convolution can be used to perform linear convolution. The circular convolution of cosine and sine periodic sequences in time/spatial domain is equivalent to multiplication in the DFT domain. Then, the DFT matrix is resulted from the DCT-II and DST-II matrices.

#### 3.4. Unified hybrid fast algorithm

Based on the above conversions from the proposed decomposition of DCT-II, we can form a hybrid fast algorithm that can cover DCT-II, DST-II, and DFT. The general block diagram of the proposed hybrid fast algorithm is shown in Fig. 4. The common recursive block of  $[P]_{N/2^{h-1}}L$  blockdiagonal() $[I_2 \otimes Z_2]$ Rblockdiagonal() $\begin{bmatrix} I_2 & I_2 \\ I_2 & -I_2 \end{bmatrix} Q_{N/2^{h-1}}$  is multiplied repeatedly

according to the size of the kernel with different transforms as like as bracket (((( $\cdot$ )))). The requiring computational complexity of individual DCT-II, DST-II, and DFT is summarized in Table 1 and Table 2. It can be seen that the proposed hybrid algorithm requires little more computations in addition and multiplication compared to Wang's result [13]. However, the proposed scheme requires a much less computational complexity in addition and multiplication compared to those of the decompositions proposed by [11,13,18]. In addition, compared to these transforms, the proposed hybrid fast algorithm can be efficiently extensible to larger transform sizes due to its diagonal block-wise inverse operation of recursive structure. Moreover, the proposed hybrid structure is easily extended to cover different applications. For example, a base station wireless communication terminal delivers a compressed version of multimedia data via wireless communications network. Either DCT-II or DST-II can be used in compressing multimedia data since the proposed decomposition is based on block diagonalization it can significantly reduce its complexity due to simple structure[11,19, 22], for various multimedia sources. The DCT image coding can be easily implemented in the proposed hybrid structure as shown in Fig. 4(b). From (45), the DCT-II is obtained by taking a real part of multiplication result of  $e^{-j\pi m/2N}$  with  $F_N = \{W^{nm}\}$ . If the DCT-II is multiplied by  $I_N C_N M_N$ , then we get DST. If the DCT and DST are convolved in time and frequency domain and multiplied by  $2e^{-j\pi m/N}$ , the DFT matrix can be obtained. Thus, the proposed hybrid algorithm enables the terminal to adapt to its operational physical device and size.



Figure 4. Recursive DCT-II/DST-II/DFT Structure Based on Jacket matrix.

#### 3.5. Numerical simulations

As shown in [7] the coding performance DST outperforms DCT at high correlation values ( $\rho$ ) and is very close to that of the KLT. Since the basis vectors of DCT maximize their energy distribution at both ends, hence the discontinuity appears at block boundaries due to quantization effects. However, since the basis vectors of DST minimizes their energy distribution at other ends, DST provides smooth transition between neighboring blocks. Therefore, the proposed hybrid transform coding scheme provides a consistent reconstruction and preserves more details, as shown in Fig. 6 with a size of 512 x 512 and 8 bits quantization.

Now consider an  $N \times N$  block of pixels, X, containing  $x_{i,j}$ , i, j=1, 2, ..., N. We can write 2-D transformation for the *k*th block X as  $Y_s = T_s Q X_k Q^T$  and  $Y_c = T_c X_k$ .

Depending on the availability of boundary values (in top- boundary and left-boundary) in images the hybrid coding scheme accomplishes the 2-D transform of a block pixels as two sequential 1-D transforms separately performed on rows and columns. Therefore the choice of 1-D transform for each direction is dependent on the corresponding prediction boundary condition.

- Vertical transform (for each column vector): employ DST if top boundary is used for prediction; otherwise use DCT.
- Horizontal transform (for each row vector): employ DST if left boundary is used for prediction; otherwise use DCT.

What we observed from numerical experiments is that the combined scheme over DCT-II only performs better in perceptual clarity as well as PSNR. Jointly optimized spatial prediction and block transform (see Fig. 5 (e) and (f)) using DCT/DST-II compression(PSNR 35.12dB) outperforms only DCT-II compression(PSNR 32.38dB). Less blocky artifacts are revealed compared to that of DCT-II. Without *a priori* knowledge of boundary condition, DCT-II performs better than any other block transform coding. The worst result is obtained using DST-II only.

#### 4. Conclusion

In this book chapter, we have derived a unified fast hybrid recursive Fourier transform based on Jacket matrix. The proposed analysis have shown that DCT-II, DST-II, and DFT can be unified by using the diagonal sparse matrix based on the Jacket matrix and recursive structure with some characters changed from DCT-II to DST-II, and DFT. The proposed algorithm also uses the matrix product of recursively lower order diagonal sparse matrix and Hadamard matrix. The resulting signal flow graphs of DCT-II, DST-II, and DFT have a regular systematic butterfly structure. Therefore, the complexity of the proposed unified hybrid algorithm has been much less as its matrix size gets larger. This butterfly structure has grown by a recursive nature of the fast hybrid Jacket Hadamard matrix. Based on a systematic butterfly structure, a unified switching system can be devised. We have also applied the circulant channel matrix in our proposed method. Thus, the proposed hybrid scheme can be effectively applied to the heterogeneous transform systems having various matrix dimensions. Jointly optimized DCT and DST-II compression scheme have revealed a better performance (about 3dB) over the DCT or DST only compression method.



(b) Zoomed original Lena image

(d) Zoomed DCT-II compressed Lena image

(f) Zoomed DCT/DST-II compressed Lena image

Figure 5. Image Coding Results showing DCT-II only and jointly optimized DCT/DST-II compression (a) Original Lena image (b) zoomed original Lena image (c) DCT-II compressed Lena image(PSNR=32.38 dB) (d) Zoomed DCT-II compressed Lena image (e) DCT/DST-II compressed Lena image (PSNR=35.12 dB) (f) Zoomed DCT/DST-II compressed Lena image.

#### Appendix

#### Appendix A

#### A Proof of Proposition 1

We use mathematical induction to prove Proposition 1. The lowest order BIJM is defined as

$$\boldsymbol{J}_{8} = \begin{bmatrix} \boldsymbol{I}_{2} & \boldsymbol{I}_{2} & \boldsymbol{I}_{2} & \boldsymbol{I}_{2} \\ \boldsymbol{I}_{2} & -\boldsymbol{C}_{2} & \boldsymbol{C}_{2} & -\boldsymbol{I}_{2} \\ \boldsymbol{I}_{2} & \boldsymbol{C}_{2} & -\boldsymbol{C}_{2} & -\boldsymbol{I}_{2} \\ \boldsymbol{I}_{2} & -\boldsymbol{I}_{2} & -\boldsymbol{I}_{2} & \boldsymbol{I}_{2} \end{bmatrix}$$
(44)

where  $C_2 = \frac{H_2}{\sqrt{2}}$ . Since

$$\boldsymbol{J}_{8}^{-1} = \begin{bmatrix} \boldsymbol{I}_{2} & \boldsymbol{I}_{2} & \boldsymbol{I}_{2} & \boldsymbol{I}_{2} \\ \boldsymbol{I}_{2} & -\boldsymbol{C}_{2}^{T} & \boldsymbol{C}_{2}^{T} & -\boldsymbol{I}_{2} \\ \boldsymbol{I}_{2} & \boldsymbol{C}_{2}^{T} & -\boldsymbol{C}_{2}^{T} & -\boldsymbol{I}_{2} \\ \boldsymbol{I}_{2} & -\boldsymbol{I}_{2} & -\boldsymbol{I}_{2} & \boldsymbol{I}_{2} \end{bmatrix}$$
(45)

equation (4) holds for 2N = 8. Now we assume that the BIJM  $J_N$  satisfies (4), i.e.,  $J_N J_N^T = \frac{N}{2} I_N$ . Since  $J_{2N} J_{2N}^T = (J_N \otimes H_2)(J_N \otimes H_2)^T = (J_N J_N^T) \otimes (H_2 H_2^T) = \frac{N}{2} I_N \otimes 2I_2 = N I_{2N}$ , this proposition is proved by mathematical induction that (4) holds for all 2N. If N = 1, certainly  $J_2 J_2^T = I_2$ .

#### Appendix B

#### A Proof of Lemma 1

According to the definition of an  $N \times N$  matrix  $B_N$ ,  $B_N$  is given as follows:

$$\boldsymbol{B}_{N} = \begin{bmatrix} C_{4N}^{\Phi_{0}} & C_{4N}^{\Phi_{1}} & C_{4N}^{\Phi_{2}} & \cdots & C_{4N}^{\Phi_{N-1}} \\ C_{4N}^{(2k_{0}+1)\Phi_{0}} & C_{4N}^{(2k_{0}+1)\Phi_{1}} & C_{4N}^{(2k_{0}+1)\Phi_{2}} & \cdots & C_{4N}^{(2k_{0}+1)\Phi_{N-1}} \\ C_{4N}^{(2k_{1}+1)\Phi_{0}} & C_{4N}^{(2k_{1}+1)\Phi_{1}} & C_{4N}^{(2k_{1}+1)\Phi_{2}} & \cdots & C_{4N}^{(2k_{1}+1)\Phi_{N-1}} \\ \vdots & \vdots & \vdots & \cdots & \vdots \\ C_{4N}^{(2k_{N-2}+1)\Phi_{0}} & C_{4N}^{(2k_{N-2}+1)\Phi_{1}} & C_{4N}^{(2k_{N-2}+1)\Phi_{2}} & \cdots & C_{4N}^{(2k_{N-2}+1)\Phi_{N-1}} \end{bmatrix}$$
(46)

where  $k_i = i + 1$ . Since  $\cos((2k + 1)\Phi_m) = 2\cos(2k\Phi_m)\cos(\Phi_m) - \cos((2k - 1)\Phi_m)$ , we have

$$C_{4N}^{(2k_i+1)\Phi_m} = -C_{4N}^{(2k_i-1)\Phi_m} + 2C_{4N}^{(2k_i)\Phi_m}C_{4N}^{\Phi_m}.$$
(47)

Using (47),  $B_N$  can be decomposed as:

$$\boldsymbol{B}_{N} = \boldsymbol{L}_{N} \begin{bmatrix} \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & \cdots & \frac{1}{\sqrt{2}} \\ C_{4N}^{2k_{0}\Phi_{0}} & C_{4N}^{2k_{0}\Phi_{1}} & C_{4N}^{2k_{0}\Phi_{2}} & \cdots & C_{4N}^{2k_{0}\Phi_{N-1}} \\ C_{4N}^{2k_{1}\Phi_{0}} & C_{4N}^{2k_{1}\Phi_{1}} & C_{4N}^{2k_{1}\Phi_{2}} & \cdots & C_{4N}^{2k_{1}\Phi_{N-1}} \\ \vdots & \vdots & \vdots & \cdots & \vdots \\ C_{4N}^{2k_{N-2}\Phi_{0}} & C_{4N}^{2k_{N-2}\Phi_{1}} & C_{4N}^{2k_{N-2}\Phi_{2}} & \cdots & C_{4N}^{2k_{N-2}\Phi_{N-1}} \end{bmatrix} \boldsymbol{D}_{N}$$

$$(48)$$

$$= \boldsymbol{L}_{N} \boldsymbol{X}_{N} \boldsymbol{D}_{N}$$

which proves (10) in Lemma 1.

#### Appendix C

#### A Proof of Equation (18)

By using the sum and difference formulas for the sine function, we can have

$$\begin{split} S_{4N}^{(2k_{N-1})\Phi_{j}} &= C_{4N}^{\Phi_{j}} = S_{4N}^{\Phi_{N-j-1}}, S_{4N}^{(2k_{i}-1)\Phi_{j}} = 2S_{4N}^{2k_{i}\Phi_{j}}C_{4N}^{\Phi_{j}} - S_{4N}^{(2k_{i+1}-1)\Phi_{j}}, \\ S_{4N}^{(2k_{i+1}-1)\Phi_{j}} &= 2S_{4N}^{(2k_{0}-1)\Phi_{j}} - S_{4N}^{(2k_{1}-1)\Phi_{j}}, \\ S_{4N}^{(2k_{0}-1)\Phi_{j}} &= \left(2S_{4N}^{(2k_{0}-1)\Phi_{j}} - 2S_{4N}^{(2k_{1})\Phi_{j}} + \dots + 2S_{4N}^{(2k_{N-2}-1)\Phi_{j}}\right)C_{4N}^{\Phi_{j}} \\ &= 2S_{4N}^{(2k_{0}-1)\Phi_{j}}C_{4N}^{\Phi_{j}} - S_{4N}^{(2k_{1}-1)\Phi_{j}}, \\ S_{4N}^{(2k_{1}-1)\Phi_{j}} &= \left(2S_{4N}^{(2k_{1}-1)\Phi_{j}} - 2S_{4N}^{(2k_{1}-1)\Phi_{j}} + \dots + 2S_{4N}^{(2k_{N-2}+1)\Phi_{j}}\right)C_{4N}^{\Phi_{j}} \\ &= 2S_{4N}^{(2k_{1}-1)\Phi_{j}}C_{4N}^{\Phi_{j}} - S_{4N}^{(2k_{2}-1)\Phi_{j}}, \\ \vdots \\ S_{4N}^{(2k_{N-3}-1)\Phi_{j}} &= \left(2S_{4N}^{(2k_{N-3}-1)\Phi_{j}} - 2S_{4N}^{(2k_{N-2})\Phi_{j}} + 1\right)C_{4N}^{\Phi_{j}} \\ &= 2S_{4N}^{(2k_{N-3}-1)\Phi_{j}}C_{4N}^{\Phi_{j}} - S_{4N}^{(2k_{N-2}-1)\Phi_{j}}, \\ S_{4N}^{(2k_{N-3}-1)\Phi_{j}} &= \left(2S_{4N}^{(2k_{N-3}-1)\Phi_{j}} - 2S_{4N}^{(2k_{N-2}-1)\Phi_{j}}, \\ S_{4N}^{(2k_{N-3}-1)\Phi_{j}} &= \left(2S_{4N}^{(2k_{N-3}-1)\Phi_{j}} - 2S_{4N}^{(2k_{N-2}-1)\Phi_{j}}, \\ S_{4N}^{(2k_{N-3}-1)\Phi_{j}} &= \left(2S_{4N}^{(2k_{N-2})\Phi_{j}} - 1\right)C_{4N}^{\Phi_{j}} \\ &= 2S_{4N}^{(2k_{N-2}-1)\Phi_{j}} C_{4N}^{\Phi_{j}} - S_{4N}^{(2k_{N-1}-1)\Phi_{j}} \end{split}$$

where  $k_i = i + 1$ ,  $\Phi_j = 2j + 1$ ,  $i, j = 0, 1, \dots, N - 1$ .

By taking (49) and into the right hand side of (18), we have

$$\boldsymbol{U}_{N}\boldsymbol{Y}_{N}\boldsymbol{D}_{N} = \begin{bmatrix} S_{4N}^{(2k_{0}-1)\Phi_{0}} & S_{4N}^{(2k_{0}-1)\Phi_{1}} & \cdots & S_{4N}^{(2k_{0}-1)\Phi_{N-1}} \\ S_{4N}^{(2k_{1}-1)\Phi_{0}} & S_{4N}^{(2k_{1}-1)\Phi_{1}} & \cdots & S_{4N}^{(2k_{1}-1)\Phi_{N-1}} \\ \vdots & \vdots & \ddots & \vdots \\ S_{4N}^{(2k_{N}-1-1)\Phi_{0}} & S_{4N}^{(2k_{N}-1-1)\Phi_{1}} & \cdots & S_{4N}^{(2k_{N}-1)\Phi_{N-1}} \end{bmatrix}.$$
(50)

The left hand side of (18) matrix  $[A]_N$  from  $[Y]_N$  can be represented by

$$\boldsymbol{A}_{N} = \begin{bmatrix} S_{4N}^{(2k_{0}-1)\phi_{0}} & S_{4N}^{(2k_{0}-1)\phi_{1}} & \cdots & S_{4N}^{(2k_{0}-1)\phi_{N-1}} \\ S_{4N}^{(2k_{1}-1)\phi_{0}} & S_{4N}^{(2k_{1}-1)\phi_{1}} & \cdots & S_{4N}^{(2k_{1}-1)\phi_{N-1}} \\ \vdots & \vdots & \ddots & \vdots \\ S_{4N}^{(2k_{N-1}-1)\phi_{0}} & S_{4N}^{(2k_{N-1}-1)\phi_{1}} & \cdots & S_{4N}^{(2k_{N-1}-1)\phi_{N-1}} \end{bmatrix}.$$
(51)

We can obtain (50) and (51) are the same and the expression of (18) is correct.

#### Acknowledgements

This work was supported by MEST 2012-002521, NRF, Korea.

#### Author details

Daechul Park1\* and Moon Ho Lee2

\*Address all correspondence to: fia4joy@gmail.com

1 Hannam University, Department of Information and Communication engineering, Korea

2 Chonbuk National University, Division of Electronics and Information Engineering, Korea

#### References

- [1] Rao, KR. and Yip, P., *Discrete Cosine Transform: Algorithms, Advantages, Applications*. Boston, MA: Academic Press, 1990.
- [2] Richardson, IE., *The H.264 Advanced Video Compression Standard*, 2nd ed. Hoboken, New Jersey: John Wiley and Sons.
- [3] Rao, KR., Kim, DN., and Hwang, J. J., *Fast Fourier Transform: Algorithm and Applications*. New York, N.Y.: Springer, 2010.
- [4] Jain, A. K., Fundamentals of Digital Image Processing. Prentice Hall, 1987.
- [5] Wang, R., Introduction to Orthogonal Transforms: With Applications in Data Processing and Analysis. Cambridge, UK: Cambridge University Press, 2012.
- [6] ITU-T SG16 WP3/JCT-VC, CE 7.5, "Performance analysis of adaptive DCT/DST selection," July 2011.
- [7] Hai, J., Saxena, A., Melkote, V., and Rose, K., "Jointly optimized spatial prediction and block transform for video and image coding," *IEEE Trans. Image Process.*, vol. 21, no. 4, pp. 1874–1884, April 2012.
- [8] Strang, G. and Nguyen, T., Wavelets and Filer Banks. Wellesley, MA: Wellesley-Cambridge Press, 1996.
- [9] Lee, MH., "A new reverse Jacket transform and its fast algorithm," *IEEE Trans. Circuits Syst. II*, vol. 47, no. 1, pp. 39–47, Jan. 2000.
- [10] Chen, Z., Lee, MH, and Zeng, G., "Fast cocyclic Jacket transform," IEEE Trans. Signal Process., vol. 56, pp. 2143–2148, May 2008.

- [11] Lee, MH., Jacket Matrices-Construction and Its Application for Fast Cooperative Wireless Signal Processing. LAP LAMBERT Academic publishing, Germany, November, 2012.
- [12] Wang, CL. and Chen, CY., "High-throughput VLSI architectures for the 1-D and 2-D discrete cosine transform," *IEEE Trans. Circuits Syst. Video Technol.*, vol. 5, pp. 31–40, Feb. 1995.
- [13] Wang, Z., "Fast Algorithm for the Discrete W Transform and for the Discrete Fourier Transform," *IEEE Trans. on Acoustics, Speech and Signal Process.*, vol. 32, No. 4, pp. 803 – 816, Aug. 1984.
- [14] Lee, MH., "High speed multidimensional systolic arrays for discrete Fourier transform," *IEEE Trans. Circuits Syst. II*, vol. 39, no. 12, pp. 876–879, Dec. 1992.
- [15] Kim, KJ., Fan, Y.,Iltis, R. A., Poor, H. V., and Lee, M. H., "A reduced feedback precoder for MIMO-OFDM cooperative diversity system," *IEEE Trans. Veh. Technol.*, vol. 61, pp. 584–596, Feb. 2012.
- [16] Jang, U., Cho, K., Ryu, W., and Lee, HJ., "Interference management with block diagonalization for macro/femto coexisting networks," *ETRI Journal*, vol. 34, pp. 297–307, June 2012.
- [17] Hou, HS., "A fast recursive algorithm for computing the discrete cosine transform," *IEEE Trans. Acoust., Speech, Signal Process.*, vol. 35, no. 10, pp. 1455–1461, Oct. 1987.
- [18] Chen, WH., Smith, CH., and Fralick, SC., "A fast computational algorithm for the discrete cosine transform," *IEEE Trans. Commun.*, vol. 25, no. 9, pp. 1004–1009, Sep. 1977.
- [19] Spencer, Q. H., Lee, A. Swindlehurst, M. Haardt, "Zero-forcing methods for downlink spatial multiplexing in multiuser MIMO channels", *IEEE Trans. Signal Process.*, vol. 52,no. 2, Feb. 2004.
- [20] Andrews, HC., Caspari, KL., "A generalized technique for spectral analysis," IEEE Trans. Computers, vol. 19, no. 1, pp.16-17, 1970.
- [21] Reju, VG.,Koh, SN.,Soon, IY., "Convolution using discrete sine and cosine transforms", IEEE Signal Processing Letters, vol. 14, no. 7, July 2007.
- [22] Lee, MH., Khan, MHA., Sarker, MA. L., Guo, Y. and Kim, KJ., "A MIMO LTE precoding based on fast diagonal weighted Jacket matrices", *Fiber and Integrated Optics*, *Taylor and Francis*, Invited paper, vol. 31, no. 2, pp. 111-132, March 2012.
- [23] Khan, MHA., Li, J., Lee, MH., "A block diagonal Jacket matrices for MIMO broadcast channel" *IEEE International Symposium on Broadband Multimedia Systems and Broadcasting*, Brunel University, June 4-7<sup>th</sup>, 2013, UK.
# Efficient FFT-based Algorithms for Multipath Interference Mitigation in GNSS

Renbiao Wu, Qiongqiong Jia, Wenyi Wang and Jie Li

Additional information is available at the end of the chapter

http://dx.doi.org/10.5772/59940

# 1. Introduction

GNSS (Global Navigation Satellite System) has been found application in many areas. In some cases, the performance requirements for GNSS are very high. There are many error sources that would degrade the positioning performance of GNSS, e.g., clock errors, ephemeris errors, tropospheric propagation delay, and multipath. Many positioning errors mentioned above are constant for all GNSS receivers in a given small area and can be removed or reduced by using the popular differential technique. However, due to the geographical position difference between the reference station and the receiver, the multipath environment of receivers, such as amplitudes and number of multipath signals, is totally different with that of the reference station. Thus differential technique can not eliminate the multipath error. Many studies have shown that the multipath interference will lead to a position error around several meters which endangers the reliability and accuracy of GNSS. Therefore, multipath interference mitigation has been a hot topic in the field of satellite navigation receiver design.

Multipath interferences are the signals reflected by the objects around the GNSS receiver. Then the multipath interference and the LOS (line of sight) signal are simultaneously received by antenna which brings a phase distortion in the tracking loops of receivers. Finally, the phase distortion results in the tracking and positioning error.

There have been many studies about the effect of multipath interference. Kalyanaraman et al. in [1] analyzed the multipath effects on code tracking loop. Kos et al. [2] provided a detailed analysis of the multipath effects on the positioning error. Main multipath interference mitigation techniques are based on antenna technique and signal processing algorithms.



© 2015 The Author(s). Licensee InTech. This chapter is distributed under the terms of the Creative Commons Attribution License (http://creativecommons.org/licenses/by/3.0), which permits unrestricted use, distribution, and eproduction in any medium, provided the original work is properly cited.

By mounting the antenna in a well-designed place based on the multipath environment, Maqsood et al. in [3] compared the performances of multipath interference mitigation for different antennas. Ray et al. in [4] proposed a multipath mitigation algorithm based on an antenna array. A design principle of antenna was proposed by Alfred et al. in [5] for satellite navigation landing system. The multipath mitigation technique based on the special antenna can only suppress the multipath signal coming from the ground below the antenna. However, it is useless for the multipath interference signal reflected by the objects above the antenna.

Popular signal processing techniques are the narrow correlator and MEDLL (Multipath Estimated Delay Locked Loop). Narrow correlator is adopted in many GNSS receivers which suppresses multipath interference by reducing the early-late correlator spacing. The signal model for the narrow correlator is provided by Michael et al. in [6]. Cannon et al. in [7] analyzed the performance of narrow correlator in the satellite navigation system. The performance of narrow correlator can be improved by decreasing the early-late correlator spacing. However, the narrow correlator assumes that the bandwidth of the received signal is infinite which is invalid in the practical applications. Thus, when the early-late correlation spacing is less than the reciprocal of the channel bandwidth, the tracking error cannot be further decreased by reducing the early-late correlator spacing. MEDLL is a multipath interference mitigation algorithm based on the statistical theory as in [8], which estimates the time delays via the maximum likelihood criterion. Therefore, the complexity of MEDLL is much higher than narrow correlator.

This chapter firstly presents a new acquisition algorithm for GNSS. Then two multipath interference mitigation algorithms based on the DPE (Decoupled Parameter Estimation) parameter estimation algorithms are presented. The FFT algorithm is utilized to reduce the computational complexity in all proposed algorithms. Numerical results are provided to demonstrate the performances of the proposed algorithms. The remainder of this chapter is arranged as follows. Section 2 presents the new acquisition algorithm. Two multipath interference mitigation algorithms are separately presented in Section 3. Section 4 concludes the chapter.

# 2. A novel GNSS acquisition algorithm

### 2.1. Data model and problem formulation

GNSS signal is composed of three parts, the carrier, the ranging codes and the data codes. In order to facilitate the presentation, GPS is taken as an example. However, the proposed algorithm is also suitable for other GNSS system. The carrier of GPS (Global Navigation System) consists of the three different frequency bands, i.e., L1 (1575.42 MHz), L2 (1227.6 MHz) and L5 (1176.45MHz), see [9-10]. The ranging codes are pseudo random noise (PRN) codes including C/A code, P code and M code which are known in advance. Data codes or the navigation data are binary codes containing the satellite ephemeris, satellite status, clock system, the orbit perturbation correction of the satellite clock motion state and the atmospheric refraction correction, etc..

Suppose that one receiver obtained the signals from P satellites and the received data can be expressed as

$$y(t) = \sum_{p=1}^{P} \alpha_{p} d_{p} (t - \tau_{p}) c_{p} (t - \tau_{p}) e^{j \omega_{dp} (t - \tau_{p})} + e(t)$$
(1)

where  $d_p(t)$  represents the navigation data of the  $p^{th}$  satellite,  $c_p(t)$  is the C/A code of the  $p^{th}$  satellite, e(t) is the thermal noise,  $a_p$ ,  $\tau_p$  and  $\omega_{dp}$  denote the amplitude, time delay and Doppler frequency of the  $p^{th}$  satellite, respectively. It should be noted that only the L1 signal is considered in this chapter.

After A/D conversion, the data can be written as

$$y(n) = \sum_{p=1}^{P} \alpha_{p} d_{p} (n - \tau_{p}) c_{p} (n - \tau_{p}) e^{j \omega_{dp} (n - \tau_{p})} + e(n)$$
(2)

The conventional acquisition procedure is a two-dimensional searching algorithm, which is time consuming even when using parallel searching algorithm. Moreover, the frequency resolution of the conventional acquisition algorithm cannot satisfy the requirements of the tracking loop. Hence, a more accurate frequency estimation is required before tracking in the conventional receiver.

Therefore, a new GNSS acquisition algorithm is proposed in this section. The Doppler frequency is firstly estimated. After that, the initial code phase is then obtained via NLS (Nonlinear Least Square) fitting. Compared with the conventional acquisition algorithm, the proposed algorithm can obtain a comparative performance with a lower computational complexity.

### 2.2. Principle of the novel acquisition algorithm

It can be noted from the data model in section 2.1 that there are three unknown parameters in the acquisition process, which are the PRN index of the  $p^{th}$  satellite, the corresponding Doppler frequency  $\omega_{dp}$  and its initial code phase  $\tau_p$ .

### 2.2.1. Doppler frequency estimation

Due to the navigation data and C/A code are  $\pm 1$  in GPS system, it can be seen from equation (2) that the Fourier spectrum of each satellite contains multiple frequency components. Therefore, the Doppler frequency cannot be extracted from the spectrum directly. To eliminate the influence on frequency estimation brought by the navigation data and C/A code, we square equation (2) as in [11]

$$y^{2}(n) = \sum_{p=1}^{P} \alpha_{p}^{2} d_{p}^{2} (n - \tau_{p}) c_{p}^{2} (n - \tau_{p}) e^{j2\omega_{dp}(n - \tau_{p})} + 2e(n) \sum_{p=1}^{P} \alpha_{p} d_{p} (n - \tau_{p}) c_{p} (n - \tau_{p}) e^{j\omega_{dp}(n - \tau_{p})} + 2\sum_{p=1}^{P-1} \sum_{r=p+1}^{P} \alpha_{p} \alpha_{r} d_{p} (n - \tau_{p}) d_{r} (n - \tau_{r}) c_{p} (n - \tau_{p}) c_{r} (n - \tau_{r}) e^{j[\omega_{dp}(n - \tau_{p}) + \omega_{dr}(n - \tau_{r})]} + e^{2}(n)$$
(3)

Since the value of navigation data and C/A code is  $\pm 1$  in GPS system, then the above equation can be simplified as

$$y^{2}(n) = \sum_{p=1}^{p} \alpha_{p}^{2} e^{j2\omega_{dp}(n-\tau_{p})} + e_{1}(n)$$
(4)

where,

$$e_{1}(n) = 2\sum_{p=1}^{p-1} \sum_{r=p+1}^{p} \alpha_{p} \alpha_{r} d_{p}(n-\tau_{p}) d_{r}(n-\tau_{r}) c_{p}(n-\tau_{p}) c_{r}(n-\tau_{r}) e^{j[\omega_{dp}(n-\tau_{p})+\omega_{dr}(n-\tau_{r})]} + 2e(n) \sum_{p=1}^{p} \alpha_{p} d_{p}(n-\tau_{p}) c_{p}(n-\tau_{p}) e^{j\omega_{dp}(n-\tau_{p})} + e^{2}(n)$$
(5)

It can be seen from equation (4) that the spectrum of each satellite only contains a single dominant frequency component corresponding to the Doppler frequency. For the reason that not only the correlation of C/A code of different satellites is very small but also the signal and noise are uncorrelated, it is obviously that in equation (5) the product terms of different C/A codes as well as the product of noise and signal are close to zero. Fourier analysis method can be directly used to estimate the signal frequency.

The Fourier transform of equation (4) can be expressed as

$$F(\omega) = \left| \sum_{n=-N/2}^{N/2-1} y^2(n) e^{-j\omega n} \right|$$
(6)

where  $\omega = 2\omega_{dp}$  can be obtained based on the locations of the first *p* dominant peaks of *F*( $\omega$ ). A more accurate estimation result can be achieved by using FFT (Fast Fourier Transform) padding with zeros.

The estimated value of  $\hat{\omega}$  is in the range of  $[-\pi, \pi]$ , thus from equation (6) we know that the estimated value of  $\hat{\omega}_{dp}$   $[-\pi/2, \pi/2]$ . As  $\omega_{dp}$   $[-\pi, \pi]$ , the estimated frequency could be  $\hat{\omega}_{dp}$  or  $\hat{\omega}_{dp} + \pi$ . Therefore, the frequency ambiguity will lead to a mistake. Due to the IF (Intermediate Frequency) of the satellite signals is definitely known after down conversion and the range of Doppler shift is between ±10kHz [12], the difference between true frequency and the ambiguity



Figure 1. Frequency spectrum before and after square operation

one is generally greater than the Doppler shift. Therefore, ambiguity frequency can be excluded by determining whether the frequency is in the range of the Doppler shift.

The frequency spectrum of the received data before and after the square operation is shown in Figure 1. It can be noted that before square operation, there are multiple dominant frequency components. Thus the Doppler frequency cannot be extracted directly. However, after being squared, there is only one dominant Doppler frequency present in the spectrum, so an accurate Doppler frequency can be estimated.

### 2.2.2. Code phase estimation and matching

After obtaining the Doppler frequency, the initial phases and the PRN index of the C/A code from all satellites can be estimated by using its autocorrelation characteristic. Let  $s_p(n)=d_p(n)c_p(n)e^{j\omega_{dp}n}$ , then equation (2) can be expressed as

$$y(n) = \sum_{p=1}^{p} \alpha_{p} s_{p}(n - \tau_{p}) + e(n)$$
(7)

As the Doppler frequency  $\hat{\omega}_{dq}$  has been estimated,  $\hat{\omega}_{dq}$  can be used to take the place of  $\omega_{dq}$ . Then the signal sent by the  $q^{th}$  satellite can be reconstructed as

$$\hat{s}_q(n) = d_q(n)c_q(n)e^{j\hat{\omega}_{dq}n}$$
(8)

Suppose the time delay from the  $q^{th}$  satellite to the receiver is  $\tau_{q'}$  then the received signal can be written as

$$y_q(n) = \alpha_q \hat{s}_q(n - \tau_q) + e_2(n)$$
 (9)

where  $e_2(n) = \sum_{\substack{p=1 \ p \neq q}}^{p} \alpha_p s_p(n-\tau_p) + \alpha_q s(n-\tau_q) - \alpha_q \hat{s}(n-\tau_q) + e(n)$ . The DFT (Discrete Fourier Transform) of

equation (9) can be written as

$$y_{f}(k) = \alpha_{q} \hat{s}_{fq}(k) e^{j\omega_{q}k} + e_{f2}(k)$$
(10)

where  $y_f(k)$ ,  $\hat{s}_{fq}(k)$  and  $e_{f2}(k)$  are the DFT of y(n),  $\hat{s}_q(n)$  and  $e_2(n)$  respectively,  $\omega_q = -2\pi\tau_q f_s / N$  with  $f_s$  is the sampling frequency. Note, here  $x_f$  is used to represent the DFT of x. Hence, the estimation of  $\tau_q$  is transformed to the estimation of  $\omega_q$ .

To estimate  $\omega_{q'}$  we define the following NLS cost function [12-15]

$$z_{f}(\hat{\omega}_{q}) = \sum_{k=-N/2}^{N/2-1} \left| y_{f}(k) - \hat{s}_{jq}(k) \alpha_{q} e^{j\omega_{q}k} \right|^{2}$$
(11)

Let

$$\hat{\mathbf{S}}_{fq} = diag \left\{ \hat{s}_{fq} \left( -N / 2 \right), \hat{s}_{fq} \left( -N / 2 + 1 \right), \dots, \hat{s}_{fq} \left( N / 2 - 1 \right) \right\}$$
(12)

$$\mathbf{a}(\omega_q) = \left[ e^{j\omega_q(-N/2)}, e^{j\omega_q(-N/2+1)}, ..., e^{j\omega_q(N/2-1)} \right]^T$$
(13)

$$\mathbf{y}_{f} = \left[ y_{f}(-N/2), y_{f}(-N/2+1), ..., y_{f}(N/2-1) \right]^{T}$$
(14)

where  $()^{T}$  denotes the transpose operation. Then the cost function in equation (11) can be transformed as

$$Z(\hat{\omega}_q) = \left\| \mathbf{y}_f - \alpha_q \hat{\mathbf{S}}_{fq} \mathbf{a}(\omega_q) \right\|^2$$
(15)

where  $\| \|$  denotes the Euclidean norm. Minimizing  $Z(\hat{\omega}_q)$  with respect to  $\omega_q$  yields the estimated  $\hat{\omega}_q$  as

$$\hat{\omega}_{q} = \arg \max_{\omega_{q}} \left| \mathbf{a}^{H}(\omega_{q}) \hat{\mathbf{S}}_{fq}^{H} \mathbf{y}_{f} \right|^{2}$$
(16)

The time delay estimation can be further obtained by

$$\hat{\tau}_q = -\hat{\omega}_q N / (2\pi f_s) \tag{17}$$

Equation (16) can be solved by using FFT algorithm with a low computation burden. Since the PRN index of the received signal is unknown, consequently, it is not feasible to reconstruct  $\hat{s}_q(n)$  directly by equation (8). Therefore, we should reconstruct signal of each satellite with the estimated Doppler frequency  $\hat{\omega}_q$ . Then the cross correlation of the reconstructed signal and the received one can be calculated. Furthermore, the corresponding time delay can be estimated from equation (16).

It is well-known that the cross correlation coefficients of different C/A codes are very small. In addition, the signal and noise are uncorrelated. Thus Fourier analysis results of the above mentioned component are close to zero. The maximum correlation value can only be obtained in the case that the C/A code of the reconstructed signal is the same as the received one. Therefore, the PRN index can be obtained. Furthermore, the code delay can be estimated by the location of the maximum correlation value. Then, we obtained all the unknown parameters.

### 2.3. Comparison of acquisition algorithms

Suppose the searching time for Doppler frequency estimation is Q in the conventional acquisition algorithm, P is the number of satellite received by the receiver. In GPS, the typical values of Q and P are 21 and 4-8, respectively, as in [9, 11]. The total number of satellites M is 32. Since Doppler frequency and code delay are unknown in the conventional acquisition algorithm, Q frequency points should be searched over certain frequency range. What's more, M satellites are also to be searched for each of the Q frequency points. While in the proposed algorithm, the Doppler frequencies of P satellites have been estimated, only P accurate frequencies need to be searched.

Figure 2 compares the searching process of the proposed algorithm and the conventional one. It can be seen that the computation complexity of the proposed algorithm is significantly lower than that of the conventional algorithm in that the typical value of *Q* is obviously greater than *P*.

Comparison of computation burden between new acquisition algorithm and conventional acquisition algorithm are shown Table 1. It can be clearly seen from Table 1 that, since Q is



Figure 2. Comparison of searching process between new algorithm and conventional algorithm

always greater than *P*, the computation complexity of the proposed algorithm is lower than the conventional acquisition procedure. In practices, only 4 satellites are enough to determine the user position, which is less than 8, hence the computation burden should be further decreased. As the number of satellite is equal to 4, only half of the original computation complexity is required.

	Multiplication times	Addition times	FFT times	Time Complexity
conventional method	7MQ+4M	2MQ+3M	2MQ	O(MQ)
new method	6MP+4P	3MP+7P	M (P+1) +1	O(MP)

Table 1. Comparison of computation burden between new algorithm and conventional one

#### 2.4. Numerical results

To verify the performance of the proposed algorithm, GPS signals from 8 satellites with PRN indexes 1, 2, 13, 20, 22, 24, 25 and 27 are simulated. Considering the IF is 1.25MHz, the sampling rate is 7.5MHz, the pre integration time is 1ms and the signal to noise ratio (SNR) is -20dB. The frequency searching step of the conventional acquisition algorithm is 1kHz. The acquisition results are shown in Figure 3.



(b) proposed acquisition algorithm



In Figure 3, the horizontal axis stands for the PRN index of the satellites and the vertical axis denotes the acquisition metric. Since the proposed algorithm only calculates the correlation of the received satellite signal and the local reference signal, correlation results of the other satellite are not shown in Figure 3(b). It can be noted that acquisition results are identical, and the peak value of the proposed algorithm is higher than the conventional one. Therefore, the proposed algorithm has a comparative performance with the conventional one.

### 3. Two novel methods for multipath mitigation

#### 3.1. Multipath data model

The term multipath is derived from the fact that a signal transmitted from a GNSS satellite can follow a 'multiple' number of propagation 'paths' to the receiving antenna. This is possible because the signal can be reflected back to the antenna from surrounding objects, including the earth's surface.

Suppose the signal transmitted by GNSS satellites can be written as

$$x(t) = d(t)c(t)e^{j\omega_c t}$$
(18)

where d(t) is the navigation data, c(t) is the C/A code in GPS. Here, we take the two path signal model as an example, which can be generalized to multiple reflection path signals directly. The received signal including the LOS signal with a single reflection can be written as

$$\overline{y}(t) = \sum_{p=1}^{2} \alpha'_{p} d(t - \tau_{p}) c(t - \tau_{p}) e^{j\omega_{c}(t - \tau_{p})} + e(t)$$
(19)

where  $\alpha_1'$ ,  $\tau_1$  is amplitude and code delay of the LOS signal,  $\alpha_2'$ ,  $\tau_2$  is amplitude and code delay of the reflect signal, e(t) is the thermal noise. Equation (19) can also be deployed as

$$\overline{y}(t) = \sum_{p=1}^{2} \alpha'_{p} d(t - \tau_{p}) c(t - \tau_{p}) e^{j\omega_{c}(t - \tau_{p})} + e(t)$$

$$= \left( \alpha'_{1} d(t - \tau_{1}) c(t - \tau_{1}) e^{-j\omega_{c}\tau_{1}} + \alpha'_{2} d(t - \tau_{2}) c(t - \tau_{2}) e^{-j\omega_{c}\tau_{2}} \right) e^{j\omega_{c}t} + e(t)$$
(20)

To obtain the Doppler frequency of the LOS signal, we use the following relation

$$\phi = \omega_c \tau_1 = \omega_c \frac{R_1(t)}{c} \tag{21}$$

Assume the radial velocity of the receiver relative to the satellite is  $v_1$ , then the range between them can be given by

$$R_{1}(t) = R_{0} + v_{1}t$$
(22)

where  $\mathbf{R}_0$  is the initial range between receiver and satellite, then equation (21) can be further given by

$$\phi = \omega_c \tau_1 = \omega_c \frac{R_0 + v_1 t}{c} = 2\pi \left(\frac{R_0}{\lambda} + \frac{v_1 t}{\lambda}\right)$$
(23)

As the relative radial velocity is constant, the Doppler frequency can be obtained by

$$\omega_{d1} = \frac{d\phi}{dt} = \frac{v_1}{\lambda} \tag{24}$$

The propagation range of the multipath signal can be written as

$$R_2(t) = R_0 + v_1 t + \Delta R(t) \tag{25}$$

where  $\Delta \mathbf{R}(t)$  is the propagation range difference between the LOS signal and the reflected one. Since satellites are far away from the receiver, the range difference  $\Delta \mathbf{R}(t)$  can be considered as constant in the short integration time. Then equation (21) can be represented as

$$\omega_c \tau_p = \omega_c \frac{R_0 + v_1 t}{c} = 2\pi \left( \frac{R_0}{\lambda} + \frac{v_1 t}{\lambda} + \frac{\Delta R}{\lambda} \right)$$
(26)

Further simplify of equation (20) we can get

$$\overline{y}(t) = \left(\alpha_1'd\left(t-\tau_1\right)c\left(t-\tau_1\right)e^{-j\varphi_1} + \alpha_2'd\left(t-\tau_2\right)c\left(t-\tau_2\right)e^{-j\left(\varphi_1+\Delta\varphi\right)}\right)e^{j2\pi\omega_d't} + e(t)$$
(27)

where  $\omega'_{d} = \omega_{d1} + \omega_{c}$  is the Doppler frequency of the received signal,  $\varphi_{1} = \mathbf{R}_{0}/\lambda$  and  $\varphi_{2} = \varphi_{1} + \Delta \varphi$  are the phase of the LOS signal and the reflect one respectively, with  $\Delta \varphi$  an extra phase caused by the extra propagation range  $\Delta \mathbf{R}$ . Accordingly, the LOS signal and reflect signal share the same Doppler shift.

After A/D conversion, the transformed digital signal can be written as

$$\overline{y}(n) = \sum_{p=1}^{2} \alpha'_{p} d(n - \tau_{p}) c(n - \tau_{p}) e^{-j\varphi_{p}} e^{j\omega'_{d}n} + e(n)$$
(28)

Assume the Doppler frequency has been estimated accurately, then the complex phase  $e^{j\omega'_d n}$  can be compensated after down-conversion. Hence, equation (28) can be written as

$$y(n) = \sum_{p=1}^{2} \alpha'_{p} d(n - \tau_{p}) c(n - \tau_{p}) e^{-j\varphi_{p}} + \mathscr{U}(n)$$
(29)

where  $\tilde{e}(n)$  is equal to  $e(n)e^{-j\omega'_{d}n}$  that share the same statistics characteristic with e(n). So we still use e(n) to represent the noise data.

The in-phase component of equation (29) can be given by

$$y_{1}(n) = \sum_{p=1}^{2} \alpha'_{p} d(n - \tau_{p}) c(n - \tau_{p}) \cos(\varphi_{p} - \varphi_{c}) + e(n)$$
(30)

where  $\varphi_c$  is the synthetic phase of the LOS signal and the reflect one. Assume *d* is the early-late correlator spacing in the classical DLL, the estimated code delay of the direct signal is  $\hat{\tau}_1$ . Then the early and late code can be written as

$$s_E(t) = y_I(t - \hat{\tau}_1 - d/2)$$
(31)

$$s_L(t) = y_I(t - \hat{\tau}_1 + d/2)$$
(32)

In classical DLL, the in-phase early and late correlation value is given as

$$R_{E}(\varepsilon) = \sum_{p=1}^{2} \alpha_{p} R(\varepsilon + \Delta \tau_{p} - d/2) \cos(\varphi_{p} - \varphi_{c})$$
(33)

$$R_{L}(\varepsilon) = \sum_{p=1}^{2} \alpha_{p} R(\varepsilon + \Delta \tau_{p} + d/2) \cos(\varphi_{p} - \varphi_{c})$$
(34)

where  $\varepsilon = \tau_1 - \hat{\tau}_1$  is the estimation error of the LOS signal, namely tracking error.  $\Delta \tau = \tau_2 - \tau_1$  is the relative delay of the multipath signal to the LOS. The discrimination function of the classical DLL (Delay Locked Loop) can be written as



Figure 4. Correlation peak when multipath is present

$$D(\varepsilon) = R_{\varepsilon}(\varepsilon) - R_{L}(\varepsilon)$$
  
=  $\sum_{p=1}^{2} \alpha_{p} \Big[ R(\varepsilon + \Delta \tau_{p} - d/2) - R(\varepsilon + \Delta \tau_{p} + d/2) \Big] \cos(\varphi_{p} - \varphi_{c})$  (35)

In GNSS navigation, the receiver is concerned to maximize the correlation function between the received and locally generated signals. This can be accomplished by determining the locations of the zero output of the discriminator which corresponds to the maximum of the correlation function. Here, the early-late correlator is used to determine the position of this zero. However, the presence of multipath introduces some bias in the position of the first arrival peak and has an impact in the user's position, which can be clearly seen in Figure 4. Then the classical DLL failed to cope with multipath propagation, see [7-8].

#### 3.2. Code delay estimation

#### 3.2.1. Code delay estimation in the correlation domain via NLS

In this subsection, a code delay estimation algorithm based on DPE in correlation domain is proposed. To deploy the proposed algorithm, we combine the complex constant phase  $e^{-j\varphi_p}$  and the real amplitude  $\alpha'_p$  in equation (29) together as a new complex variable  $\alpha''_p$ . Then equation (29) can be written as

$$y(n) = \sum_{p=1}^{2} \alpha_{p}'' d(n - \tau_{p}) c(n - \tau_{p}) + e(n)$$
(36)

The navigation data cycle is much longer than that of the C/A code, but only one cycle of the C/A code is used in the code delay estimation. Consequently, the navigation data jump can be neglected in the signal reconstruction. Then the navigation data +1 or -1 is written into  $\alpha_{p}^{"}$  and denoted as  $\alpha_{p}$ . Therefore equation (36) can be written as

$$y(n) = \sum_{p=1}^{2} \alpha_{p} c(n - \tau_{p}) + e(n)$$
(37)

To simplify the following expression, s() is introduced to represent c(). Then equation (37) can be represented as

$$y(n) = \sum_{p=1}^{2} \alpha_{p} s(n - \tau_{p}) + e(n)$$
(38)

Multipath interference mitigation based on code delay estimation focus on the estimation of the LOS delay  $\tau_1$  and the reflect delay  $\tau_2$ , where the estimated result can be used to migrate the multipath. After acquisition, the correlation between the received satellite signal and the local reference signal is used to estimate the parameter of both the LOS signal and the reflected one. The proposed code delay estimation algorithm can take the place of the classical DLL, which can be described in details as follows.

To obtain the initial code delay, the correlation function between the received satellite signal and the reference signal is represented as

$$r(n) = \operatorname{corr}(s(n), y(n))$$
(39)

where corr() represents the cross correlation operation. Since the noise is uncorrelated with the signal, equation (39) can be further expressed as

$$r(n) = \sum_{p=1}^{2} \alpha_{p} r^{s} (n - \tau_{p}) + w(n)$$
(40)

where  $r^{s}(n)$  is the autocorrelation of s(n), w(n) = corr(s(n), e(n)) can still be thought as noise that sharing the same statistic characteristics with e(n). Apply DFT to equation (40)

Efficient FFT-based Algorithms for Multipath Interference Mitigation in GNSS 39 http://dx.doi.org/10.5772/59940

$$p_f(k) = r_f^s(k) \sum_{p=1}^2 \alpha_p e^{j\omega_p k} + w_f(k)$$
(41)

where  $p_f(k)$ ,  $r_f^s(k)$ ,  $w_f(k)$  are the DFT of p(n),  $r^s(n)$  and w(n) respectively,  $\omega_p = -2\pi\tau_p / NT_s$  with  $T_s$  is the sampling interval.

Define a NLS cost function as

$$C_{1}\left(\left\{\omega_{p},\alpha_{p}\right\}_{p=1}^{2}\right) = \sum_{k=-N/2}^{N/2} \left\|p_{f}(k) - r_{f}^{s}(k)\sum_{p=1}^{2}\alpha_{p}e^{j\omega_{p}k}\right\|^{2}$$
(42)

The unknown parameters  $\{\omega_p, a_p\}_{p=1}^2$  can be obtained by minimizing the cost function  $C_1(\{\omega_p, \alpha_p\}_{p=1}^2)$ . Whereas, searching over a multidimensional space to solve the NLS problem requires higher computational complexity. To reduce the complexity, the Weighted Fourier Transform and RELAXation (WRELAX) algorithm (see [12]) is utilized here to solve the NLS problem. Let

$$\mathbf{a}(\omega_{p}) = \left[e^{j\omega_{p}(-N/2)}, e^{j\omega_{p}(-N/2+1)}, ..., e^{j\omega_{p}(N/2-1)}\right]^{\mathrm{T}}$$
(43)

$$\mathbf{p}_{f} = \left[ p_{f}(-N/2), p_{f}(-N/2+1), ..., p_{f}(N/2-1) \right]^{\mathrm{T}}$$
(44)

$$\mathbf{R}_{f} = diag\left\{r_{f}^{s}(-N/2), r_{f}^{s}(-N/2+1), ..., r_{f}^{s}(N/2-1)\right\}$$
(45)

Consequently the cost function in equation (42) can be rewritten as

$$C_{1}(\{\boldsymbol{\omega}_{p},\boldsymbol{\alpha}_{p}\}_{p=1}^{2}) = \left\|\mathbf{p}_{f} - \sum_{p=1}^{2} \boldsymbol{\alpha}_{p} \mathbf{R}_{f} \mathbf{a}(\boldsymbol{\omega}_{p})\right\|^{2}$$
(46)

Further, we assume  $\{\hat{\omega}_q, \hat{\alpha}_q\}_{q=1,q\neq p}^2$  have been estimated, then

$$\mathbf{p}_{fp} = \mathbf{p}_f - \sum_{\substack{q=1\\ q \neq p}}^2 \hat{\alpha}_q [\mathbf{R}_f \mathbf{a}(\hat{\omega}_p)]$$
(47)

Substitute equation (47) into equation (46) we have

$$C_2(\{\omega_p, \alpha_p\}_{p=1}^2) = \left\| \mathbf{p}_{fp} - \alpha_p \mathbf{R}_f \mathbf{a}(\omega_p) \right\|^2$$
(48)

By minimizing the cost function  $C_{2'}$  estimation of  $\hat{\omega}_p$  and  $\hat{\alpha}_p$  can be obtained from

$$\hat{\omega}_{p} = \arg \max_{\omega_{p}} \left| \mathbf{a}^{\mathrm{H}}(\omega_{p}) \left( \mathbf{R}_{f}^{*} \mathbf{p}_{fp} \right) \right|^{2}$$
(49)

and

$$\hat{\alpha}_{p} = \frac{\mathbf{a}^{\mathrm{H}}(\omega_{p}) \left(\mathbf{R}_{f}^{*} \mathbf{p}_{fp}\right)}{\left\|\mathbf{R}_{f}\right\|_{F}^{2}} \bigg|_{\omega_{p} = \hat{\omega}_{p}}$$
(50)

where  $\| \|_{F}$  represents the Frobenius norm. Hence,  $\hat{\omega}_{p}$  can be obtained as the location of the periodogram  $|\mathbf{a}^{H}(\omega_{p})(\mathbf{R}_{f}\mathbf{p}_{fp})|^{2}$ , which can be efficiently computed by using FFT to the data sequence  $\mathbf{R}_{f}\mathbf{p}_{fp}$  padded with zeros. (Note the padding with zeros is necessary to determine  $\hat{\omega}_{p}$  with more accuracy.) Then  $\hat{a}_{p}$  is easily computed from the complex height of the peak of  $\frac{\mathbf{a}^{H}(\hat{\omega}_{p})(\mathbf{R}_{f}\mathbf{p}_{fp})}{\|\mathbf{R}_{f}\|_{F}^{2}}$ .

With the above simple preparations, we now proceed to present the correlation domain algorithm for the minimization of the NLS cost function. The proposed algorithm comprises the following steps.

Step 1. Assume p=1. Obtain  $\{\hat{\alpha}_1, \hat{\alpha}_1\}$  from equation (49) and equation (50).

Step 2. Assume p=2 (the LOS signal and one reflected path). Compute  $\mathbf{p}_{f2}$  with (47) by using  $\{\hat{\omega}_1, \hat{\alpha}_1\}$  obtained in Step (1). Obtain  $\{\hat{\omega}_2, \hat{\alpha}_2\}$  from  $\mathbf{p}_{f2}$  described above.

Next, compute  $\mathbf{p}_{f1}$  with (47) by using  $\{\hat{\omega}_2, \hat{\alpha}_2\}$  and redetermine  $\{\hat{\omega}_1, \hat{\alpha}_1\}$  from  $\mathbf{p}_{f1}$  as in equation (49) and equation (50) above.

Iterate the previous two substeps until "practical convergence" is achieved then we can obtain  $\{\hat{\omega}_p, \hat{\alpha}_p\}_{p=1}^2$ . Furthermore, by using  $\hat{\omega}_p = -2\pi \hat{\tau}_p / NT_s$  the code delay  $\hat{\tau}_p$ , p=1, 2 can be obtained.

From the previous description one can find that the proposed algorithm can be implemented by simply FFT operation which leads to a less computation load.

The diagram of the novel code delay estimation algorithm is shown in Figure 5.

Efficient FFT-based Algorithms for Multipath Interference Mitigation in GNSS 41 http://dx.doi.org/10.5772/59940



Figure 5. Diagram of the correlation domain code delay estimation algorithm

#### 3.2.2. Code delay estimation in the data domain via NLS

Another DPE algorithm is proposed in this subsection. Different from the correlation domain algorithm, the unknown parameters  $\{\alpha_p, \tau_p\}_{p=1}^2$  can also be estimated directly in the data domain, which can be described as follows.

Again, the signal after down-conversion is given by

$$y(n) = \sum_{p=1}^{2} \alpha_{p} s(n - \tau_{p}) + e(n)$$
(51)

To obtain the unknown parameters  $\{\alpha_p, \tau_p\}_{p=1}^2$  in equation (51), DFT is applied firstly

$$y_f(k) = s_f(k) \sum_{p=1}^{2} \alpha_p e^{j\omega_p k} + e_f(k), -N / 2 \le k \le N / 2 - 1$$
(52)

where  $y_f(k)$ ,  $s_f(k)$ ,  $e_f(k)$  are the DFT of y(n), s(n) and e(n) respectively.  $\omega_p = -2\pi\tau_p f_s/N$  with  $f_s$  represents the sampling frequency. Till now, the code delay estimation is transformed to the angular frequency  $\omega_p$  estimation, after which  $\tau_p$  can be obtained by the relation  $\tau_p = -\omega_p N/2\pi f_s$ .

To obtain  $(\hat{a}_{p}, \hat{\omega}_{p})$ , a NLS cost function as follows is defined

$$Q_{1}\left(\left\{\alpha_{p},\omega_{p}\right\}_{p=1}^{2}\right) = \sum_{k=-N/2}^{N/2-1} \left|y_{f}(k) - s_{f}(k)\sum_{p=1}^{2}\alpha_{p}e^{j\omega_{p}k}\right|^{2}$$
(53)

Let

$$\mathbf{S}_{f} = diag \left\{ s_{f}(-N/2), s_{f}(-N/2+1), \dots, s_{f}(N/2-1) \right\}$$
(54)

$$\mathbf{y}_{f} = \left[ y_{f}(-N/2), y_{f}(-N/2+1), \dots y_{f}(N/2-1) \right]^{T}$$
(55)

$$\mathbf{a}(\omega_{p}) = \left[e^{j\omega_{p}(-N/2)}, e^{j\omega_{p}(-N/2+1)}, ..., e^{j\omega_{p}(N/2-1)}\right]^{T}$$
(56)

Hence, minimizing the cost function in equation (53) is equivalent to minimizing the following cost function

$$Q_{2}\left(\left\{\boldsymbol{\alpha}_{p},\boldsymbol{\omega}_{p}\right\}_{p=1}^{2}\right) = \left\|\mathbf{y}_{f} - \sum_{p=1}^{2} \boldsymbol{\alpha}_{p} \mathbf{S}_{f} \mathbf{a}\left(\boldsymbol{\omega}_{p}\right)\right\|^{2}$$
(57)

Assume  $\{\hat{\alpha}_q, \hat{\omega}_q\}_{q=1,q\neq p}^2$  is known prior or has been estimated, then we have

$$\mathbf{y}_{fp} = \mathbf{y}_f - \sum_{\substack{q=1\\q\neq p}}^2 \hat{\alpha}_q \Big[ \mathbf{S}_f \mathbf{a} \big( \hat{\omega}_p \big) \Big]$$
(58)

Substitute equation (58) into equation (57)

$$Q_2(\alpha_p, \omega_p) = \left\| \mathbf{y}_{fp} - \alpha_p \mathbf{S}_f \mathbf{a}(\omega_p) \right\|^2$$
(59)

Equation (59) gets the minimum while  $\mathbf{y}_{fp} = \alpha_p \mathbf{S}_f \mathbf{a}(\omega_p)$ , then the estimation results  $\hat{\omega}_p$  and  $\hat{\alpha}_p$  can be obtained in the following way

$$\hat{\omega}_{p} = \arg \max_{\omega_{p}} \left| \mathbf{a}^{\mathrm{H}}(\omega_{p}) \left( \mathbf{S}_{f}^{*} \mathbf{y}_{fp} \right) \right|^{2}$$
(60)

$$\hat{\alpha}_{p} = \frac{\mathbf{a}^{\mathrm{H}}(\omega_{p})(\mathbf{S}_{f}^{*}\mathbf{y}_{fp})}{\left\|\mathbf{S}_{f}\right\|_{F}^{2}} \bigg|_{\omega_{p}=\hat{\omega}_{p}}$$
(61)

From equation (60),  $\hat{\omega}_p$  can be obtained as the location of the periodogram  $|\mathbf{a}^H(\omega)(\mathbf{S}_f^*\mathbf{y}_{fp})|^2$ , which can be efficiently computed by using the FFT with the data sequence  $\mathbf{S}_f^*\mathbf{y}_{fp}$  padded with zeros. (Note the padding with zeros is necessary to determine  $\hat{\omega}_p$  with more accuracy.) Then  $\hat{\alpha}_p$  is easily computed from the complex height of the peak of  $\frac{\mathbf{a}^H(\omega_p)(\mathbf{S}_f^*\mathbf{y}_{fp})}{\|\mathbf{S}_f\|_F^2}$ .

The diagram of the data domain code delay estimation algorithm is shown as in Figure 6.



Figure 6. Diagram of the data domain code delay estimation algorithm

With the above simple preparations, we now proceed to present the relaxation algorithm for the minimization of the nonlinear least-squares cost function. The data domain WRELAX algorithm comprises the following steps.

Step 1. Assume p=1. Obtain  $\{\hat{\omega}_1, \hat{\alpha}_1\}$  from equation (61) and equation (60).

Step 2. Assume p=2 (the LOS signal and one reflected path). Compute  $y_{f2}$  with (47) by using  $\{\hat{\omega}_1, \hat{\alpha}_1\}$  obtained in Step (1). Obtain  $\{\hat{\omega}_2, \hat{\alpha}_2\}$  from  $y_{f2}$  described above.

Next, compute  $y_{f1}$  with equation (47) by using  $\{\hat{\omega}_2, \hat{\alpha}_2\}$  and redetermine  $\{\hat{\omega}_1, \hat{\alpha}_1\}$  from  $y_{f1}$  as in equation (49) and equation (50) above.

Iterate the previous two substeps until "practical convergence" is achieved then we can obtain  $\{\hat{\omega}_p, \hat{\alpha}_p\}_{p=1}^2$ . Furthermore, by using  $\hat{\omega}_p = -2\pi \hat{\tau}_p / NT_s$  the code delay  $\hat{\tau}_p$ , p=1, 2 can be obtained.

From the previous description one can find that the proposed algorithm can be implemented by simply FFT operation which deserves a less computation load.

#### 3.2.3. Comparison of the above two algorithms

To further analyze the two proposed algorithms, the cost functions of them are further discussed in this subsection. Following the discussion in section 3.2.1 and section 3.2.2, we define

$$\mathbf{s}_{f} = \left[ s_{f} \left( -N/2 \right), s_{f} \left( -N/2 + 1 \right), \dots, s_{f} \left( N/2 - 1 \right) \right]^{\mathrm{T}}$$
(62)

Then

$$\mathbf{R}_f = \mathbf{s}_f \mathbf{s}_f^{\mathrm{H}} \tag{63}$$

In the noise free situation we have

$$\mathbf{p}_{fp} = \alpha_p \mathbf{R}_f \mathbf{a}(\omega_p) \tag{64}$$

Then the correlation domain cost function in equation (49) can be further decomposed as

$$\hat{\omega}_{p} = \arg \max_{\omega_{p}} \left| \mathbf{a}^{\mathrm{H}}(\omega_{p}) \mathbf{R}_{fs}^{*} \mathbf{p}_{fp} \right|^{2}$$

$$= \arg \max_{\omega_{p}} \left| \mathbf{a}^{\mathrm{H}}(\omega_{p}) \mathbf{R}_{fs}^{*} \left( \alpha_{p} \mathbf{R}_{fs} \mathbf{a}(\omega_{p}) \right) \right|^{2}$$

$$= \arg \max_{\omega_{p}} \left| \mathbf{a}^{\mathrm{H}}(\omega_{p}) \left( \mathbf{s}_{f} \times \mathbf{s}_{f}^{\mathrm{H}} \right)^{*} \left( \alpha_{p} \left( \mathbf{s}_{f} \times \mathbf{s}_{f}^{\mathrm{H}} \right) \mathbf{a}(\omega_{p}) \right) \right|^{2}$$

$$= \arg \max_{\omega_{p}} \left| \mathbf{a}^{\mathrm{H}}(\omega_{p}) \left[ \left( \mathbf{s}_{f}^{\mathrm{T}} \times \mathbf{s}_{f}^{*} \right) \times \left( \mathbf{s}_{f} \times \mathbf{s}_{f}^{\mathrm{H}} \right) \right] \left( \alpha_{p} \mathbf{a}(\omega_{p}) \right) \right|^{2}$$
(65)

And in the same situation the data domain cost function in equation (60) can be deployed in the following way

$$\hat{\omega}_{p} = \arg \max_{\omega_{p}} \left| \mathbf{a}^{\mathrm{H}}(\omega_{p}) \mathbf{S}_{f}^{*} \mathbf{y}_{fp} \right|^{2}$$

$$= \arg \max_{\omega_{p}} \left| \mathbf{a}^{\mathrm{H}}(\omega_{p}) \mathbf{S}_{f}^{*}(\alpha_{p} \mathbf{S}_{f} \mathbf{a}(\omega_{p})) \right|^{2}$$

$$= \arg \max_{\omega_{p}} \left| \mathbf{a}^{\mathrm{H}}(\omega_{p}) (\mathbf{s}_{f}^{*} \mathbf{s}_{f}^{\mathrm{T}}) (\alpha_{p} \mathbf{a}(\omega_{p})) \right|^{2}$$
(66)

It has been discussed in previous subsection that  $\hat{\omega}_p$  can be obtained by using the FFT with the data sequence  $\mathbf{R}_f \mathbf{p}_{fp}$  and  $\mathbf{S}_f {}^H \mathbf{y}_{fp'}$ , respectively. Note  $(a_p \mathbf{a}(\omega_p))$  is an impulse signal, and FFT $(\mathbf{s}_f^* \mathbf{s}_f^T)$  convolutions with the impulse signal is still FFT $(\mathbf{s}_f^* \mathbf{s}_f^T)$  but with a code delay, which is the parameter to be estimated. From equation (65) and (66) we realized that the cost function are the FFT of  $a_p \mathbf{a}(\omega_p)$  weighted by different window function, where window function in the correlation domain is  $w_1 = \text{FFT}((\mathbf{s}_f^T \mathbf{s}_f^T))$ , but the window function in data domain is  $w_2 = \text{FFT}(\mathbf{s}_f^* \mathbf{s}_f^T)$ . It's clear that the weighted window  $w_1$ ,  $w_2$  will broaden the cost function, and the impact of  $w_1$  is more serious than that of  $w_2$ , which can also be seen from the comparison of the cost function given in Figure 7. From this point of view, the proposed data domain algorithm would deserve a more accurate estimation result.



Figure 7. Comparison of the correlation domain and the data domain cost function

Correlation of the received data and the locally generated signal and the auto-correlation of the locally generated signal should be calculated in correlation domain WRELAX algorithm.

Suppose the iteration times of the two proposed algorithms are the same, the correlation domain WRELAX algorithm is more complex than the data domain WRELAX algorithm.

#### 3.2.4. Numerical results

To investigate the performance of the proposed algorithm in the presence of multipath, a simulation experiment was performed. The code delay estimation error can be represented as the function of  $\tau$ , and as explained in [I] and [7], maximum and minimum errors occur when the multipath signal is in-phase  $\Delta \varphi = 0$  °or out-of-phase  $\Delta \varphi = \pm 180$  °with the LOS signal. The curve of the maximum and minimum errors is regarded as the error envelopes, which is used in the following numerical experiment to evaluate the performance.



(b). details of (a)

Figure 8. Comparison of the error envelopes

Suppose there is only one reflected multipath signal combined with the LOS signal. The noise and the receiver bandwidth are not considered in the experiment. The relative amplitude of the direct and the reflected signal is  $\alpha_2/\alpha_1=0.5$ . The code delay difference  $\Delta \tau = \tau_2 - \tau_1$  is varied from 0 to 1.5 chips. The error is calculated at the maximum points when the multipath signal is at 0° in phase with respect to the LOS signal. The results are shown in Figure 8(a).

In Figure 8, the curve 'classical DLL' denotes the error envelope of the classical DLL, and the curve 'narrow correlator' denotes the error envelope of the narrow correlator with spacing d=0.1 chip. Both the 'classical DLL' and the 'narrow correlator' were calculated by taking the DLL equations and solving for the tracking error. The curve 'MEDLL', 'Correlation Domain' and 'Data Domain' denote the code delay estimation error of MEDLL, proposed correlation domain algorithm and data domain algorithm, respectively. The results indicate that in the presence of multipath, the classical DLL technique has a large tracking error, which fails in multipath mitigation. The tracking error is reduced in the narrow correlator. However, based on the previous conclusion, the tracking error is nearly constant when the correlation spacing is less than 0.1 chip. The tracking accuracy of the algorithms in this section and MEDLL show a considerable improvement over the narrow correlator technique and the classical DLL technique. The improved performance can be of great help in critical GPS applications where the multipath errors associated with using conventional receivers can easily exceed the accuracy requirements. To further compare the performance of the two proposed algorithms and MEDLL, we magnify the results in Figure 8(a) to obtain Figure 8(b). It is clear that the proposed two algorithms have a more favorable performance than MEDLL. Furthermore, the proposed data domain algorithm is superior to the correlation domain algorithm, which is consistent with the conclusion in section 3.2.3.

# 4. Conclusion

A novel acquisition algorithm is firstly proposed in this chapter. In the proposed algorithm, the Doppler frequency is obtained by utilizing FFT of the squared data. Then, the PRN index and initial code phases of the satellite are obtained based on the NLS criterion. It can be seen that the proposed algorithm can not only reduce the computation complexity but also attain a comparable performance to the conventional acquisition algorithm.

After that, two algorithms are presented to suppress the multipath interference by estimating the code delay. In the proposed algorithms, the code delay was obtained by solving a NLS equation, which can be further realized by FFT operation. Compared with the conventional estimation algorithm, the proposed two algorithms perform better in multipath propagating environments and bear lower computation burden.

# Acknowledgements

The work of this chapter is supported by the Project of the National Natural Science Foundation of China (Grant No. 61179064, 61172112, 61271404 and 61471363), and the Fundamental Research Funds for the Central Universities (Grant 3122014D008 and 3122014B001).

## Author details

Renbiao Wu<sup>1</sup>, Qiongqiong Jia<sup>1</sup>, Wenyi Wang<sup>1</sup> and Jie Li<sup>2</sup>

1 Tianjin Key Lab for Advanced Signal Processing, Civil Aviation University of China, Tianjin, P. R. China

2 Department of Electronic and Information Engineering, Zhonghuan Information College Tianjin University of Technology, Tianjin, P. R. China

### References

- Kalyanaraman S K, Braasch M S, Kelly J M. Code Tracking Architecture Influence on GPS Carrier Multipath. IEEE Transactions on Aerospace and Electronic Systems 2006; 42(2) 548-561.
- [2] Kos T, Markezic I, Pokrajcic J. Effects of Multipath Reception on GPS Positioning Performance. 52nd International Symposium ELMAR-2010: conference proceedings, 15-17 September 2010, Zadar, Croatia. 399-402.
- [3] Scire-Scappuzzo F, Makarov S N. A Low-Multipath Wideband GPS Antenna With Cutoff or Non-Cutoff Corrugated Ground Plane. Antennas and Propagation 2009; 57(1): 33-46
- [4] Maqsood M, Gao S, Brown T, et al. A Compact Multipath Mitigating Ground Plane for Multiband GNSS Antennas. IEEE TRANSACTIONS ON ANTENNAS AND PROPAGATION 2014; 61(5) 2775-2782.
- [5] Ray J K, Cannon M E, Fenton P. GPS Code and Carrier Multipath Mitigation Using a Multiantenna System. IEEE Transactions on Aerospace and Electronic Systems 2001; 37(1) 183-195.
- [6] Alfred R L. GPS Landing System Reference Antenna. IEEE Antennas and Propagation Society 2010; 52(1) 104-113.
- [7] Michael S B. GPS Multipath Model Validation. IEEE Position Location and Navigation Symposium 1996: conference proceedings, April 1996, Atlanta, GA. 672-678.
- [8] Cannon M E, Lachapelle G, Qiu W, et al. Performance Analysis of a Narrow Correlator Spacing Receiver for Precise Static GPS Positioning. IEEE Position Location and Navigation Symposium 1994: conference proceedings, April 1994, Las Vegas. 2994– 2999
- [9] Tung Hai Ta, Son Hong Ngo. A Novel Signal Acquisition Method for GPS Dual-Frequency Ll C/A and L2C Receivers. International Conference on Advanced Technologies for Communications (ATC 2011) : conference proceedings, Aug 2011. 231-234.

- [10] Chengjun Li, Mingquan Lu, Zhenming Feng, Qi Zhang. Study on GPS Acquisition Algorithm and Performance Analysis. Journal of Electronics & Information Technology 2010; 32(2) 296-300.
- [11] Olivier Besson, Peter Stoica. Nonlinear least-squares frequency estimation and detection for sinusoidal signals with arbitrary envelope. Digital Signal Processing 1999; 9(1) 45-56.
- [12] Jian Li, Renbiao Wu. An efficient algorithm for time delay estimation. IEEE Transactions on Signal Processing 1998; 46(8) 2231-2235.
- [13] Jian Li, Dunmin Zheng, Peter Stoica. Angle and Waveform Estimation via RELAX. IEEE Transactions on Aerospace and Electronic Systems 1997; 33(3) 1077-1087.
- [14] Renbiao Wu, Jian Li, Zhengshe Liu. Super resolution time delay estimation via MODE-WRELAX. IEEE Transactions on Aerospace and Electronic Systems 1999; 35(1) 294-307.
- [15] Renbiao Wu, Jian Li. Time-Delay Estimation via Optimizing Highly Oscillatory Cost Functions. IEEE Journal of Oceanic Engineering 1998; 23(3) 235-244.

# Use of Fast Fourier Transform for Sensitivity Analysis

Andrej Prošek and Matjaž Leskovar

Additional information is available at the end of the chapter

http://dx.doi.org/10.5772/59769

# 1. Introduction

The uncertainty quantification of code calculations is typically accompanied by a sensitivity analysis, in which the influence of the individual contributors to the uncertainty is determined. In the sensitivity analysis, the basic step is to perform sensitivity calculations varying the input parameters. One or more input parameters could be varied at a time. The typical statistical methods for the sensitivity analysis used in uncertainty methods are for example Pearson's Correlation Coefficient, Standardized Regression Coefficient, Partial Correlation Coefficient and others [1]. The output results are time domain signals. The objective of this study was to use fast Fourier transform (FFT) based approaches to determine the sensitivity of output parameters. In the reference [2], the FFT based approaches have been used for the accuracy quantification. The difference between the accuracy quantification and the sensitivity analysis is that in the accuracy quantification the experimental data are compared to the code calculated data, while in the sensitivity analysis the reference calculation signal is compared to the sensitivity run calculation signal. To do this comparison, first the fast Fourier transform is used to transform time domain signals into frequency domain signals. Then, the average amplitude is calculated, which is the sum of the amplitudes of the frequency domain difference signal (between the sensitivity run calculation signal and the reference calculation signal) normalized by the sum of the amplitudes of the frequency domain reference signal. Finally, the figures of merit based on the average amplitude are used to judge the sensitivity.

Such a FFT based approach is different from the typical sensitivity analysis using a statistical procedure to determine the influence of sensitive input parameters on the output parameter. Namely, the influence of the sensitive input parameters is represented by the average amplitude which remembers the previous history.

In this study it is shown that the proposed FFT based tool is complementary and a good alternative to the mentioned typical statistical methods, if one parameter is varied at a time.



© 2015 The Author(s). Licensee InTech. This chapter is distributed under the terms of the Creative Commons Attribution License (http://creativecommons.org/licenses/by/3.0), which permits unrestricted use, distribution, and eproduction in any medium, provided the original work is properly cited.

The advantage of the proposed method is that the results of the sensitivity analysis obtained by the FFT based tool could be ranked. It provides a consistent ranking of sensitive input parameters according to their influence to the output parameter when one parameter is varied at a time, and based on the fact that the same method can be used for more participants performing calculations. For example, there is no need to have ranking levels like it was proposed in the Phase III of the Best Estimate Methods – Uncertainty and Sensitivity Evaluation (BEMUSE) programme [3] for the qualitative judgement, because in this approach the figure of merit is a quantitative value and therefore can be directly ranked. The zero value of the figure of merit means a not relevant sensitive parameter and the larger the figure of merit is the more influential the input parameter is.

The difference between statistical methods and the FFT based approach is that in the case of statistical methods the influence of each varied input parameter on the output result can be obtained even if more parameters are varied at a time. This cannot be done by FFT based tools when more parameters are varied at a time. Rather, the total influence of sensitive parameters on the result is given by the FFT based tool. But the good thing is that the same measure is used for both single and multiple variations and in this way the compensation effects of the influence of different sensitive parameters could be studied. As was already mentioned the FFT based approaches are complementary to statistical methods.

In this Chapter, first the original fast Fourier transform based method (FFTBM) approach is described. The average amplitude, the signal mirroring, the FFTBM Add-in tool and the time dependent accuracy measures are introduced. Based on signal mirroring the improved FFTBM by signal mirroring (FFTBM-SM) was developed. By calculating the time dependent average amplitude it can be answered, which discrepancy due to the parameter variation contributes to the sensitivity and how much is its contribution. The past application of the FFT based tool for the accuracy quantification showed that the original FFTBM gave an unrealistic judgment of the average amplitude for monotonically increasing or decreasing functions, causing problems in the FFTBM results interpretation. It was found out [4] that the reason for such an unrealistic calculated accuracy of increasing/decreasing signals is the edge between the first and last data point of the investigated signal, when the signal is periodically extended. Namely, if the values of the first and last data point of the investigated signal differ, then there are discontinuities present in the periodically extended signal seen by the discrete Fourier transform, which views the finite domain signal as an infinite periodic signal. The discontinuities give several harmonic components in the frequency domain, thus increasing the sum of the amplitudes, on which FFTBM is based, and by this influencing the accuracy. The influence of the edge due to the periodically extended signal is for clarity reasons called the edge effect.

Then the methods used for the sensitivity analysis are described. For the demonstration of the sensitivity study using FFT based tools the L2-5 test, which simulates the large break loss of coolant accident in the Loss of Fluid test (LOFT) facility, was used. The signals used were obtained from the Organisation for Economic Co-operation and Development (OECD) BEMUSE project. In the BEMUSE project there were 14 participants, each performing a reference calculation and 15 sensitivity runs of the LOFT L2-5 test. Three output parameters

were provided: the upper plenum pressure, the primary side mass inventory and the rod surface temperature.

Finally, the application of the FFT based approaches to the sensitivity analysis is described. Both FFTBM and FFTBM-SM were used.

# 2. Fast fourier transform based method description

The FFT based method is proposed for the sensitivity analysis, which is analogous to the FFT based code-accuracy assessment described in ref. [5]. The FFT based approach for code accuracy consists of three steps: a) selection of the test case (experimental or plant measured time trends to compare), b) qualitative analysis, and c) quantitative analysis. The qualitative analysis is necessary before quantifying the discrepancies between the measured and calculated trends. The qualitative analysis includes also the visual observation of plots and the evaluation of the discrepancies between the measured and calculated trends, which should be predictable and understood. For the sensitivity analysis the same FFT based approach is used for the quantitative analysis as used for the code-accuracy. However, the signals compared now are the output signal obtained with the reference value of the input parameter and the output signal as the result of the sensitive input parameter variation.

In the quantitative analysis, the influence of the sensitive input parameter variation is judged in the frequency domain. Therefore the time domain signals used in the sensitivity analysis have to be transformed in the frequency domain signals. The addressed time domain signals assume values different from zero only in the interval  $[0, T_d]$ , where  $T_d$  is the duration of the signal. Also the digital computers can only work with information that is discrete and finite in length (e.g. *N* points) and there is no version of the Fourier transform that uses finite length signals [6]. The way around this is to make the finite data look like an infinite length signal. This is done by imagining that the signal has an infinite number of samples on the left and right of the actual points. The imagined samples can be a duplication of the actual data points. In this case, the signal looks discrete and periodic. This calls for the discrete Fourier transform (DFT) to be used. There are several ways to calculate DFT. One method is FFT. While it produces the same results as the other approaches, it is incredibly more efficient. The key point to understand the FFTBM is that the periodicity is invoked in order to be able to use a mathematical tool, i.e., the DFT. It seems that the developers of the original FFTBM have not been sufficiently aware of this fact.

The discrete Fourier transform views both, the time domain and the frequency domain, as periodic [6]. However, the signals to be used for the comparison are not periodic and the user must conform to the DFT's view of the world. When a new period starts, the *N* samples on the left side are not related to the samples on the right side. However, DFT views these *N* points to be a single period of an infinitely long periodic signal. This means that the left side of the signal is connected to the right side of the signal, and vice versa. The most serious consequence of the time domain periodicity is the occurrence of the edge, where the signals are glued. When the signal spectrum is calculated with DFT, the edge is taken into account, despite the fact that

the edge has no physical meaning for the comparison, since it was introduced artificially by the applied numerical method. It is known that the edge produces a variegated spectrum of frequencies due to the discontinuity of the edge. These frequencies originating from the artificially introduced edge may overshadow the frequency spectrum of the investigated signal. Therefore an improved version of FFTBM by signal mirroring has been proposed, which is described in detail in [4]. Both the original FFTBM and the improved FFTBM by signal mirroring have been used in the demonstration application. The same equations are used for the calculation of the average amplitude, like for the original FFTBM, except that, instead of the original signals, the symmetrized signals are used (for further details see ref. [4]). In the following it is first described how the average amplitude is calculated.

#### 2.1. Average amplitude

FFT is another method for calculating the DFT. While it produces the same result as the other approaches, it significantly reduces the computation time. FFT usually operates with a number of values *N* that is a power of two. Typically, *N* is selected between 32 and 4096 [6]. In addition, the sampling theorem must be fulfilled to avoid the distortion of sampled signals due to the aliasing occurrence. The sampling theorem says: "a signal that varies continuously with time is completely determined by its values at an infinite sequence of equally spaced times if the frequency of these sampling times is greater than twice the highest frequency component of the signal" [7]. Thus if the number of points defining the function in the time domain is  $N=2^{m}$ <sup>+1</sup>, then according to the sampling theorem the sampling frequency is:

$$\frac{1}{\tau} = f_s = 2f_{\max} = \frac{N}{t_d} = \frac{2^{m+1}}{t_d}$$
(1)

where  $\tau$  is the sampling interval,  $t_d$  is the transient time duration of the sampled signal and  $f_{\text{max}}$  is the highest (maximum) frequency component of the signal. The sampling theorem does not hold beyond  $f_{max}$ . From the relation in Eq. (1) it is seen that the number of points selection is strictly connected to the sampling frequency. The FFT algorithm requires the number of points, equally spaced, which is a power with base 2. Generally an interpolation is necessary to satisfy this requirement. The original FFTBM is done so that the default value of the exponent m ranges from 8 to 11. This gives N ranging from 512 to 4096. The final number of points used by FFTBM is determined depending on the value of  $f_{\text{fix}}$  which is the minimum requested maximum frequency and is input value. If  $f_{max}$  is not larger than  $f_{fixr}$  the number of points is doubled (exponent m is increased for 1) until the criterion is satisfied or the exponent m equals to 11. Please note, that the minimum value of the exponent m is 8. The FFTBM application implies the following input values: the fixed frequency  $f_{\text{fix}}$  (minimum maximum frequency of the analysis, this determines the number of points N), the cut off frequency ( $f_{cut}$ ), the start time  $t_s$  and the end time  $t_e$  of the analysed window (determines the analysis window  $t_d = t_s - t_e$ ). A cut off frequency has been introduced to cut off spurious contributions, generally negligible. When  $f_{\text{cut}}$  is equal or larger than  $f_{\text{fixr}}$  all frequency components are considered.

For the calculation of the differences between the output signal obtained with the reference value of the input parameter (reference signal  $F_{ref}(t)$ ) and the output signal as the result of the sensitive input parameter variation (sensitive signal  $F_{sen}(t)$ ), the reference signal ( $F_{ref}(t)$ ) and the difference signal  $\Delta F(t)$  are needed. The difference signal in the time domain is defined as:

$$\Delta F(t) = F_{ref}(t) - F_{sen}(t).$$
<sup>(2)</sup>

After performing the fast Fourier transform the obtained spectra of amplitudes are used for the calculation of the average amplitude (*AA*):

$$AA = \frac{\sum_{n=0}^{2^{m}} \left| \tilde{\Delta} F(f_{n}) \right|}{\sum_{n=0}^{2^{m}} \left| \tilde{F}_{ref}(f_{n}) \right|},$$
(3)

where  $|\tilde{\Delta}F(f_n)|$  is the difference signal amplitude at frequency  $f_n$  and  $|\tilde{F}_{ref}(f_n)|$  is the reference signal amplitude at frequency  $f_n$ . The AA factor can be considered as a sort of average fractional difference and the closer the AA value is to zero, the smaller is the sensitivity (influence). In our specific application, the larger the sensitivity is the larger is the difference between the signals, normally resulting in a larger AA value. Typically, based on the previous experience in the accuracy quantification the values of AA below 0.3 indicate a small influence (in the case of pressure below 0.1), while the values above 0.5 indicate a large influence.

The above Eq. (3) can be also viewed as:

$$AA = \frac{AA_{dif}}{AA_{ref}},$$
(4)

where  $AA_{dif}$  is the average amplitude of the difference signal and  $AA_{ref}$  is the average amplitude of the reference signal:

$$AA_{dif} = \frac{1}{2^{m} + 1} \sum_{n=0}^{2^{m}} \left| \tilde{\Delta} F(f_{n}) \right|,$$
(5)

$$AA_{ref} = \frac{1}{2^m + 1} \sum_{n=0}^{2^m} \left| \tilde{F}_{ref}(f_n) \right|.$$
(6)

If the reference and sensitive signals are the same, the difference signal is zero. The larger the difference is, the larger is  $AA_{dif}$  (in principle). On the other hand,  $AA_{ref}$  normalizes the average amplitude AA and the higher the sum of amplitudes is, the lower is the average amplitude AA. This means that for ranking the sensitivities of the selected output parameter only  $AA_{dif}$  has an influence. On the other hand, for judging the influence of a single sensitive parameter variation on different output parameters, besides  $AA_{dif}$  also  $AA_{ref}$  influences the ranking due to the different  $AA_{ref}$  the output parameters have.

fraction 
$$A0 = \frac{\left|\tilde{\Delta}F(f_0)\right|}{\sum_{n=0}^{2^m} \left|\tilde{\Delta}F(f_n)\right|},$$
 (7)

where  $|\tilde{\Delta}F(f_0)|$  is the mean value of the difference signal and it is equivalent to the mean error (ME) in the time domain as defined in ref. [8]. The measure *fraction* A0 shows when the frequency amplitudes are dominating or when the mean values (like constant differences) are dominating the sum of the amplitudes.

### 2.2. Signal mirroring

If we have a function F(t) where  $0 \le t \le t_d$  and  $t_d$  is the transient time duration, its mirrored function is defined as  $F_{mir}(t)=F(-t)$ , where  $-t_d \le t \le 0$ . From these functions a new function is composed which is symmetrical in regard to the y-axis:  $F_m(t)$ , where  $-t_d \le t \le t_d$ . This is illustrated in Figure 1. By composing the original signal (shown in Figure 1(a)) and its mirrored signal (signal mirroring), a signal without the edge between the first and the last data sample is obtained, and it is called symmetrized signal (shown in Figure 1(b)). It has the double number of points in order not to lose any information. Also it should be noted that the edge is not present in the original time domain signal (see Figure 1(a)). However, when performing FFT, the aperiodic original signal is treated as a periodic original signal as mentioned before and therefore the edge is part of the periodic original signal, what is not physical. In the case of the symmetrized signal the edge is not present even when treating the signal as periodic.

For the calculation of the average amplitude by signal mirroring  $AA_m$  the Eq. (3) is used like for the calculation of AA, except that, instead of the original signals, the symmetrized signals are used. This may be efficiently done by signal mirroring, where the investigated signal is mirrored before the original FFTBM is applied. By composing the original signal and its mirrored signal (signal mirroring), a symmetric signal (also called symmetrized signal) with the same characteristics is obtained, but without introducing the edge when viewed as an infinite periodic signal (for details refer to refs. [4, 9]). FFTBM using the symmetrized signals is called FFTBM-SM.



Figure 1. Examples of (a) original digital signal and (b) symmetrized digital signal

### 2.3. FFTBM Add-in tool

To take the advantages of spread sheets in preparing input forms, analysing data (including analysis of values), modifying graphs and the capability to store time recorded data, plots, input forms and results, the Jožef Stefan Institute (JSI) in-house Microsoft Excel Add-in for the accuracy evaluation of thermal-hydraulic code calculations with FFTBM has been developed in 2003 [10]. Later the tool was upgraded with the capability to symmetrize the signals, and some other improvements. The upgraded tool is called JSI FFTBM Add-in 2007 [11] and it has been used for the sensitivity study, described in this chapter. It includes both FFTBM and FFTBM-SM. As already mentioned, the difference between FFTBM and FFTBM-SM is that in the latter the signals are symmetrized to eliminate the edge effect in calculating the average amplitude by signal mirroring ( $AA_m$ ).

JSI FFTBM Add-in 2007 provides additional information on interpolated data of the signals used, the difference signals, the amplitude spectra and the AA dependency on the cut frequency. The user can use the interpolated data for visual checking about the agreement of the original signal and the interpolated signal. The amplitude spectra give the possibility to compare the spectra between different signals. Information on the AA dependency on the cut frequency is used to check if the cut frequency is selected properly. Usually the dependency is not so big, therefore by default AA at the selected  $f_{cut}$  frequencies is calculated:

- minimal AA (AA<sub>min</sub>) at frequency (when  $f_{cut} > 0.05 f_{max}$ ) which gives the minimum AA,
- average AA (AA<sub>avg</sub>) is calculated as the average AA at all cut frequencies,
- maximal AA (AA<sub>max</sub>) at the frequency (when  $f_{cut} > 0.05 f_{max}$ ) which gives the maximum AA,
- 5 percentile AA (AA<sub>05</sub>) at frequency  $f_{\text{cut}} = 0.05 f_{\text{max}}$
- 50 percentile AA (AA<sub>50</sub>) at frequency  $f_{cut} = 0.5 f_{max}$
- 100 percentile AA (AA<sub>100</sub>) considering all amplitudes (for  $f_{cut} = f_{max}$ ).

This gives an indication if AA is significantly dependent on the cut frequency. In principle, AA should not be much different when half or all frequencies from the amplitude spectrum are considered for the AA calculation. If this is not the case, deeper insight into AA is needed

to judge if there is a spurious contribution present in the signal. For example, in the case of measured data, noise may be present in the signal. In the case of code calculated digital data, noise is not present in the signals, therefore the whole amplitude spectrum is recommended for the AA calculation. Nevertheless, the user should be aware that AA depends on the cut frequency and that the result may change when not all frequencies are considered. Typically higher frequency components have lower amplitudes than lower frequencies, therefore the lower frequency content is always used for the AA calculation (only higher frequency components are filtered).

### 2.4. Time dependent average amplitude

In the ref. [12] the influence of the time window selection was studied. Instead of a few phenomenological windows a series of narrow windows (phases) could be selected. This gives the possibility to get the time dependency of the average amplitude. The increasing time interval was defined as a set of time intervals each increased for the duration of one narrow time window and the last time interval being the whole transient duration time. By increasing the time interval we see how the average amplitude changes with the time progression as it is shown in Figure 2. The average amplitude was calculated by the original FFTBM not considering the edge effect. Therefore the average amplitude shown in Figure 2(b) first increases and then partly decreases in spite of the discrepancy present all this time during the temperature increase shown in Figure 2(a).

The time dependent average amplitude is also indispensable for the sensitivity analysis. From such a time dependant average amplitude it can be easily seen when the largest influence occurs on the output parameter due to the sensitive parameter variation.



Figure 2. Time trend of (a) primary pressure and (b) the corresponding average amplitude

### 3. Methods used for sensitivity analysis

In BEMUSE, Phase II, single parameter sensitivity analyses have been proposed and performed by the participants to study the influence of different parameters (break area, gap conductivity, core pressure drops, time of scram etc.) upon the predicted large-break loss-of-coolant accident (LBLOCA) evolution [13]. The performed sensitivity studies were intended to be used as guidance for deriving uncertainties of relevant input parameters like for phase III of the BEMUSE programme.

The sensitivity analysis is concerned, generally, with the influence of inputs on the output and output variability. Generally, sensitivity analyses are conducted by defining the model and its independent and dependent variables, assigning probability density functions to each input parameter, generating an input matrix through an appropriate random sampling method, performing calculations, and assessing the influences and relative importance of each input/ output relationship.

In our demonstration case, the calculated data obtained in the Phase II of BEMUSE provided by the host organization have been used. The input matrix consists of the single parameter variation. The range of variations has been proposed by the host organization. For sensitivity calculations, only one value (minimal or maximal) of the input parameter was proposed when the range of the parameter variation was specified for selected sensitive parameter. For each single parameter variation the calculation was performed. The influence of the sensitive parameter variation has been estimated through the application of FFT based approaches.

We will call sensitivity (of the output parameter Y versus the i-th input parameter X<sub>i</sub>) a measure having the dimension of  $\frac{\partial Y}{\partial X_i}$  that is independent of the range of variation of the parameter X<sub>i</sub>. Sensitivity is related to output variability.

We will call influence a measure of the effect of the variation of the parameter  $X_i$  on its full range  $(\Delta X_i)$  having the dimension of  $\frac{\partial Y}{\partial X_i} \Delta X_i$  (same as Y) or more often dimensionless form

 $\frac{\partial Y}{\partial X_i} \frac{\Delta Y}{\Delta X_i}.$ 

In our sensitivity analysis the influences were determined. Please note that classical measures of influences are: Pearson's or Spearman's Correlation Coefficients, Standardised Regression Coefficients, etc. [14]. In FFT based approaches the AA is a dimensionless number, showing influences in terms of the average amplitude obtained in the frequency domain which represents the physical influence (e.g. temperature or pressure change).

# 3.1. Test description

The LOFT L2-5 test was selected for this demonstration because a huge amount of data was available [15]. The reference and sensitivity calculations of the LOFT L2-5 test were performed in the phase II of the BEMUSE research program. The nuclear LOFT integral test facility is a scale model of a pressurized water reactor. The objective of the test was to simulate a loss of coolant accident (LOCA) caused by a double-ended, off-shear guillotine cold leg rupture coupled with a loss of off-site power. The experiment was initiated by opening the quick opening blowdown valves in the broken loop hot and cold legs. The reactor scrammed and emergency core cooling systems started their injection. After initial heatup the core was

quenched at 65 s, following the core reflood. The low pressure injection system (LPIS) was stopped at 107.1 s, after the experiment was considered complete. In total 14 calculations from 13 organizations were performed. For more detailed information on the calculations the reader is referred to [4, 15].

### 3.2. Sensitivity calculations description

The series of sensitivity calculations with assigned parameters was proposed to participants. For each parameter the host organization recommended the value to be used. The short description of the cases to be analysed is given in Table 1.

ID	Parameter	Recommended values (RV)	Description		
S-1	Break Area	RC x 1.15	Tube diameter from reactor pressure vessel to break point shall be modified in respect to RC.		
S-2	Gap Conductivity	RC x 0.2	Only in the hot rod in the hot channel (zone 4).		
S-3	Gap Thickness	RC x 3	Only in the hot rod in the hot channel (zone 4).		
S-4	Presence of Crud	0.15 mm	Consideration of 0.15 mm of crud in hot rod in hot channel with thermal conductivity that is characteristic of ceramic material, e.g. Al2O3.		
S-5	Fuel Conductivity	RC x 0.4	Only in the hot rod in the hot channel (zone 4).		
S-6	Core Pressure Drop	RC + D: $DP_{tot}=(DP_{tot})_{RC} \times 1.3$	The pressure drop across the core shall increase (decrease) of an amount D to obtain a total pressure drop that is 30% bigger than the total pressure drop of the reference case.		
S-7	CCFL at Upper Tie Plate (UTP) and/or connection upper plenum (UP)	Range not assigned	Counter courant flow limitation (CCFL) is nodalization dependent. Each participant can propose a solution.		
S-8	Decay Power	RC x 1.25	The decay power has to be 25% bigger than in the reference case.		
S-9	Time of Scram	RC + 1 s	The power curve shall follow the imposed trend that implies full power till RC + 1 sec and after that shall followed the decay power.		
S-10	Maximum Linear Power	RC x 1.5	Only in the hot rod in the hot channel (zone 4).		
S-11	Accumulator Pressure	RC - 0.5 MPa	Set point of accumulator pressure 0.5 MPa lower than the set point in the base case (= 4.29 MPa).		
S-12	Accumulator Liquid Mass	RC x 0.7	Accumulator liquid mass shall be 0.7 times the value in the reference case.		
S-13	Pressurizer Level	RC - 0.5 m	Pressurizer level shall be 0.5 m lower than in the reference case.		
S-14	HPIS	Failure	Failure of HPIS.		
S-15	LPIS injection initiated	RC + 30 s	Delay in starting LPIS injection.		
RC: va	alue used in Reference Case				

Table 1. List of sensitivity analyses and proposed parameter variations (adapted per Table 6 in ref. [15])
Name	S-1	S-2	S-3	S-4	S-5	S-6	S-7	S-8	S-9	S-10	S-11	S-12	S-13	S-14	S-15
P-1	RC × 1.15 (area)	RC × 0.5	$\checkmark$	$\checkmark$	RC × 0.5	$\checkmark$	CCFL at UTP	$\checkmark$							
P-2	√*	$\sqrt{*}$	√*		√*	√*		$\sqrt{*}$	√*	√*	√*	$\checkmark$	√*	√*	√*
P-3	RC × 0.7	RC × 2	$\sqrt{*}$	$\sqrt{*}$	√*	$\sqrt{*}$		√*	√*	√*	$\sqrt{*}$	√*	√*	√*	$\sqrt{*}$
P-4	$\checkmark$		$\checkmark$		$\checkmark$	$\checkmark$		$\checkmark$							
P-5	Adjusted to pressure	√*				RC × 2 (resist- ance)		V	V	V					
P-6	RC × 1.15 (open size)	$\checkmark$	$\checkmark$	√*	$\sqrt{*}$	√*	√*	√*	√*	√*	√*	√*	√*	√*	√*
P-7	√*					$\sqrt{*}$		√*		√*	$\sqrt{*}$				
P-8	$\checkmark$	RC × 0.41	RC × 2.4	$\checkmark$	RC × 0.6	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	RC × 1.2	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$
P-9	$\sqrt{*}$	√*	√*	√*	√*	√*	CCFL at UP	√*	√*	√*	√*	$\sqrt{*}$	√*	√*	√*
P-10	$\checkmark$	$\checkmark$	$\checkmark$		$\checkmark$	$\checkmark$		$\checkmark$							
P-11	√*	$\sqrt{*}$	$\sqrt{*}$	√*	√*	$\sqrt{*}$		√*	√*	√*	√*	√*	√*	√*	√*
P-12	V	V	$\checkmark$	$\checkmark$	$\checkmark$		turned off	$\checkmark$							
P-13	RC × 1.15 (area)	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	default	$\checkmark$							
P-14	$\checkmark$	$\checkmark$	$\checkmark$		$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$		$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$

In Table 2 sensitivity calculations performed by 14 participants are shown. Each row presents sensitivity calculations S-1 to S-15. If the calculation is performed with recommended values, the sign  $\sqrt{}$  is used. If another value has been used, the value of the sensitive parameter is indicated. If the sensitivity calculation has not been performed, the cell is shaded grey.

\* no information given in Ref. [15], but high certainty that recommended values were used;

 $\sqrt{}$  - recommended value used

Table 2. Sensitivity calculations performed by participants

#### 3.3. Figures of merit for sensitivity analysis

Same figures of merit were proposed for the original FFTBM and improved FFTBM-SM. In the case of signal mirroring the additional index m is used to distinguish the FFTBM-SM from FFTBM. The first figure of merit is the average amplitude (AA or  $AA_m$ ), which tells how the single input parameter variation (or combination of input parameter variations) influences the

output parameter. As there are several sensitive input parameters, several participants performing sensitivity runs and more selected output parameters, three additional figures of merit were proposed. The average amplitude of the participant sensitivity runs  $(AA_p \text{ or } AA_{mp})$  is used to judge which sensitivity runs set is more influential to the input parameter variations.  $AA_p \text{ or } AA_{mp}$  is calculated as the average of AAs for the participant sensitivity runs (15 in our specific case). The average amplitude of the sensitivity runs for the same sensitive parameter (AA<sub>s</sub> or AA<sub>ms</sub>) is used to judge how influential (in average) the sensitive parameter is in calculations performed by different participants.  $AA_s$  or  $AA_{ms}$  is calculated as the average of AAs of participants for the same sensitivity run (14 in our specific case). Finally, the total average amplitude (AA<sub>t</sub> or  $AA_{mt}$ ) is the average AA or average AA<sub>m</sub> obtained from all sensitivity runs performed by all participants.

# 4. Application of FFT based approches to sensitivity analysis

In this section the application of the original FFTBM and FFTBM-SM is demonstrated. As was explained in Subsection 2.1, two digital signals (reference and sensitive) of the same duration are used for calculating the average amplitude, which is a measure of the influence of the sensitive parameter variation. An example of calculating  $AA_m$  is given first. Then the single value influence (based on the average amplitude) for the whole time window is given. Finally, the time dependent influence is presented for the sensitivity runs. We conclude this section with the discussion.

## 4.1. AA<sub>m</sub> figure of merit example

In the example the influence of sensitive parameters on three output parameters for the interval 0-119.5 s (whole transient time) is shown for calculations of participant P-14. The participant P-14 provided for each time trend 241 samples. This means that the sampling frequency was 2 Hz. The input values for FFTBM-SM were therefore the following:  $f_{\rm fix}$ =2 Hz,  $f_{\rm cut}$ =2 Hz,  $t_b$ =0 s and  $t_e$ =119.5 s (time 119.5 s was selected because some users provided the last data point at a value slightly smaller than 120 s). Per sampling theorem (Eq. (1)) at least 478 data points are needed. However, the minimum number of points per FFTBM-SM is 512. Table 3 shows that requesting more samples than required has a minor influence on the results.

To get some qualitative impression on the influence of input parameters on output parameters judged by FFTBM-SM, Figure 3 shows time trends of P-14 upper plenum pressure, primary side mass and cladding temperature. Visually it may be indicated that the upper plenum pressure is the most influenced by the break flow (S-1). On the other hand, hot rod parameters (S-2, S-3, S-4 and S-5) and accumulator initial mass (S-12) do not have significant influence on upper plenum pressure (see Figures 3(a2), 3(a3), 3(a4) and 3(a5)). The primary side mass inventory is the most influenced by the gap conductivity (S-2), fuel conductivity (S-5), and the accumulator liquid mass (S-12). When comparing S-2 and S-5 calculations, one may indicate that the S-5 calculation is a bit closer to the reference calculation. On the other hand, comparing the S-2 and S-12 calculation, in the case of S-2 the difference is absolutely larger than S-12,

	Up	per plent	ım pressi	ure	-	Primary	side mas	6	Rod surface temperature					
	N=29	N=210	N=2 <sup>11</sup>	N=2 <sup>12</sup>	N=29	N=210	N=211	N=2 <sup>12</sup>	N=29	N=210	N=2 <sup>11</sup>	N=212		
S-1	0.085	0.088	0.089	0.089	0.102	0.103	0.103	0.104	0.330	0.335	0.338	0.339		
S-2	0.032	0.033	0.034	0.034	0.124	0.125	0.125	0.125	0.799	0.806	0.805	0.807		
S-3	0.015	0.016	0.016	0.016	0.056	0.056	0.057	0.057	0.488	0.491	0.494	0.495		
S-4	0.015	0.016	0.016	0.016	0.056	0.057	0.057	0.057	0.295	0.301	0.301	0.303		
S-5	0.026	0.027	0.027	0.027	0.108	0.108	0.109	0.109	0.937	0.944	0.948	0.948		
S-6	0.019	0.019	0.020	0.020	0.046	0.046	0.046	0.046	0.256	0.258	0.261	0.263		
S-7	0.023	0.024	0.024	0.024	0.051	0.051	0.052	0.052	0.258	0.269	0.270	0.272		
S-8	0.016	0.016	0.017	0.017	0.041	0.041	0.042	0.042	0.143	0.145	0.147	0.148		
S-9	0.018	0.019	0.019	0.019	0.039	0.040	0.040	0.040	0.205	0.208	0.209	0.210		
S-10	0.015	0.016	0.016	0.017	0.043	0.043	0.044	0.044	0.449	0.460	0.460	0.461		
S-11	0.021	0.022	0.022	0.022	0.090	0.090	0.091	0.091	0.239	0.240	0.243	0.245		
S-12	0.029	0.030	0.030	0.031	0.117	0.118	0.119	0.119	0.480	0.487	0.488	0.490		
S-13	0.045	0.046	0.046	0.047	0.065	0.066	0.066	0.066	0.302	0.308	0.310	0.311		
S-14	0.015	0.016	0.016	0.016	0.052	0.053	0.053	0.053	0.255	0.256	0.259	0.261		
S-15	0.016	0.016	0.017	0.017	0.059	0.059	0.060	0.060	0.147	0.150	0.151	0.152		

Table 3. Average amplitude AAm for the whole time interval for participant P-14 calculated by FFFTB-SM as a function of the number of samples N  $\,$ 

however in case of S-12 the difference is present a longer time than in the case of S-2. The calculated  $AA_m$  is comparable.

To see this in more detail, Figure 4 shows part of the magnitude difference signal spectra  $|\tilde{\Delta}F(f_n)|$  for S-2 and S-12, which are used for the calculation of AA<sub>dif</sub> per Eq. (5). Please note that  $f_{max}$  is 2.14 Hz. However, summing of amplitudes up to 0.2 Hz contributes more than 90% to total AA<sub>dif</sub> (for S-2 the sum is 11.26 out of 12.43 and for S-12 the sum is 10.83 out of 11.79). Summing amplitudes up to 0.05 Hz (representing 13 samples out of 513) contributes more than 80% to total AA<sub>dif</sub> (for S-2 the sum is 10.16 out of 12.43 and for S-12 the sum is 9.57 out of 11.79). One may see that the zero frequency component (mean value of difference signal in the time domain) is larger for S-2 than S-12 and that due to this contribution finally S-2 is judged as more influential than S-12.

## 4.2. Single value influence for whole time window

In the example presented in Section 4.1,  $AA_m$  for the P-14 calculation was determined. In this section all fourteen calculations are considered, and both FFTBM and FFTBM-SM are used for calculating all figures of merit presented in Section 3.3. The obtained results for the sensitive parameter influence on the three output parameters (upper plenum pressure, primary side mass inventory and rod surface temperature) are shown in Tables 4 through 6.

The qualitative comparison between FFTBM and FFTBM-SM results showed that the agreement is quite good. This is expected as at the end of the transient the influence of the sensitive parameter is generally insignificant, resulting that in the difference signal the edge is very



Figure 3. Participant P-14 time trends of (a) primary pressure, (b) primary side mass and (c) rod surface temperature for S-1, S-2, S-3, S-5 and S-12 with  $AA_m$ 

small or not present at all. The edge is still present in the reference signal, but because it is used for the normalization it has no impact on the ranking of parameters and so the qualitative agreement between FFTBM and FFTBM-SM is good. This is not the case for the quantitative agreement as the normalization directly impacts the average amplitude. The average amplitudes obtained by both FFTBM and FFTBM-SM suggest that the most influential parameter for the upper plenum pressure is in all calculations the break flow area (S-1). To judge how influential the parameter is, the average amplitude of the sensitivity runs for the same sensitive parameter (AA<sub>s</sub> or AA<sub>ms</sub>) obtained both by FFTBM and FFTBM-SM show that the variations of the break flow area (S-1), pressurizer level (S-13), core pressure drop (S-6) and presence of crud (S-4) the most influence the output parameter upper plenum pressure. The only difference between the FFTBM and FFTBM-SM results is that ranks for S-6 and S-4 are changed.

(a) Applic	cation o	of FFTB	M - up	per ple	num pi	ressure	, time i	nterval	0 - 119	.5 s						
ID-S	S-1	S-2	S-3	S-4	S-5	S-6	S-7	S-8	S-9	S-10	S-11	S-12	S-13	S-14	S-15	
ID-P	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AAp
P-1	0.051	0.011	0.010	0.006	0.009	0.011	0.008	0.013	0.011	0.019	0.019	0.015	0.036	0.011	0.010	0.016
P-2	0.042	0.008	0.010		0.008	0.005		0.002	0.006	0.001	0.006	0.015	0.013	0.001	0.002	0.009
P-3	0.070	0.025	0.035	0.030	0.034	0.108		0.045	0.028	0.042	0.043	0.045	0.060	0.010	0.008	🥚 0.042
P-4	0.110		0.014		0.013	0.015		0.011	0.011	0.012	0.030	0.033	0.027	0.010	0.012	0.025
P-5	0.089	0.014				0.016		0.023	0.018	0.019						🥌 0.030
P-6	0.029	0.010	0.012	0.013	0.010	0.077	0.015	0.009	0.011	0.010	0.011	0.010	0.017	0.008	0.005	0.016
P-7	0.030					0.008		0.006		0.005	0.009					0.012
P-8	0.068	0.013	0.009	0.010	0.012	0.015	0.018	0.014	0.015	0.015	0.016	0.018	0.027	0.012	0.010	0.018
P-9	0.074	0.007	0.009	0.008	0.008	0.010	0.009	0.009	0.010	0.008	0.011	0.015	0.027	0.000	0.008	0.014
P-10	0.059	0.030	0.018		0.008	0.023		0.006	0.007	0.029	0.039	0.009	0.052	0.004	0.012	0.023
P-11	0.035	0.008	0.012	0.117	0.016	0.012		0.012	0.013	0.011	0.019	0.019	0.028	0.012	0.016	0.024
P-12	0.035	0.006	0.009	0.007	0.008	0.009	0.010	0.004	0.009	0.008	0.009	0.006	0.021	0.004	0.009	0.010
P-13	0.041	0.014	0.015	0.011	0.016	0.132	0.016	0.014	0.013	0.015	0.017	0.011	0.024	0.006	0.005	0.023
P-14	0.044	0.017	0.008	0.008	0.013	0.010	0.012	0.008	0.009	0.008	0.011	0.015	0.023	0.008	0.008	0.013
AAs	0.055	0.014	0.013	0.023	0.013	0.032	0.013	0.012	0.012	0.014	0.018	0.017	0.030	0.007	0.009	AAt=0.019
Legend:			0.02-0.	04		>0.04										
(b) Applic	cation o	of FFTB	M-SM	- uppei	plenu	m pres	sure, tii	me inte	rval 0 -	119.5 s	;					
(b) Applic ID-S	cation o S-1	of FFTB S-2	M-SM S-3	- uppei S-4	plenu S-5	m pres S-6	sure, tii S-7	me inte S-8	rval 0 - S-9	119.5 s S-10	S-11	S-12	S-13	S-14	S-15	
(b) Applic ID-S ID-P	S-1 AA <sub>m</sub>	of FFTB S-2 AA <sub>m</sub>	S-3 AAm	- upper S-4 AA <sub>m</sub>	S-5 AA <sub>m</sub>	m press S-6 AA <sub>m</sub>	sure, tii S-7 AA <sub>m</sub>	ne inte S-8 AA <sub>m</sub>	rval 0 - S-9 AA <sub>m</sub>	119.5 s S-10 AA <sub>m</sub>	S-11 AA <sub>m</sub>	S-12 AA <sub>m</sub>	S-13 AA <sub>m</sub>	S-14 AA <sub>m</sub>	S-15 AA <sub>m</sub>	AA <sub>mp</sub>
(b) Applic ID-S ID-P P-1	S-1 AA <sub>m</sub> 0.098	of FFTB S-2 AA <sub>m</sub> 0.021	M-SM S-3 AA <sub>m</sub> 0.020	- upper S-4 AA <sub>m</sub> 0.012	S-5 AA <sub>m</sub> 0.018	m press S-6 AA <sub>m</sub> 0.021	Sure, tii S-7 AA <sub>m</sub> 0.016	ne inte S-8 AA <sub>m</sub> 0.026	rval 0 - S-9 AA <sub>m</sub> 0.022	119.5 s S-10 AA <sub>m</sub> 0.038	S-11 AA <sub>m</sub> 0.038	S-12 AA <sub>m</sub> 0.030	S-13 AA <sub>m</sub> 0.070	S-14 AA <sub>m</sub> 0.021	S-15 AA <sub>m</sub> 0.019	AA <sub>mp</sub> 0.031
(b) Applic ID-S ID-P P-1 P-2	S-1           AAm           0.098           0.080	of FFTB S-2 AA <sub>m</sub> 0.021 0.016	M-SM S-3 AA <sub>m</sub> 0.020 0.018	- upper S-4 AA <sub>m</sub> 0.012	<ul> <li>plenu</li> <li>S-5</li> <li>AA<sub>m</sub></li> <li>0.018</li> <li>0.014</li> </ul>	m press S-6 AA <sub>m</sub> 0.021 0.009	Sure, tii S-7 AA <sub>m</sub> 0.016	me inte S-8 AA <sub>m</sub> 0.026 0.003	rval 0 - S-9 AA <sub>m</sub> 0.022 0.011	119.5 s S-10 AA <sub>m</sub> 0.038 0.002	S-11 AA <sub>m</sub> 0.038 0.012	S-12 AA <sub>m</sub> 0.030 0.029	S-13 AA <sub>m</sub> 0.070 0.026	S-14 AA <sub>m</sub> 0.021 0.002	S-15 AA <sub>m</sub> 0.019 0.004	AA <sub>mp</sub> 0.031 0.017
(b) Applia ID-S ID-P P-1 P-2 P-3	AAm       0.098       0.145	of FFTB S-2 AA <sub>m</sub> 0.021 0.016 0.048	M-SM S-3 AA <sub>m</sub> 0.020 0.018 0.071	- upper S-4 AA <sub>m</sub> 0.012 0.055	plenu       S-5       AAm       0.018       0.014       0.065	m press S-6 AA <sub>m</sub> 0.021 0.009 0.127	S-7 AA <sub>m</sub> 0.016	me inte S-8 AA <sub>m</sub> 0.026 0.003 0.090	rval 0 - S-9 AA <sub>m</sub> 0.022 0.011 0.054	119.5 s S-10 AA <sub>m</sub> 0.038 0.002 0.084	S-11 AA <sub>m</sub> 0.038 0.012 0.086	S-12 AA <sub>m</sub> 0.030 0.029 0.090	S-13 AA <sub>m</sub> 0.070 0.026 0.120	S-14 AA <sub>m</sub> 0.021 0.002 0.019	S-15 AA <sub>m</sub> 0.019 0.004 0.015	AA <sub>mp</sub> 0.031 0.017 0.076
(b) Applid ID-S ID-P P-1 P-2 P-3 P-4	S-1       AAm       0.098       0.080       0.145       0.212	of FFTB S-2 AA <sub>m</sub> 0.021 0.016 0.048	M-SM S-3 AA <sub>m</sub> 0.020 0.018 0.071 0.026	- upper S-4 AA <sub>m</sub> 0.012 0.055	plenu       S-5       AAm       0.018       0.014       0.065       0.025	m press S-6 AA <sub>m</sub> 0.021 0.009 0.127 0.028	S-7 AA <sub>m</sub> 0.016	me inte S-8 AA <sub>m</sub> 0.026 0.003 0.090 0.021	rval 0 - S-9 AA <sub>m</sub> 0.022 0.011 0.054 0.023	119.5 s S-10 AA <sub>m</sub> 0.038 0.002 0.084 0.023	S-11 AA <sub>m</sub> 0.038 0.012 0.086 0.059	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051	S-14 AA <sub>m</sub> 0.021 0.002 0.019 0.019	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023	AA <sub>mp</sub> 0.031 0.017 0.076 0.048
(b) Applia ID-S ID-P P-1 P-2 P-3 P-4 P-5	S-1           AAm           0.098           0.145           0.212           0.160	of FFTB S-2 AAm 0.021 0.016 0.048 0.024	M-SM S-3 AA <sub>m</sub> 0.020 0.018 0.071 0.026	- upper S-4 AA <sub>m</sub> 0.012 0.055	plenu           S-5           AAm           0.018           0.014           0.065           0.025	<ul> <li>m press</li> <li>S-6</li> <li>AA<sub>m</sub></li> <li>0.021</li> <li>0.009</li> <li>0.127</li> <li>0.028</li> <li>0.028</li> </ul>	S-7 AA <sub>m</sub> 0.016	S-8           AAm           0.026           0.003           0.090           0.021           0.039	rval 0 - S-9 AAm 0.022 0.011 0.054 0.023 0.032	119.5 s S-10 AAm 0.038 0.002 0.084 0.023 0.034	S-11 AAm 0.038 0.012 0.086 0.059	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051	S-14 AAm 0.021 0.002 0.019 0.019	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023	AA <sub>mp</sub> 0.031 0.017 0.076 0.048 0.053
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6	S-1       AAm       0.098       0.080       0.145       0.212       0.160       0.054	of FFTB S-2 AAm 0.021 0.016 0.048 0.024 0.019	M-SM S-3 AA <sub>m</sub> 0.020 0.018 0.071 0.026 0.021	- upper S-4 AA <sub>m</sub> 0.012 0.055 0.023	plenu           S-5           AAm           0.018           0.014           0.065           0.025           0.018	m press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.130	S-7 AAm 0.016	S-8           AAm           0.026           0.003           0.090           0.021           0.039           0.016	rval 0 - S-9 AA <sub>m</sub> 0.022 0.011 0.054 0.023 0.032 0.032	119.5 s S-10 AA <sub>m</sub> 0.038 0.002 0.084 0.023 0.034 0.018	S-11 AA <sub>m</sub> 0.038 0.012 0.086 0.059 0.021	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064 0.018	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051 0.032	S-14 AA <sub>m</sub> 0.021 0.002 0.019 0.019 0.014	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.010	AA <sub>mp</sub> 0.031 0.017 0.076 0.048 0.048 0.053 0.029
(b) Applic ID-S ID-P P-1 P-2 P-3 P-3 P-4 P-5 P-6 P-6 P-7	S-1           AAm           0.098           0.145           0.212           0.160           0.054           0.056	of FFTB S-2 AAm 0.021 0.016 0.048 0.024 0.019	M-SM S-3 AA <sub>m</sub> 0.020 0.018 0.071 0.026 0.021	- upper S-4 AA <sub>m</sub> 0.012 0.055 0.023	plenu           S-5           AAm           0.018           0.014           0.065           0.025           0.018	m press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.130           0.016	S-7 AAm 0.016	me inte S-8 AAm 0.026 0.003 0.090 0.021 0.039 0.016 0.010	rval 0 - S-9 AAm 0.022 0.011 0.054 0.023 0.032 0.032	119.5 s S-10 AAm 0.038 0.002 0.084 0.023 0.034 0.018 0.008	S-11 AAm 0.038 0.012 0.086 0.059 0.021 0.021	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064 0.018	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051 0.032	S-14 AA <sub>m</sub> 0.021 0.002 0.019 0.019 0.014	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.010	AAmp 0.031 0.017 0.076 0.048 0.053 0.029 0.021
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8	S-1           S-1           AAm           0.098           0.145           0.212           0.160           0.054           0.054           0.127	of FFTB S-2 AAm 0.021 0.016 0.048 0.024 0.019 0.024	M-SM S-3 AA <sub>m</sub> 0.020 0.018 0.071 0.026 0.021 0.021	- upper S-4 AAm 0.012 0.055 0.023 0.018	plenu           S-5           AAm           0.018           0.014           0.065           0.025           0.018           0.018           0.018           0.018	m press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.130           0.016           0.029	sure, tin S-7 AA <sub>m</sub> 0.016 0.028 0.028	me inte S-8 AAm 0.026 0.003 0.090 0.021 0.039 0.016 0.010 0.026	val 0 -           S-9           AAm           0.022           0.011           0.054           0.023           0.032           0.020           0.020	119.5 s S-10 AAm 0.038 0.002 0.084 0.023 0.034 0.018 0.008 0.028	S-11 AA <sub>m</sub> 0.038 0.012 0.086 0.059 0.021 0.021 0.016 0.031	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064 0.018 0.036	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051 0.032 0.032	S-14 AA <sub>m</sub> 0.021 0.002 0.019 0.019 0.014 0.024	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.010 0.010	AAmp 0.031 0.017 0.076 0.048 0.053 0.029 0.021 0.034
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8 P-9	S-1           S-1           AAm           0.098           0.145           0.212           0.160           0.054           0.056           0.127           0.139	of FFTB S-2 AAm 0.021 0.016 0.048 0.024 0.019 0.024 0.013	M-SM S-3 AA <sub>m</sub> 0.020 0.018 0.021 0.021 0.021 0.017 0.017	- upper S-4 AA <sub>m</sub> 0.012 0.055 0.023 0.018 0.015	plenu           S-5           AAm           0.018           0.014           0.065           0.025           0.018           0.018           0.024           0.015	m press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.130           0.016           0.029           0.018	sure, tii S-7 AA <sub>m</sub> 0.016 0.028 0.028 0.034 0.017	me inte S-8 AAm 0.026 0.003 0.090 0.021 0.039 0.016 0.010 0.026 0.017	val 0 -           S-9           AAm           0.022           0.011           0.054           0.023           0.032           0.020           0.029           0.019	119.5 s S-10 AA <sub>m</sub> 0.038 0.002 0.084 0.023 0.034 0.018 0.008 0.028 0.028	S-11 AA <sub>m</sub> 0.038 0.012 0.086 0.059 0.059 0.021 0.016 0.031 0.022	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064 0.018 0.018 0.036 0.028	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051 0.032 0.032 0.050 0.053	S-14 AA <sub>m</sub> 0.021 0.002 0.019 0.019 0.014 0.024 0.024	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.023 0.010 0.010 0.018 0.014	AAmp 0.031 0.017 0.076 0.048 0.053 0.029 0.021 0.034 0.027
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8 P-9 P-10	S-1           S-1           AAm           0.098           0.145           0.212           0.160           0.054           0.056           0.127           0.139           0.118	f FFTB S-2 AA <sub>m</sub> 0.021 0.016 0.048 0.024 0.019 0.024 0.013 0.060	H-SM S-3 AA <sub>m</sub> 0.020 0.018 0.021 0.026 0.021 0.017 0.017 0.035	- upper S-4 AA <sub>m</sub> 0.012 0.055 0.023 0.023 0.018 0.015	plenu           S-5           AAm           0.018           0.014           0.065           0.025           0.018           0.018           0.018           0.018           0.018           0.019           0.018	m press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.0130           0.016           0.029           0.018           0.043	sure, tii S-7 AA <sub>m</sub> 0.016 0.028 0.028 0.034 0.017	me inte S-8 AAm 0.026 0.003 0.090 0.021 0.039 0.016 0.010 0.026 0.017 0.012	val 0 -           S-9           AAm           0.022           0.011           0.054           0.023           0.032           0.020           0.020           0.020           0.021           0.022           0.032           0.020           0.021           0.022           0.023           0.024           0.032           0.032           0.032	119.5 s           S-10           AAm           0.038           0.002           0.084           0.023           0.034           0.018           0.008           0.028           0.015           0.056	S-11 AA <sub>m</sub> 0.038 0.012 0.086 0.059 0.021 0.016 0.031 0.022 0.073	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064 0.018 0.018 0.036 0.028 0.017	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051 0.032 0.032 0.050 0.053 0.098	S-14 AA <sub>m</sub> 0.021 0.019 0.019 0.019 0.014 0.024 0.024 0.000 0.009	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.010 0.010 0.018 0.014 0.024	AAmp 0.031 0.017 0.076 0.048 0.053 0.029 0.021 0.034 0.027 0.044
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-4 P-5 P-6 P-7 P-8 P-9 P-10 P-11	S-1           AAm           0.098           0.145           0.212           0.160           0.054           0.056           0.127           0.139           0.118           0.068	of FFTB           S-2           AAm           0.021           0.016           0.048           0.024           0.019           0.024           0.013           0.060           0.017	H-SM S-3 AA <sub>m</sub> 0.020 0.018 0.021 0.021 0.017 0.017 0.017 0.035 0.024	- upper S-4 AA <sub>m</sub> 0.012 0.055 0.023 0.023 0.018 0.015	plenu           S-5           AAm           0.018           0.014           0.065           0.025           0.018           0.024           0.015           0.030	m press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.016           0.029           0.018           0.043	sure, tin S-7 AA <sub>m</sub> 0.016 0.028 0.034 0.017	me inte S-8 AA <sub>m</sub> 0.026 0.003 0.090 0.021 0.039 0.016 0.010 0.026 0.017 0.012 0.024	val 0 -           S-9           AAm           0.022           0.011           0.054           0.023           0.032           0.020           0.020           0.020           0.021           0.022           0.032           0.020           0.021           0.022           0.023           0.024           0.025	119.5 s S-10 AA <sub>m</sub> 0.038 0.002 0.084 0.023 0.034 0.018 0.008 0.028 0.028 0.025 0.023	S-11           AAm           0.038           0.012           0.086           0.059           0.021           0.016           0.031           0.022           0.073	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064 0.018 0.018 0.036 0.028 0.017 0.036	S-13         AAm         0.070         0.026         0.120         0.051         0.032         0.032         0.050         0.050         0.050         0.053         0.052	S-14 AA <sub>m</sub> 0.021 0.019 0.019 0.019 0.014 0.024 0.024 0.000 0.009 0.024	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.010 0.010 0.018 0.014 0.024 0.033	AAmp 0.031 0.017 0.076 0.048 0.053 0.029 0.021 0.034 0.027 0.044 0.044
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8 P-9 P-10 P-11 P-12	S-1           AAm           0.098           0.145           0.212           0.160           0.054           0.055           0.127           0.139           0.118           0.068           0.065	of         FFTB           S-2         AAm           0.021         0.016           0.048         0.024           0.019         0.024           0.013         0.060           0.017         0.011	N-SM           S-3           AAm           0.020           0.018           0.071           0.026           0.021           0.017           0.017           0.035           0.024           0.017	- upper S-4 AAm 0.012 0.055 0.023 0.023 0.018 0.015 0.234 0.014	plenu           S-5           AAm           0.018           0.014           0.065           0.025           0.018           0.024           0.015           0.030           0.016	m press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.016           0.029           0.018           0.043           0.023           0.017	sure, tin S-7 AA <sub>m</sub> 0.016 0.028 0.028 0.034 0.017	me inte           S-8           AAm           0.026           0.003           0.021           0.039           0.016           0.010           0.026           0.010           0.026           0.010           0.026           0.010           0.026           0.012           0.024           0.008	val 0 -           S-9           AAm           0.022           0.011           0.054           0.023           0.032           0.020           0.029           0.013           0.025           0.016	119.5 s S-10 AA <sub>m</sub> 0.038 0.002 0.084 0.023 0.034 0.018 0.008 0.028 0.015 0.056 0.023 0.014	S-11           AAm           0.038           0.012           0.086           0.059           0.021           0.016           0.031           0.022           0.073           0.036           0.018	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064 0.018 0.018 0.036 0.028 0.017 0.036 0.010	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051 0.032 0.032 0.050 0.053 0.098 0.052 0.039	S-14 AA <sub>m</sub> 0.021 0.019 0.019 0.014 0.004 0.0024 0.000 0.024 0.007	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.010 0.010 0.018 0.014 0.024 0.033 0.017	AAmp 0.031 0.017 0.076 0.048 0.053 0.029 0.021 0.034 0.027 0.044 0.046 0.019
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8 P-9 P-10 P-11 P-12 P-13	S-1           AAm           0.098           0.145           0.212           0.145           0.212           0.160           0.054           0.055           0.118           0.068           0.065           0.072	of         FFTB           S-2         AAm           0.021         0.016           0.048         0.024           0.019         0.024           0.013         0.060           0.017         0.011           0.024         0.024	N-SM           S-3           AAm           0.020           0.018           0.071           0.026           0.021           0.017           0.017           0.035           0.024           0.017           0.024	- upper S-4 AA <sub>m</sub> 0.012 0.055 0.023 0.023 0.018 0.015 0.234 0.014 0.019	plenu           S-5           AAm           0.018           0.014           0.065           0.025           0.018           0.018           0.018           0.018           0.015           0.015           0.030           0.016           0.027	n press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.016           0.029           0.016           0.023           0.023           0.017           0.225	sure, tin S-7 AA <sub>m</sub> 0.016 0.028 0.028 0.034 0.017 0.019 0.029	me inter           S-8           AAm           0.026           0.003           0.090           0.021           0.039           0.016           0.010           0.026           0.017           0.024           0.008           0.024	val 0           S-9           AAm           0.022           0.011           0.054           0.023           0.032           0.020           0.020           0.020           0.029           0.013           0.025           0.016           0.023	119.5 s           S-10           AAm           0.038           0.002           0.084           0.023           0.034           0.018           0.008           0.028           0.015           0.023           0.014           0.023	S-11 AA <sub>m</sub> 0.038 0.012 0.086 0.059 0.021 0.016 0.031 0.022 0.073 0.036 0.018 0.030	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064 0.018 0.036 0.028 0.017 0.036 0.010 0.018	S-13 AA <sub>m</sub> 0.070 0.026 0.051 0.051 0.032 0.050 0.053 0.098 0.052 0.039 0.042	S-14 AA <sub>m</sub> 0.021 0.019 0.019 0.019 0.014 0.024 0.000 0.009 0.024 0.007 0.010	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.010 0.010 0.018 0.014 0.024 0.033 0.017 0.007	AAmp 0.031 0.017 0.076 0.048 0.053 0.029 0.021 0.034 0.027 0.044 0.046 0.019 0.040
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-7 P-7 P-8 P-7 P-7 P-8 P-9 P-10 P-11 P-12 P-13 P-14	S-1           S-1           AAm           0.098           0.080           0.145           0.141           0.045           0.045           0.0455	of         FFTB           S-2         AAm           0.021         0.016           0.048         0.024           0.019         0.024           0.013         0.060           0.017         0.011           0.024         0.032	M-SM           S-3           AAm           0.020           0.018           0.021           0.022           0.017           0.017           0.017           0.017           0.017           0.017           0.017           0.017           0.017           0.024           0.017           0.024           0.017           0.026	- upper S-4 AAm 0.012 0.055 0.055 0.012 0.018 0.018 0.018 0.018 0.014 0.019 0.015	plenu           S-5           AAm           0.018           0.0125           0.024           0.015           0.016           0.027           0.026	m press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.028           0.016           0.029           0.016           0.029           0.018           0.043           0.017           0.225           0.019	sure, tin S-7 AA <sub>m</sub> 0.016 0.028 0.034 0.034 0.017 0.029 0.029 0.023	me intel           S-8           AAm           0.026           0.003           0.090           0.021           0.039           0.016           0.010           0.026           0.010           0.026           0.010           0.026           0.010           0.026           0.012           0.024           0.008           0.024           0.016	Image: Non-structure           S-9           S-9           AAm           0.022           0.011           0.054           0.023           0.020           0.020           0.021           0.022           0.023           0.020           0.020           0.021           0.022           0.019           0.016           0.023           0.018	119.5 s           S-10           AAm           0.038           0.002           0.084           0.023           0.034           0.018           0.028           0.028           0.015           0.023           0.014           0.026           0.015	S-11 AA <sub>m</sub> 0.038 0.012 0.086 0.059 0.021 0.016 0.031 0.022 0.073 0.036 0.018 0.030 0.021	S-12 AA <sub>m</sub> 0.030 0.029 0.064 0.018 0.036 0.028 0.017 0.036 0.010 0.018 0.029	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051 0.032 0.032 0.032 0.050 0.053 0.058 0.052 0.039 0.042	S-14 AA <sub>m</sub> 0.021 0.002 0.019 0.019 0.019 0.019 0.024 0.000 0.024 0.000 0.024 0.007 0.010 0.015	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.010 0.018 0.014 0.014 0.024 0.033 0.017 0.007 0.016	AAmp 0.031 0.017 0.076 0.048 0.053 0.029 0.021 0.034 0.027 0.044 0.044 0.046 0.019 0.026
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8 P-7 P-8 P-9 P-10 P-11 P-12 P-13 P-14 AAms	still           S-1           S-1           AAm           0.098           0.080           0.145           0.145           0.145           0.145           0.145           0.145           0.145           0.145           0.145           0.145           0.145           0.054           0.127           0.139           0.148           0.068           0.072           0.085           0.106	of         FFTB           S-2         AAm           0.021         0.016           0.048         0.024           0.019         0.013           0.060         0.017           0.024         0.010           0.024         0.013           0.060         0.017           0.024         0.032           0.024         0.032	M-SM           S-3           AAm           0.020           0.017           0.021           0.017           0.017           0.017           0.017           0.017           0.017           0.017           0.017           0.017           0.024           0.015           0.026	- upper S-4 AA <sub>m</sub> 0.012 0.055 0.055 0.012 0.015 0.018 0.015 0.014 0.019 0.015 0.045	plenu           S-5           AAm           0.018           0.018           0.0125           0.015           0.015           0.016           0.027           0.026           0.027           0.026	m press           S-6           AAm           0.021           0.009           0.127           0.028           0.028           0.028           0.016           0.029           0.016           0.029           0.018           0.043           0.017           0.225           0.019           0.052	sure, tin S-7 AAm 0.016 0.028 0.028 0.034 0.017 0.029 0.023 0.024	me intel           S-8           AAm           0.026           0.003           0.090           0.021           0.039           0.016           0.010           0.026           0.010           0.021           0.020           0.010           0.024           0.008           0.024           0.016           0.024           0.016           0.024           0.016	IVAL         0           S-9         AAm           0.022         0.011           0.054         0.023           0.020         0.012           0.020         0.020           0.020         0.019           0.019         0.019           0.025         0.016           0.023         0.016           0.024         0.016	119.5 s           S-10           AAm           0.038           0.002           0.084           0.023           0.034           0.018           0.008           0.018           0.018           0.023           0.034           0.015           0.026           0.015           0.026           0.015           0.027	S-11 AA <sub>m</sub> 0.038 0.012 0.086 0.059 0.021 0.016 0.031 0.022 0.073 0.036 0.038 0.030 0.031 0.030 0.031	S-12 AA <sub>m</sub> 0.030 0.029 0.090 0.064 0.018 0.036 0.028 0.017 0.036 0.010 0.018 0.029 0.034	S-13 AA <sub>m</sub> 0.070 0.026 0.120 0.051 0.032 0.032 0.050 0.053 0.058 0.052 0.039 0.042 0.045 0.056	S-14 AA <sub>m</sub> 0.021 0.002 0.019 0.019 0.019 0.019 0.024 0.000 0.024 0.000 0.024 0.007 0.010 0.015 0.014	S-15 AA <sub>m</sub> 0.019 0.004 0.015 0.023 0.010 0.018 0.014 0.014 0.024 0.033 0.017 0.007 0.016 0.017	AAmp 0.031 0.017 0.076 0.048 0.053 0.029 0.021 0.034 0.044 0.044 0.044 0.044 0.040 0.019 0.026 AAm=0.030

**Table 4.** Influence of sensitive parameters on upper plenum pressure in time interval 0-119.5 s as judged by (a) original FFTBM and (b) improved FFTBM by signal mirroring

When looking calculations, the most influenced upper plenum calculation is P-3. To judge how the calculation is influenced by the sensitive parameters variation, the average amplitude of the participant sensitivity runs ( $AA_p$  or  $AA_{mp}$ ) is used. Besides P-3 the P-5 calculation was also judged as the much influenced by the sensitive parameter variations. Both methods qualitatively give the same results for the average amplitude of the participant sensitivity runs. The total average amplitude ( $AA_t$  or  $AA_{mt}$ ) show the overall influence of the sensitive parameters variations of all calculations on the output upper plenum pressure. The higher the value is the higher is the influence. The ratio between  $AA_{mt}$  and  $AA_t$  to be 1.88 also tells what the contribution of the edge effect is in average.



Figure 4. Magnitude difference signal spectra for S-2 and S-12 runs of P-14 participants

The average amplitudes shown in Table 5, obtained by both FFTBM and FFTBM-SM suggest that the most influential parameter for the primary side mass inventory when considering all calculations is the accumulator liquid mass (S-12). Both the  $AA_s$  and  $AA_{ms}$  indicate the accumulator liquid mass (S-12), break flow area (S-1), accumulator pressure (S-11) and pressurizer level (S-13) the most influential sensitive parameters on the primary side mass inventory.

When looking the calculations, the most influenced primary side mass inventory calculation is P-3. The  $AA_p$  and  $AA_{mp}$  indicate as the second most influenced the P-13 calculation. Again both methods qualitatively give very similar results for the average amplitude of the participant sensitivity runs. The  $AA_t$  and  $AA_{mt}$  show that the overall influence of the sensitive parameters variations of all calculations on the output primary side mass inventory is higher than on the upper plenum pressure. The ratio between  $AA_{mt}$  and  $AA_t$  is 1.55, indicating that the primary side mass inventory is less influenced by the edge effect (see also Figure3).

The average amplitudes shown in Table 6, obtained by both FFTBM and FFTBM-SM suggest that the most influential parameter for the rod surface temperature when considering all calculations is the fuel conductivity (S-5). Both  $AA_s$  and  $AA_{ms}$  indicate the fuel conductivity (S-5) and gap conductivity (S-2) as the most influential. Significant influences have also the gap thickness (S-3), maximum linear power (S-10), break flow area (S-1) and the accumulator liquid mass (S-12) and a few others. The only difference between the FFTBM and FFTBM-SM results is that the ranks for S-1 and S-12 are changed.

(a) Appli	ication	of FFTI	BM - pı	imary	side m	ass inv	entory,	time ii	nterval	0 - 119	.5 s					
ID-S	S-1	S-2	S-3	S-4	S-5	S-6	S-7	S-8	S-9	S-10	S-11	S-12	S-13	S-14	S-15	
ID-P	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AAp
P-1	0.052	0.026	0.019	0.018	0.015	0.026	0.018	0.017	0.015	0.017	0.048	0.052	0.032	0.014	0.02	0.026
P-2	0.046	0.014	0.014		0.013	0.015		0.014	0.015	0.016	0.017	0.084	0.027	0.012	0.02	0.023
P-3	0.102	0.083	0.071	0.060	0.092	0.180		0.118	0.064	0.086	0.124	0.137	0.124	0.013	0.01	🥚 0.091
P-4	0.125		0.022		0.021	0.042		0.018	0.037	0.023	0.054	0.091	0.036	0.025	0.03	0.043
P-5	0.071	0.027				0.022		0.051	0.038	0.033						0.040
P-6	0.066	0.036	0.056	0.020	0.052	0.045	0.061	0.035	0.035	0.036	0.034	0.158	0.044	0.040	0.07	0.052
P-7	0.035					0.035		0.017		0.007	0.026					0.024
P-8	0.083	0.053	0.016	0.046	0.025	0.051	0.042	0.022	0.038	0.033	0.042	0.073	0.069	0.031	0.03	0.043
P-9	0.073	0.014	0.013	0.015	0.011	0.012	0.012	0.022	0.020	0.008	0.038	0.093	0.033	0.000	0.06	0.028
P-10	0.089	0.010	0.003		0.059	0.019		0.039	0.034	0.019	0.153	0.095	0.041	0.038	0.04	0.049
P-11	0.041	0.019	0.024	0.145	0.041	0.020		0.048	0.020	0.033	0.040	0.053	0.032	0.039	0.07	0.045
P-12	0.039	0.010	0.033	0.018	0.022	0.022	0.024	0.007	0.037	0.025	0.024	0.203	0.039	0.029	0.09	0.042
P-13	0.072	0.047	0.035	0.045	0.066	0.077	0.000	0.050	0.077	0.044	0.092	0.179	0.075	0.049	0.07	🥌 0.065
P-14	0.049	0.136	0.035	0.034	0.104	0.032	0.026	0.022	0.023	0.023	0.049	0.090	0.060	0.041	0.05	0.052
AAs	0.067	0.040	0.028	0.044	0.043	0.043	0.026	0.034	0.035	0.029	0.057	0.109	0.051	0.028	0.05	AAt=0.046
Legend:			0.05-0	.1			>0.1									
(b) Appl	ication	of FFT	BM-SM	l - prim	nary sic	le mass	inven	tory, tii	ne inte	rval 0 -	119.5 s	;				
(b) Appl ID-S	ication S-1	of FFT S-2	BM-SM S-3	l - prim S-4	ary sic S-5	le mass S-6	inven S-7	tory, tii S-8	ne inte S-9	rval 0 - S-10	119.5 s S-11	s S-12	S-13	S-14	S-15	
(b) Appl ID-S ID-P	ication S-1 AA <sub>m</sub>	of FFT S-2 AA <sub>m</sub>	BM-SM S-3 AA <sub>m</sub>	I - prim S-4 AA <sub>m</sub>	S-5 AA <sub>m</sub>	le mass S-6 AA <sub>m</sub>	inven S-7 AA <sub>m</sub>	tory, tii S-8 AA <sub>m</sub>	ne inte S-9 AA <sub>m</sub>	rval 0 - S-10 AA <sub>m</sub>	119.5 s S-11 AA <sub>m</sub>	S-12 AA <sub>m</sub>	S-13 AA <sub>m</sub>	S-14 AA <sub>m</sub>	S-15 AA <sub>m</sub>	AA <sub>mp</sub>
(b) Appl ID-S ID-P P-1	S-1 AA <sub>m</sub> 0.096	of FFT S-2 AA <sub>m</sub> 0.043	BM-SM S-3 AA <sub>m</sub> 0.034	I - prim S-4 AA <sub>m</sub> 0.030	S-5 AA <sub>m</sub> 0.028	le mass S-6 AA <sub>m</sub> 0.034	S-7 AA <sub>m</sub>	S-8 AA <sub>m</sub> 0.033	ne inte S-9 AA <sub>m</sub> 0.028	rval 0 - S-10 AA <sub>m</sub> 0.032	119.5 s S-11 AA <sub>m</sub> 0.071	S-12 AAm 0.084	S-13 AA <sub>m</sub> 0.062	S-14 AA <sub>m</sub> 0.025	S-15 AA <sub>m</sub> 0.037	AA <sub>mp</sub> <ul> <li>0.045</li> </ul>
(b) Appl: ID-S ID-P P-1 P-2	S-1 AA <sub>m</sub> 0.096	of FFT S-2 AA <sub>m</sub> 0.043 0.028	BM-SM S-3 AA <sub>m</sub> 0.034 0.028	- prim S-4 AA <sub>m</sub> 0.030	AAry sic S-5 AAm 0.028 0.025	le mass S-6 AA <sub>m</sub> 0.034 0.028	S-7 AA <sub>m</sub> 0.030	tory, tin S-8 AA <sub>m</sub> 0.033 0.025	ne inte S-9 AA <sub>m</sub> 0.028 0.028	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029	119.5 s S-11 AA <sub>m</sub> 0.071 0.035	S-12 AA <sub>m</sub> 0.084 0.139	S-13 AA <sub>m</sub> 0.062 0.047	S-14 AA <sub>m</sub> 0.025 0.024	S-15 AA <sub>m</sub> 0.037 0.033	AA <sub>mp</sub> 0.045 0.044
(b) Appl ID-S ID-P P-1 P-2 P-3	S-1       AAm       0.096       0.171	of FFT S-2 AA <sub>m</sub> 0.043 0.028 0.146	BM-SM S-3 AA <sub>m</sub> 0.034 0.028 0.142	- prim S-4 AA <sub>m</sub> 0.030 0.107	S-5 AA <sub>m</sub> 0.028 0.025 0.158	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215	S-7 AA <sub>m</sub> 0.030	5-8 AA <sub>m</sub> 0.033 0.025 0.212	ne inte S-9 AA <sub>m</sub> 0.028 0.028 0.124	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168	119.5 s S-11 AA <sub>m</sub> 0.071 0.035 0.202	S-12 AA <sub>m</sub> 0.084 0.139 0.226	S-13 AA <sub>m</sub> 0.062 0.047 0.229	S-14 AA <sub>m</sub> 0.025 0.024 0.027	S-15 AA <sub>m</sub> 0.037 0.033 0.027	AA <sub>mp</sub> 0.045 0.044 0.154
(b) Appl ID-S ID-P P-1 P-2 P-3 P-4	S-1           AAm           0.096           0.096           0.171           0.227	of FFT S-2 AA <sub>m</sub> 0.043 0.028 0.146	BM-SM S-3 AA <sub>m</sub> 0.034 0.028 0.142 0.041	I - prim S-4 AA <sub>m</sub> 0.030 0.107	AAm 0.028 0.025 0.158 0.040	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076	invent S-7 AA <sub>m</sub> 0.030	ory, tin S-8 AA <sub>m</sub> 0.033 0.025 0.212 0.036	ne inte S-9 AA <sub>m</sub> 0.028 0.028 0.124 0.063	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045	119.5 s S-11 AA <sub>m</sub> 0.071 0.035 0.202 0.107	S-12 AAm 0.084 0.139 0.226 0.160	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043	S-15 AA <sub>m</sub> 0.037 0.033 0.027 0.048	AA <sub>mp</sub> 0.045 0.044 0.154 0.080
(b) Appl ID-S ID-P P-1 P-2 P-3 P-4 P-5	S-1           AAm           0.096           0.096           0.171           0.227           0.141	of FFTI S-2 AA <sub>m</sub> 0.043 0.028 0.146	BM-SM S-3 AA <sub>m</sub> 0.034 0.028 0.142 0.041	I - prim S-4 AA <sub>m</sub> 0.030 0.107	AAry sic S-5 AAm 0.028 0.025 0.158 0.040	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076 0.041	invent S-7 AA <sub>m</sub> 0.030	tory, tin S-8 AAm 0.033 0.025 0.212 0.036 0.086	S-9           AAm           0.028           0.028           0.124           0.063           0.072	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.063	119.5 s S-11 AA <sub>m</sub> 0.071 0.035 0.202 0.107	S-12 AAm 0.084 0.139 0.226 0.160	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043	S-15 AA <sub>m</sub> 0.037 0.033 0.027 0.048	AA <sub>mp</sub> 0.045 0.044 0.154 0.080 0.076
(b) Appl ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6	S-1           AAm           0.096           0.171           0.227           0.141	of FFT S-2 AA <sub>m</sub> 0.043 0.028 0.146 0.049 0.058	BM-SM S-3 AA <sub>m</sub> 0.034 0.028 0.142 0.041 0.076	I - prim S-4 AA <sub>m</sub> 0.030 0.107	ary sic S-5 AA <sub>m</sub> 0.028 0.025 0.158 0.040	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076 0.041 0.074	invent S-7 AA <sub>m</sub> 0.030 0.081	tory, tin S-8 AAm 0.033 0.025 0.212 0.036 0.086 0.050	ne inte S-9 AA <sub>m</sub> 0.028 0.028 0.124 0.063 0.072 0.055	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.063 0.055	119.5 s S-11 AA <sub>m</sub> 0.071 0.035 0.202 0.107	S-12 AAm 0.084 0.139 0.226 0.160	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071 0.085	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043 0.055	S-15 AA <sub>m</sub> 0.037 0.027 0.048 0.069	AA <sub>mp</sub> 0.045 0.044 0.154 0.080 0.076 0.072
(b) Appl- ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7	Image: Constraint of the sector of	of FFT S-2 AAm 0.043 0.028 0.146 0.049 0.058	BM-SM S-3 AAm 0.034 0.028 0.142 0.041 0.076	I - prim S-4 AAm 0.030 0.107 0.035	AAm           0.028           0.025           0.158           0.040	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076 0.041 0.074 0.051	invent S-7 AA <sub>m</sub> 0.030 0.081	tory, tin S-8 AA <sub>m</sub> 0.033 0.025 0.212 0.036 0.086 0.050 0.020	ne inte S-9 AA <sub>m</sub> 0.028 0.028 0.124 0.063 0.072 0.055	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.063 0.055 0.014	119.5 s S-11 AAm 0.071 0.035 0.202 0.107 0.060 0.048	S-12 AAm 0.084 0.139 0.226 0.160	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071 0.085	S-14 AAm 0.025 0.024 0.027 0.043 0.055	S-15 AAm 0.037 0.033 0.027 0.048 0.069	AA <sub>mp</sub> 0.045 0.044 0.154 0.080 0.076 0.072 0.039
(b) Appl ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8	S-1           AAm           0.096           0.171           0.227           0.141           0.096           0.152	of FFT S-2 AAm 0.043 0.028 0.146 0.049 0.058 0.073	BM-SM S-3 AA <sub>m</sub> 0.034 0.028 0.142 0.041 0.076 0.032	[ - prim S-4 AA <sub>m</sub> 0.030 0.107 0.035 0.091	Ary sic S-5 AA <sub>m</sub> 0.028 0.025 0.158 0.040 0.070 0.070	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076 0.041 0.074 0.051 0.094	invent S-7 AA <sub>m</sub> 0.030 0.081	tory, tin S-8 AA <sub>m</sub> 0.033 0.025 0.212 0.036 0.086 0.050 0.020 0.020 0.042	ne inte S-9 AA <sub>m</sub> 0.028 0.028 0.028 0.028 0.028 0.023 0.072 0.055	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.063 0.055 0.014 0.067	119.5 s S-11 AA <sub>m</sub> 0.071 0.035 0.202 0.107 0.060 0.048 0.077	S-12 AAm 0.084 0.139 0.226 0.160 0.159 0.133	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071 0.085 0.085	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043 0.055 0.062	S-15 AA <sub>m</sub> 0.037 0.027 0.048 0.069 0.069	AA <sub>mp</sub> 0.045  0.044  0.154  0.080  0.076  0.072  0.039  0.078
(b) Appl ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8 P-9	S-1           AAm           0.096           0.071           0.227           0.141           0.096           0.152           0.136	of FFT S-2 AAm 0.043 0.028 0.146 0.049 0.058 0.073 0.024	BM-SM S-3 AAm 0.034 0.028 0.142 0.041 0.076 0.032 0.019	I - prim S-4 AA <sub>m</sub> 0.030 0.107 0.035 0.091 0.022	ary sid S-5 AAm 0.028 0.025 0.158 0.040 0.070 0.047 0.020	e mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076 0.041 0.074 0.051 0.094 0.022	invent S-7 AA <sub>m</sub> 0.030 0.081 0.081 0.021	ory, tin S-8 AA <sub>m</sub> 0.033 0.025 0.212 0.036 0.086 0.050 0.020 0.020 0.042 0.026	ne inte S-9 AAm 0.028 0.028 0.028 0.028 0.028 0.063 0.072 0.055 0.074 0.029	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.063 0.055 0.014 0.067 0.014	119.5 s S-11 AA <sub>m</sub> 0.071 0.035 0.202 0.107 0.007 0.060 0.048 0.077 0.052	S-12 AAm 0.084 0.139 0.226 0.160 0.160 0.159 0.133 0.134	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071 0.085 0.085	S-14 AAm 0.025 0.024 0.027 0.043 0.055 0.062 0.000	S-15 AA <sub>m</sub> 0.037 0.027 0.048 0.069 0.069 0.053 0.062	AA <sub>mp</sub> 0.045  0.044  0.154  0.080  0.076  0.072  0.039  0.078  0.043
(b) Appl ID-S ID-P P-1 P-2 P-3 P-3 P-4 P-5 P-6 P-7 P-8 P-9 P-10	AAm           0.096           0.171           0.227           0.141           0.096           0.141           0.096           0.152           0.136           0.111	of FFT S-2 AA <sub>m</sub> 0.043 0.028 0.146 0.049 0.058 0.073 0.024 0.017	BM-SM S-3 AAm 0.034 0.028 0.142 0.041 0.041 0.076 0.032 0.019 0.006	- prim S-4 AAm 0.030 0.107 0.035 0.091 0.022	Ary sid S-5 AAm 0.028 0.025 0.158 0.040 0.040 0.070 0.047 0.020 0.073	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076 0.041 0.074 0.051 0.094 0.022 0.025	invent S-7 AA <sub>m</sub> 0.030 0.081 0.081 0.021	ory, tin S-8 AA <sub>m</sub> 0.033 0.025 0.212 0.036 0.086 0.050 0.020 0.042 0.026 0.048	ne inte S-9 AA <sub>m</sub> 0.028 0.028 0.028 0.028 0.063 0.072 0.055 0.074 0.029 0.043	rval 0 - S-10 AAm 0.032 0.029 0.168 0.045 0.045 0.063 0.055 0.014 0.067 0.014 0.034	119.5 s S-11 AAm 0.071 0.035 0.202 0.107 0.060 0.048 0.077 0.052 0.161	S-12 AAm 0.084 0.139 0.226 0.160 0.160 0.159 0.133 0.133 0.134 0.101	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071 0.085 0.085 0.084 0.057 0.065	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043 0.055 0.055 0.062 0.000 0.062	S-15 AA <sub>m</sub> 0.037 0.033 0.027 0.048 0.048 0.069 0.053 0.062 0.062	AA <sub>mp</sub> 0.045  0.044  0.154  0.080  0.076  0.072  0.039  0.078  0.043  0.062
(b) Appl ID-S ID-P P-1 P-2 P-3 P-3 P-3 P-3 P-4 P-5 P-5 P-6 P-7 P-6 P-7 P-8 P-9 P-10 P-11	AAm           S-1           AAm           0.096           0.171           0.227           0.141           0.096           0.152           0.136           0.130	of FFT S-2 AA <sub>m</sub> 0.043 0.028 0.146 0.049 0.058 0.073 0.073 0.024 0.017 0.038	BM-SM S-3 AA <sub>m</sub> 0.034 0.028 0.142 0.041 0.076 0.032 0.019 0.006 0.044	- prim S-4 AA <sub>m</sub> 0.030 0.107 0.007 0.035 0.091 0.022 0.290	ary side           S-5           AAm           0.028           0.025           0.158           0.040           0.070           0.047           0.020           0.073           0.064	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076 0.041 0.074 0.051 0.094 0.022 0.025 0.038	invent S-7 AA <sub>m</sub> 0.030 0.081 0.081 0.021	ory, tin S-8 AA <sub>m</sub> 0.033 0.025 0.212 0.036 0.086 0.050 0.020 0.042 0.026 0.048 0.077	ne inte           S-9           AAm           0.028           0.124           0.063           0.072           0.055           0.074           0.029           0.043	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.063 0.055 0.014 0.067 0.014 0.034 0.058	119.5 s S-11 AA <sub>m</sub> 0.071 0.035 0.202 0.107 0.060 0.048 0.077 0.052 0.161 0.068	S-12 AAm 0.084 0.139 0.226 0.160 0.159 0.159 0.133 0.133 0.134 0.101 0.091	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071 0.085 0.085 0.084 0.057 0.065 0.060	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043 0.055 0.062 0.062 0.062 0.057	S-15 AA <sub>m</sub> 0.037 0.033 0.027 0.048 0.069 0.053 0.062 0.062 0.094	AAmp 0.045 0.044 0.154 0.080 0.076 0.072 0.039 0.078 0.043 0.062 0.077
(b) Appl ID-S ID-P P-1 P-2 P-3 P-3 P-4 P-5 P-6 P-7 P-7 P-8 P-9 P-10 P-11 P-12	Cation           S-1           AAm           0.096           0.171           0.227           0.141           0.096           0.152           0.136           0.111           0.070           0.057	of FFT S-2 AA <sub>m</sub> 0.043 0.028 0.146 0.049 0.058 0.073 0.024 0.017 0.038 0.011	BM-SM S-3 AA <sub>m</sub> 0.034 0.028 0.142 0.041 0.041 0.076 0.032 0.019 0.006 0.044 0.035	- prim S-4 AA <sub>m</sub> 0.030 0.107 0.007 0.035 0.091 0.022 0.290 0.019	Ary sic S-5 AA <sub>m</sub> 0.028 0.025 0.158 0.040 0.070 0.070 0.047 0.020 0.073 0.064 0.025	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076 0.041 0.074 0.051 0.094 0.022 0.025 0.038 0.025	invent S-7 AA <sub>m</sub> 0.030 0.081 0.081 0.081 0.021	ory, tin S-8 AA <sub>m</sub> 0.033 0.025 0.212 0.036 0.086 0.050 0.020 0.020 0.042 0.026 0.048 0.077 0.007	ne inte           S-9           AAm           0.028           0.124           0.063           0.072           0.055           0.074           0.029           0.043           0.037	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.063 0.055 0.014 0.067 0.014 0.067 0.014 0.034 0.058 0.027	119.5 s S-11 AA <sub>m</sub> 0.071 0.035 0.202 0.107 0.060 0.048 0.077 0.052 0.161 0.068 0.035	S-12 AAm 0.084 0.139 0.226 0.160 0.160 0.133 0.134 0.134 0.101 0.091 0.135	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071 0.085 0.085 0.084 0.057 0.065 0.060 0.050	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043 0.043 0.055 0.062 0.000 0.062 0.057 0.019	S-15 AA <sub>m</sub> 0.037 0.033 0.027 0.048 0.069 0.069 0.062 0.062 0.094 0.066	AAmp 0.045 0.044 0.154 0.080 0.076 0.072 0.039 0.078 0.043 0.062 0.077 0.039
(b) Appl ID-S ID-P P-1 P-2 P-3 P-3 P-3 P-4 P-5 P-5 P-6 P-7 P-7 P-7 P-8 P-9 P-10 P-11 P-12 P-13	Cation           S-1           AAm           0.096           0.0171           0.227           0.141           0.096           0.152           0.136           0.111           0.070           0.133	of FFTI S-2 AA <sub>m</sub> 0.043 0.028 0.146 0.049 0.058 0.073 0.024 0.017 0.038 0.011 0.085	BM-SM S-3 AA <sub>m</sub> 0.034 0.028 0.041 0.041 0.076 0.032 0.019 0.006 0.044 0.035 0.063	- prim S-4 AA <sub>m</sub> 0.030 0.107 0.035 0.091 0.022 0.290 0.290 0.290 0.290	AAry sic S-5 AAm 0.028 0.025 0.158 0.040 0.070 0.070 0.047 0.020 0.073 0.064 0.025 0.102	le mass S-6 AA <sub>m</sub> 0.034 0.028 0.215 0.076 0.041 0.074 0.051 0.094 0.022 0.025 0.038 0.025 0.129	inveni S-7 AAm 0.030 0.030 0.081 0.081 0.081 0.021 0.030 0.030 0.000	S-8           AAm           0.033           0.025           0.212           0.036           0.020           0.036           0.020           0.020           0.020           0.022           0.020           0.042           0.026           0.042           0.027           0.026           0.027           0.0077           0.092	ne inter S-9 AAm 0.028 0.028 0.028 0.028 0.028 0.028 0.029 0.043 0.035 0.037 0.128	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.063 0.055 0.014 0.067 0.014 0.034 0.058 0.027 0.076	119.5 s S-11 AA <sub>m</sub> 0.071 0.035 0.202 0.107 0.060 0.048 0.077 0.052 0.161 0.068 0.035 0.144	S S-12 AA <sub>m</sub> 0.084 0.139 0.226 0.139 0.130 0.133 0.134 0.131 0.091 0.135 0.235	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.047 0.047 0.045 0.085 0.084 0.057 0.065 0.060 0.050 0.050	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043 0.055 0.062 0.062 0.062 0.057 0.019 0.091	S-15 AA <sub>m</sub> 0.037 0.033 0.027 0.048 0.069 0.069 0.053 0.062 0.062 0.094 0.066 0.124	AAmp 0.045 0.044 0.154 0.080 0.076 0.072 0.039 0.078 0.043 0.062 0.077 0.039 0.039 0.039 0.039
(b) Appl ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-5 P-6 P-7 P-8 P-7 P-8 P-9 P-10 P-11 P-12 P-13 P-14	Cation           S-1           AAm           0.096           0.171           0.227           0.141           0.096           0.152           0.136           0.111           0.077           0.133           0.102	0 FFTI S-2 AAm 0.043 0.028 0.146 0.049 0.058 0.073 0.024 0.017 0.038 0.011 0.085 0.124	BM-SM S-3 AA <sub>m</sub> 0.034 0.028 0.142 0.041 0.041 0.076 0.032 0.019 0.006 0.044 0.035 0.063 0.056	I - prim S-4 AA <sub>m</sub> 0.030 0.107 0.007 0.005 0.091 0.022 0.290 0.019 0.085 0.056	ary sic           S-5           AAm           0.028           0.158           0.040           0.070           0.040           0.070           0.040           0.070           0.040           0.070           0.040           0.070           0.041           0.025           0.042           0.041           0.042           0.041           0.042           0.041           0.042           0.041           0.042           0.041	S-6           AAm           0.034           0.028           0.215           0.076           0.041           0.074           0.051           0.094           0.022           0.038           0.025           0.129           0.046	inveni S-7 AAm 0.030 0.030 0.081 0.081 0.081 0.021 0.030 0.030 0.030	Sea           AAm           0.033           0.025           0.212           0.036           0.025           0.212           0.036           0.020           0.042           0.042           0.042           0.042           0.077           0.092           0.041	ne inte S-9 AA <sub>m</sub> 0.028 0.028 0.028 0.028 0.023 0.072 0.055 0.074 0.029 0.043 0.035 0.037 0.128 0.039	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.063 0.055 0.014 0.057 0.014 0.034 0.027 0.076 0.043	119.5 s           S-11           AAm           0.071           0.035           0.202           0.107           0.060           0.048           0.077           0.052           0.161           0.068           0.035           0.144           0.090	S-12           AAm           0.084           0.139           0.226           0.160           0.159           0.133           0.134           0.101           0.035           0.235           0.117	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071 0.085 0.085 0.085 0.065 0.060 0.050 0.050	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043 0.055 0.062 0.062 0.062 0.057 0.019 0.052	S-15 AA <sub>m</sub> 0.037 0.033 0.027 0.048 0.069 0.069 0.053 0.062 0.062 0.094 0.066 0.124 0.059	AAmp 0.045 0.044 0.154 0.080 0.076 0.072 0.039 0.039 0.043 0.062 0.077 0.039 0.039 0.039 0.039 0.039 0.039 0.039
(b) Appl ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-5 P-5 P-6 P-7 P-7 P-8 P-7 P-8 P-9 P-10 P-11 P-12 P-13 P-14 AA <sub>ms</sub>	Cation           S-1           AAm           0.096           0.171           0.227           0.141           0.096           0.152           0.136           0.111           0.070           0.133           0.102           0.138	of FFTI S-2 AA <sub>m</sub> 0.043 0.028 0.146 0.049 0.058 0.073 0.024 0.073 0.024 0.017 0.038 0.011 0.085 0.124 0.058	BM-SM S-3 AAm 0.034 0.028 0.142 0.041 0.041 0.076 0.032 0.019 0.006 0.044 0.035 0.063 0.056	- print S-4 AAm 0.030 0.107 0.035 0.091 0.091 0.091 0.022 0.290 0.019 0.085 0.056	ary sic           S-5           AAm           0.028           0.158           0.040           0.070           0.040           0.070           0.040           0.070           0.040           0.070           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.040           0.041           0.0425           0.102           0.108           0.063	S-6           AAm           0.034           0.028           0.215           0.076           0.041           0.051           0.094           0.022           0.038           0.025           0.038           0.025           0.129           0.046	inveni S-7 AAm 0.030 0.030 0.081 0.081 0.021 0.030 0.030 0.030 0.031 0.042	Sea           AAm           0.033           0.025           0.212           0.036           0.020           0.042           0.042           0.048           0.077           0.007           0.007           0.007           0.007           0.007           0.007           0.007	ne inte S-9 AAm 0.028 0.028 0.028 0.028 0.023 0.072 0.055 0.074 0.029 0.043 0.035 0.037 0.128 0.039 0.058	rval 0 - S-10 AA <sub>m</sub> 0.032 0.029 0.168 0.045 0.045 0.014 0.055 0.014 0.034 0.034 0.027 0.076 0.043 0.052	119.5 s 5.11 AAm 0.071 0.035 0.202 0.107 0.048 0.048 0.077 0.052 0.161 0.068 0.035 0.144 0.090	S-12 AAm 0.084 0.139 0.226 0.160 0.130 0.159 0.133 0.134 0.101 0.091 0.135 0.235 0.117	S-13 AA <sub>m</sub> 0.062 0.047 0.229 0.071 0.085 0.085 0.065 0.060 0.050 0.050 0.065 0.081	S-14 AA <sub>m</sub> 0.025 0.024 0.027 0.043 0.043 0.062 0.062 0.062 0.057 0.019 0.052 0.043	S-15 AA <sub>m</sub> 0.037 0.033 0.027 0.048 0.069 0.069 0.053 0.062 0.094 0.066 0.124 0.059 0.061	AAmp 0.045 0.044 0.154 0.080 0.076 0.072 0.039 0.039 0.043 0.062 0.077 0.0.039 0.05 0.05 0.072 0.05 0

**Table 5.** Influence of sensitive parameters on primary side mass inventory in time interval 0-119.5 s as judged by (a) original FFTBM and (b) improved FFTBM by signal mirroring

When looking the calculations, the most influenced rod surface rod temperature calculation is P-10. The  $AA_p$  and  $AA_{mp}$  indicate that the next two most influenced are the P-2 and P-3 calculation. Again both methods qualitatively give pretty similar results for the average amplitude of the participant sensitivity runs. The  $AA_t$  and  $AA_{mt}$  show that the overall influence of the sensitive parameters variations of all calculations on the output rod surface temperature

(a) Applic	ation o	of FFTB	M - ro	d surfa	ce tem	peratu	re, time	e interv	al 0 - 1	19.5 s							
ID-S	S-1	S-2	S-3	S-4	S-5	S-6	S-7	S-8	S-9	S-10	S-11	S-12	S-13	S-14	S-15		
ID-P	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	AA	1	٩Ap
P-1	0.323	0.498	0.424	0.085	0.318	0.189	0.122	0.194	0.253	0.413	0.283	0.342	0.204	0.104	0.129	0	0.259
P-2	0.323	0.403	0.608		0.493	0.312		0.301	0.282	0.495	0.220	1.679	0.097	0.099	0.174	٠	0.422
P-3	0.432	0.451	0.476	0.406	0.703	0.496		0.415	0.386	0.266	0.426	0.198	0.212	0.247	0.184		0.378
P-4	0.368		0.252		0.445	0.185		0.210	0.289	0.527	0.195	0.388	0.207	0.328	0.107		0.292
P-5	0.184	0.284				0.174		0.330	0.308	0.328						0	0.268
P-6	0.622	0.379	0.402	0.167	0.543	0.415	0.444	0.349	0.157	0.483	0.392	0.210	0.360	0.172	0.166		0.351
P-7	0.340					0.207		0.239		0.358	0.261						0.281
P-8	0.446	0.396	0.305	0.150	0.351	0.227	0.283	0.329	0.337	0.360	0.117	0.434	0.149	0.171	0.133		0.279
P-9	0.229	0.407	0.343	0.135	0.386	0.208	0.089	0.152	0.255	0.207	0.208	0.212	0.160	0.000	0.072	0	0.204
P-10	0.345	0.848	0.555		0.762	0.264		0.349	0.339	0.683	0.311	0.238	0.401	0.080	0.307		0.422
P-11	0.207	0.507	0.639	0.335	0.243	0.358		0.681	0.204	0.437	0.224	0.239	0.279	0.104	0.142		0.328
P-12	0.344	0.598	0.419	0.216	0.543	0.192	0.110	0.252	0.339	0.825	0.232	0.187	0.245	0.145	0.211		0.324
P-13	0.253	0.535	0.339	0.124	0.464	0.343	0.238	0.197	0.349	0.221	0.290	0.256	0.111	0.090	0.160	0	0.265
P-14	0.257	0.668	0.420	0.267	0.738	0.206	0.205	0.113	0.173	0.386	0.197	0.380	0.236	0.204	0.114		0.304
AAs	0.334	0.498	0.432	0.209	0.499	0.270	0.213	0.294	0.282	0.428	0.258	0.397	0.222	0.145	0.158	AA <sub>t</sub> =	0.314
		0.25-0.4	45			>0.45											
(b) A malic																	
(b) Applic	cation c	of FFTE	BM-SM	- rod s	urface	temper	rature,	time ir	nterval	0 - 119	.5 s						
ID-S	S-1	of FFTE S-2	S-3	- rod s S-4	urface S-5	temper S-6	rature, S-7	time ir S-8	nterval S-9	0 - 119 S-10	.5 s S-11	S-12	S-13	S-14	S-15		
ID-S ID-P	S-1 AA <sub>m</sub>	of FFTE S-2 AA <sub>m</sub>	S-3 AA <sub>m</sub>	- rod s S-4 AA <sub>m</sub>	urface S-5 AA <sub>m</sub>	S-6 AA <sub>m</sub>	S-7 AA <sub>m</sub>	time ir S-8 AA <sub>m</sub>	s-9 AA <sub>m</sub>	0 - 119 S-10 AA <sub>m</sub>	.5 s S-11 AA <sub>m</sub>	S-12 AA <sub>m</sub>	S-13 AA <sub>m</sub>	S-14 AA <sub>m</sub>	S-15 AA <sub>m</sub>	A	A <sub>mp</sub>
(b) Applic ID-S ID-P P-1	S-1 AA <sub>m</sub> 0.396	of FFTE S-2 AA <sub>m</sub> 0.605	S-3 AA <sub>m</sub> 0.499	- rod s S-4 AA <sub>m</sub> 0.103	S-5 AA <sub>m</sub> 0.383	S-6 AA <sub>m</sub> 0.229	S-7 AA <sub>m</sub> 0.149	time ir S-8 AA <sub>m</sub> 0.231	S-9 AA <sub>m</sub> 0.302	0 - 119 S-10 AA <sub>m</sub> 0.490	.5 s S-11 AA <sub>m</sub> 0.338	S-12 AA <sub>m</sub> 0.415	S-13 AA <sub>m</sub> 0.247	S-14 AA <sub>m</sub> 0.127	S-15 AA <sub>m</sub> 0.155	A	A <sub>mp</sub> 0.311
ID-S ID-P P-1 P-2	S-1 AA <sub>m</sub> 0.396 0.389	of FFTE S-2 AA <sub>m</sub> 0.605 0.475	8M-SM S-3 AA <sub>m</sub> 0.499 0.717	- rod s S-4 AA <sub>m</sub> 0.103	urface S-5 AA <sub>m</sub> 0.383 0.605	temper S-6 AA <sub>m</sub> 0.229 0.368	S-7 AA <sub>m</sub> 0.149	time ir S-8 AA <sub>m</sub> 0.231 0.358	S-9           AAm           0.302           0.348	0 - 119 S-10 AA <sub>m</sub> 0.490 0.542	5 s S-11 AA <sub>m</sub> 0.338 0.265	S-12 AA <sub>m</sub> 0.415 0.913	S-13 AA <sub>m</sub> 0.247 0.121	S-14 AA <sub>m</sub> 0.127 0.120	S-15 AA <sub>m</sub> 0.155 0.214	A •	A <sub>mp</sub> 0.311 0.418
(b) Applic ID-S ID-P P-1 P-2 P-3	S-1 AA <sub>m</sub> 0.396 0.389 0.508	of FFTE S-2 AA <sub>m</sub> 0.605 0.475 0.515	S-3 AA <sub>m</sub> 0.499 0.717 0.516	- rod s S-4 AA <sub>m</sub> 0.103 0.481	urface S-5 AA <sub>m</sub> 0.383 0.605 0.861	temper S-6 AA <sub>m</sub> 0.229 0.368 0.580	S-7 AA <sub>m</sub> 0.149	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486	terval S-9 AA <sub>m</sub> 0.302 0.348 0.461	0 - 119 S-10 AA <sub>m</sub> 0.490 0.542 0.305	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489	S-12 AA <sub>m</sub> 0.415 0.913 0.234	S-13 AA <sub>m</sub> 0.247 0.121 0.250	S-14 AA <sub>m</sub> 0.127 0.120 0.285	S-15 AA <sub>m</sub> 0.155 0.214 0.217	A •	Amp 0.311 0.418 0.442
ID-S ID-P P-1 P-2 P-3 P-4	S-1           AAm           0.396           0.389           0.508           0.438	of FFTE S-2 AA <sub>m</sub> 0.605 0.475 0.515	3M-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285	- rod s S-4 AA <sub>m</sub> 0.103 0.481	urface S-5 AA <sub>m</sub> 0.383 0.605 0.861 0.504	temper S-6 AA <sub>m</sub> 0.229 0.368 0.580 0.226	S-7 AA <sub>m</sub> 0.149	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255	https://www.sciences.com           S-9           AAm           0.302           0.348           0.461           0.350	0 - 119 S-10 AA <sub>m</sub> 0.490 0.542 0.305 0.557	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230	S-12 AA <sub>m</sub> 0.415 0.913 0.234 0.459	S-13 AA <sub>m</sub> 0.247 0.121 0.250 0.249	S-14 AA <sub>m</sub> 0.127 0.120 0.285 0.402	S-15 AA <sub>m</sub> 0.155 0.214 0.217 0.131	A	0.311 0.418 0.442 0.340
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5	S-1           AAm           0.396           0.389           0.508           0.438           0.227	of FFTE S-2 AA <sub>m</sub> 0.605 0.475 0.515 0.360	3M-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285	- rod s S-4 AA <sub>m</sub> 0.103 0.481	surface           S-5           AAm           0.383           0.605           0.861           0.504	temper S-6 AA <sub>m</sub> 0.229 0.368 0.580 0.226 0.213	rature, S-7 AA <sub>m</sub> 0.149	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255 0.402	https://www.sciencescolubra           S-9           AAm           0.302           0.348           0.461           0.350           0.385	0 - 119 S-10 AAm 0.490 0.542 0.305 0.557 0.400	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230	S-12 AA <sub>m</sub> 0.415 0.913 0.234 0.459	S-13 AA <sub>m</sub> 0.247 0.121 0.250 0.249	S-14 AA <sub>m</sub> 0.127 0.120 0.285 0.402	S-15 AA <sub>m</sub> 0.155 0.214 0.217 0.131	A	0.311 0.418 0.442 0.340 0.331
(b) Applic ID-S ID-P P-1 P-2 P-3 P-3 P-4 P-5 P-6	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736	of FFTE S-2 AAm 0.605 0.475 0.515 0.360 0.467	3M-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285 0.444	- rod s S-4 AA <sub>m</sub> 0.103 0.481 0.200	urface S-5 AA <sub>m</sub> 0.383 0.605 0.861 0.504	temper S-6 AA <sub>m</sub> 0.229 0.368 0.580 0.226 0.213 0.481	rature, S-7 AA <sub>m</sub> 0.149 0.526	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255 0.402 0.412	https://www.sciencesics/action/acti	0 - 119 S-10 AA <sub>m</sub> 0.490 0.542 0.305 0.557 0.400 0.525	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230	S-12 AA <sub>m</sub> 0.415 0.913 0.234 0.459 0.247	S-13 AA <sub>m</sub> 0.247 0.121 0.250 0.249 0.423	S-14 AA <sub>m</sub> 0.127 0.120 0.285 0.402 0.201	S-15 AA <sub>m</sub> 0.155 0.214 0.217 0.131 0.196	A	Amp 0.311 0.418 0.442 0.340 0.331 0.410
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-6 P-7	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736           0.411	of FFTE S-2 AA <sub>m</sub> 0.605 0.475 0.515 0.360 0.467	3M-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285 0.444	- rod s S-4 AA <sub>m</sub> 0.103 0.481 0.200	S-5           AAm           0.383           0.605           0.861           0.504	temper S-6 AA <sub>m</sub> 0.229 0.368 0.226 0.213 0.213 0.481 0.251	xature, S-7 AA <sub>m</sub> 0.149 0.526	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255 0.402 0.412 0.412	htterval           S-9           AAm           0.302           0.348           0.461           0.350           0.385           0.183	0 - 119 S-10 AA <sub>m</sub> 0.490 0.542 0.305 0.557 0.400 0.525 0.416	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230 0.230 0.452 0.316	S-12 AA <sub>m</sub> 0.415 0.913 0.234 0.459 0.247	S-13 AA <sub>m</sub> 0.247 0.121 0.250 0.249 0.423	S-14 AA <sub>m</sub> 0.127 0.120 0.285 0.402 0.201	S-15 AA <sub>m</sub> 0.155 0.214 0.217 0.131 0.196		A <sub>mp</sub> 0.311 0.418 0.442 0.340 0.331 0.410 0.336
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736           0.411           0.528	of FFTE S-2 AA <sub>m</sub> 0.605 0.475 0.515 0.360 0.360 0.467	BM-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285 0.285 0.444	- rod s S-4 AA <sub>m</sub> 0.103 0.481 0.200 0.188	Urface S-5 AAm 0.383 0.605 0.861 0.504 0.656	temper S-6 AA <sub>m</sub> 0.229 0.368 0.226 0.213 0.213 0.481 0.251 0.274	s-7           AAm           0.149           0.526           0.342	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255 0.402 0.402 0.288 0.288	S-9           AAm           0.302           0.348           0.461           0.350           0.385           0.183           0.414	0 - 119 S-10 AA <sub>m</sub> 0.490 0.542 0.305 0.557 0.400 0.525 0.416 0.449	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230 0.230 0.452 0.316 0.316	S-12 AA <sub>m</sub> 0.415 0.234 0.234 0.459 0.247	S-13 AA <sub>m</sub> 0.247 0.121 0.250 0.249 0.249 0.423	S-14 AA <sub>m</sub> 0.127 0.285 0.402 0.201 0.201	S-15 AA <sub>m</sub> 0.155 0.214 0.217 0.131 0.131 0.196	A	A <sub>mp</sub> 0.311 0.418 0.442 0.340 0.331 0.410 0.336 0.337
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-7 P-8 P-9	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736           0.411           0.528           0.293	of FFTE S-2 AAm 0.605 0.475 0.515 0.360 0.467 0.456 0.492	BM-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285 0.285 0.444 0.372 0.372	- rod s S-4 AA <sub>m</sub> 0.103 0.481 0.200 0.188 0.172	Urface S-5 AA <sub>m</sub> 0.383 0.605 0.861 0.504 0.656 0.432 0.506	temper S-6 AA <sub>m</sub> 0.229 0.368 0.226 0.213 0.213 0.213 0.251 0.251 0.274 0.264	s-7           AAm           0.149           0.526           0.342           0.114	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255 0.402 0.402 0.412 0.288 0.404 0.294	S-9           AAm           0.302           0.348           0.461           0.350           0.385           0.183           0.414           0.311	0 - 119 S-10 AA <sub>m</sub> 0.490 0.542 0.305 0.557 0.400 0.525 0.416 0.449 0.238	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230 0.230 0.452 0.316 0.316 0.149 0.264	S-12 AA <sub>m</sub> 0.415 0.913 0.234 0.459 0.459 0.247	S-13 AA <sub>m</sub> 0.247 0.121 0.250 0.249 0.249 0.249 0.202	S-14 AA <sub>m</sub> 0.127 0.285 0.285 0.402 0.201 0.209 0.000	S-15 AA <sub>m</sub> 0.155 0.214 0.217 0.131 0.196 0.196 0.165 0.091		A <sub>mp</sub> 0.311 0.418 0.442 0.340 0.331 0.410 0.336 0.337 0.255
(b) Applic ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-5 P-5 P-6 P-7 P-8 P-9 P-9 P-10	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736           0.411           0.528           0.293           0.410	of FFTF S-2 AAm 0.605 0.475 0.515 0.360 0.360 0.467 0.456 0.492 0.492 0.982	BM-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285 0.285 0.444 0.372 0.418 0.625	- rod s S-4 AA <sub>m</sub> 0.103 0.481 0.200 0.188 0.172	urface S-5 AA <sub>m</sub> 0.383 0.605 0.861 0.504 0.656 0.432 0.506 0.930	temper S-6 AA <sub>m</sub> 0.229 0.368 0.226 0.213 0.213 0.213 0.251 0.274 0.264 0.207	s-7           AAm           0.149           0.526           0.342           0.114	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255 0.402 0.402 0.412 0.288 0.404 0.194 0.402	S-9           AAm           0.302           0.348           0.461           0.350           0.385           0.183           0.414           0.311           0.391	0 - 119 S-10 AA <sub>m</sub> 0.490 0.542 0.305 0.557 0.400 0.525 0.416 0.449 0.238 0.768	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230 0.452 0.316 0.149 0.264 0.264	S-12 AA <sub>m</sub> 0.415 0.913 0.234 0.459 0.247 0.247 0.283 0.270 0.284	S-13 AA <sub>m</sub> 0.247 0.121 0.250 0.249 0.249 0.423 0.423 0.189 0.202 0.472	S-14 AA <sub>m</sub> 0.127 0.120 0.285 0.402 0.201 0.201 0.209 0.000 0.094	S-15 AA <sub>m</sub> 0.155 0.214 0.217 0.131 0.196 0.165 0.091 0.353		Amp 0.311 0.418 0.442 0.340 0.331 0.410 0.336 0.337 0.255 0.491
(b) Applie ID-S ID-P P-1 P-2 P-3 P-4 P-5 P-6 P-5 P-6 P-7 P-8 P-9 P-10 P-11	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736           0.411           0.528           0.293           0.410           0.244	of FFTF S-2 AAm 0.605 0.475 0.515 0.360 0.467 0.467 0.456 0.492 0.492 0.982 0.579	BM-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285 0.285 0.444 0.418 0.372 0.418 0.625 0.727	- rod s S-4 AA <sub>m</sub> 0.103 0.481 0.200 0.188 0.172 0.412	urface           S-5           AAm           0.383           0.605           0.861           0.504           0.656           0.432           0.506           0.930           0.270	temper S-6 AA <sub>m</sub> 0.229 0.368 0.226 0.213 0.213 0.481 0.251 0.274 0.264 0.307 0.442	s-7           AAm           0.149           0.526           0.342           0.114	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255 0.402 0.402 0.412 0.288 0.404 0.194 0.402 0.402 0.829	AAm           S-9           AAm           0.302           0.348           0.461           0.350           0.385           0.183           0.414           0.311           0.391	0 - 119 S-10 AAm 0.490 0.542 0.305 0.557 0.400 0.525 0.416 0.449 0.238 0.768 0.523	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230 0.452 0.316 0.316 0.149 0.264 0.367 0.367	S-12 AA <sub>m</sub> 0.415 0.913 0.234 0.459 0.247 0.247 0.248 0.270 0.284 0.286	S-13         AAm         0.247         0.121         0.250         0.249         0.249         0.121         0.249         0.121         0.249         0.249         0.249         0.423         0.423         0.423         0.189         0.202         0.472         0.342	S-14 AA <sub>m</sub> 0.127 0.285 0.402 0.201 0.201 0.209 0.000 0.094 0.126	S-15         AAm         0.155         0.214         0.217         0.131         0.196         0.196         0.165         0.091         0.353         0.170		Amp 0.311 0.418 0.442 0.340 0.331 0.410 0.336 0.337 0.255 0.491 0.391
(b) Applic           ID-S           ID-P           P-1           P-2           P-3           P-4           P-5           P-6           P-7           P-8           P-9           P-10           P-11           P-12	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736           0.411           0.528           0.293           0.410           0.244           0.414	of FFTE           S-2           AAm           0.605           0.475           0.515           0.360           0.467           0.466           0.492           0.982           0.579           0.680	BM-SM           S-3           AAm           0.499           0.717           0.516           0.285           0.444           0.372           0.418           0.625           0.727           0.487	- rod s S-4 AA <sub>m</sub> 0.103 0.481 0.200 0.188 0.172 0.412 0.260	s-s           AAm           0.383           0.605           0.861           0.504           0.656           0.432           0.506           0.9300           0.432           0.506           0.9300           0.270           0.667	temper S-6 AA <sub>m</sub> 0.229 0.368 0.226 0.213 0.213 0.213 0.251 0.274 0.264 0.264 0.264 0.307 0.442 0.231	number       S-7       AAm       0.149       0.149       0.526       0.342       0.114       0.128	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255 0.402 0.402 0.402 0.288 0.404 0.288 0.404 0.288 0.404 0.29 0.309	AAm           S-9           AAm           0.302           0.348           0.461           0.385           0.385           0.183           0.414           0.311           0.391           0.343	0 - 119 S-10 AAm 0.490 0.542 0.305 0.557 0.400 0.525 0.416 0.449 0.238 0.768 0.523 0.523	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230 0.452 0.316 0.316 0.149 0.264 0.367 0.278 0.278	S-12         AAm         0.415         0.913         0.234         0.459         0.459         0.247         0.247         0.483         0.270         0.284         0.286         0.227	S-13         AAm         0.247         0.121         0.250         0.249         0.423         0.423         0.423         0.189         0.202         0.472         0.342         0.293	S-14 AA <sub>m</sub> 0.127 0.285 0.402 0.201 0.201 0.209 0.000 0.094 0.126 0.170	S-15         AAm         0.155         0.214         0.217         0.131         0.196         0.196         0.195         0.191         0.165         0.091         0.3533         0.170         0.251		Amp 0.311 0.418 0.442 0.340 0.331 0.410 0.336 0.337 0.255 0.491 0.391 0.361
(b) Applic           ID-S           ID-P           P-1           P-2           P-3           P-4           P-5           P-6           P-7           P-8           P-9           P-10           P-11           P-12           P-13	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736           0.411           0.528           0.293           0.410           0.244           0.3414	of FFTE           S-2           AAm           0.605           0.475           0.515           0.360           0.467           0.456           0.492           0.982           0.579           0.680           0.604	BM-SM           S-3           AAm           0.499           0.717           0.516           0.285           0.444           0.372           0.418           0.625           0.727           0.487           0.401	- rod s S-4 AA <sub>m</sub> 0.103 0.481 0.200 0.200 0.188 0.172 0.412 0.260 0.148	S-5           AAm           0.383           0.605           0.861           0.504           0.656           0.432           0.506           0.930           0.270           0.667           0.563	temper S-6 AA <sub>m</sub> 0.229 0.368 0.226 0.213 0.213 0.213 0.251 0.274 0.264 0.264 0.231 0.241 0.231	ature, S-7 AA <sub>m</sub> 0.149 0.526 0.526 0.342 0.114 0.128 0.291	time ir S-8 AA <sub>m</sub> 0.231 0.358 0.486 0.255 0.402 0.402 0.402 0.288 0.404 0.194 0.194 0.402 0.829 0.309 0.238	Number           S-9           AAm           0.302           0.348           0.461           0.350           0.385           0.183           0.414           0.391           0.243           0.391           0.383           0.412	0 - 119 S-10 AA <sub>m</sub> 0.490 0.542 0.305 0.557 0.400 0.525 0.416 0.449 0.238 0.238 0.523 0.523 0.637	.5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230 0.482 0.316 0.316 0.367 0.264 0.367 0.278 0.282 0.351	S-12 AA <sub>m</sub> 0.415 0.234 0.234 0.234 0.247 0.247 0.247 0.284 0.270 0.284 0.227 0.292	S-13 AA <sub>m</sub> 0.247 0.121 0.250 0.249 0.249 0.242 0.423 0.472 0.342 0.342 0.293 0.134	S-14         AAm         0.127         0.285         0.402         0.201         0.201         0.209         0.000         0.094         0.126         0.120         0.126         0.120	S-15         AAm         0.155         0.214         0.217         0.131         0.165         0.196         0.165         0.091         0.353         0.170         0.251         0.177		Amp 0.311 0.418 0.442 0.340 0.331 0.410 0.336 0.337 0.255 0.491 0.391 0.361 0.313
(b) Applic           ID-S           ID-P           P-1           P-2           P-3           P-4           P-5           P-6           P-7           P-8           P-9           P-10           P-11           P-12           P-13           P-14	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736           0.411           0.528           0.241           0.410           0.244           0.302           0.330	s-2           AAm           0.605           0.475           0.515           0.360           0.467           0.467           0.456           0.492           0.982           0.579           0.604           0.799	M-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285 0.285 0.444 0.372 0.418 0.625 0.727 0.487 0.401 0.488	- rod s S-4 AAm 0.103 0.103 0.481 0.481 0.200 0.188 0.172 0.200 0.148 0.202 0.148 0.202	urface           S-5           AAm           0.383           0.605           0.861           0.504           0.656           0.432           0.506           0.930           0.270           0.667           0.563           0.937	temper S-6 AA <sub>m</sub> 0.229 0.368 0.226 0.213 0.213 0.241 0.251 0.274 0.264 0.201 0.264 0.231 0.442 0.231 0.411 0.256	s-7         AAm           0.149         0.149           0.526         0.342           0.114         0.128           0.291         0.258	time irreliance in the irrelia	Interval           S-9           AAm           0.302           0.342           0.342           0.350           0.350           0.385           0.311           0.311           0.321           0.344           0.350           0.311           0.321           0.323           0.323           0.4142	0 - 1199 S-10 0.490 0.542 0.305 0.557 0.400 0.525 0.416 0.238 0.768 0.523 0.637 0.266 0.449	5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230 0.230 0.452 0.316 0.264 0.264 0.264 0.264 0.264 0.264 0.264 0.264 0.265 0.265 0.235 0.265 0.235 0.255	S-12 AAm 0.415 0.913 0.234 0.459 0.247 0.247 0.247 0.284 0.270 0.284 0.227 0.292 0.480	S-13 AA <sub>m</sub> 0.247 0.121 0.250 0.249 0.249 0.249 0.249 0.202 0.472 0.342 0.293 0.134 0.302	S-14 AAm 0.127 0.120 0.285 0.402 0.201 0.209 0.000 0.094 0.126 0.170 0.109 0.255	S-15 AA <sub>m</sub> 0.155 0.214 0.217 0.131 0.165 0.091 0.353 0.170 0.251 0.177 0.147		Amp 0.311 0.418 0.442 0.340 0.331 0.410 0.336 0.337 0.255 0.491 0.391 0.361 0.313 0.372
(b) Applic           ID-S           ID-P           P-1           P-2           P-3           P-4           P-5           P-6           P-7           P-8           P-9           P-10           P-11           P-12           P-13           P-14           AAms	S-1           AAm           0.396           0.389           0.508           0.438           0.227           0.736           0.411           0.528           0.2410           0.244           0.410           0.302           0.330           0.402	s-2           AAm           0.605           0.475           0.515           0.360           0.475           0.360           0.467           0.456           0.492           0.982           0.579           0.604           0.799           0.585	M-SM S-3 AA <sub>m</sub> 0.499 0.717 0.516 0.285 0.285 0.444 0.372 0.418 0.625 0.727 0.488 0.401 0.488 0.498	- rod s S-4 AA <sub>m</sub> 0.103 0.103 0.481 0.481 0.200 0.188 0.172 0.260 0.148 0.295 0.251	urface S-5 AA <sub>m</sub> 0.383 0.605 0.861 0.504 0.432 0.506 0.930 0.270 0.663 0.937 0.609	tempes S-6 AA <sub>m</sub> 0.229 0.368 0.226 0.213 0.213 0.251 0.274 0.264 0.264 0.201 0.442 0.231 0.441 0.256 0.424	s-7           AAm           0.149           0.149           0.149           0.149           0.149           0.149           0.149           0.149           0.149           0.149           0.149           0.149           0.149           0.149           0.140           0.114           0.128           0.291           0.258           0.258	time irreliance in the irrelia	Interval           S-9           AAm           0.302           0.348           0.441           0.311           0.341           0.311           0.341           0.311           0.341           0.311           0.341           0.311           0.341           0.312           0.343           0.3414	0 - 1199 S-10 0.490 0.542 0.305 0.557 0.400 0.525 0.416 0.238 0.768 0.238 0.768 0.637 0.266 0.449 0.449 0.469	5 s S-11 AA <sub>m</sub> 0.338 0.265 0.489 0.230 0.452 0.316 0.264 0.264 0.264 0.264 0.264 0.264 0.264 0.264 0.264 0.264 0.264 0.265 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.316 0.265 0.265 0.316 0.265	S-12 AAm 0.415 0.913 0.234 0.459 0.247 0.247 0.284 0.280 0.284 0.286 0.227 0.292 0.480 0.382	S-13 AAm 0.247 0.121 0.250 0.249 0.423 0.423 0.423 0.422 0.472 0.342 0.293 0.134 0.302	S-14 AAm 0.127 0.120 0.285 0.402 0.201 0.209 0.000 0.094 0.126 0.170 0.255 0.175	S-15 AA <sub>m</sub> 0.155 0.214 0.217 0.131 0.196 0.165 0.091 0.353 0.170 0.251 0.177 0.147		Amp 0.311 0.418 0.442 0.340 0.331 0.410 0.336 0.337 0.255 0.491 0.391 0.361 0.313 0.372 0.372 0.372

**Table 6.** Influence of sensitive parameters on rod surface temperature in time interval 0-119.5 s as judged by (a) original FFTBM and (b) improved FFTBM by signal mirroring

is higher than on the primary side mass inventory. The ratio between  $AA_{mt}$  and  $AA_t$  is 1.17, indicating that the rod surface temperature is the least influenced by the edge effect (see also Figure 3).

## 4.3. Time dependent influence

The results presented in Section 4.2 give information on the accumulated influence of sensitive parameters for the whole transient duration (single value figures of merit). Additional insight into the results is obtained from the time dependent average amplitudes for each single variation of parameters. They provide information how the influence changes during the transient progression.

Figure 5 shows the comparison between the FFTBM and FFTBM-SM results for the P-14 sensitive calculations shown in Figure 3. It is shown how the sensitive parameter influence changes during the transient progression. The judged quantitative influence in Figure 5 reflects well what is seen during the visual observation of Figure 3, in which 5 out of 15 sensitive parameter variations for the three output parameters for the P-14 calculation are shown. Please note that the FFT based approaches are especially to be used when there are several calculations (fourteen in our case) with several sensitive parameter variations (fifteen in our case) to judge the influence of the sensitive parameters in an uniform way.

When looking the output parameter upper plenum pressure, both FFTBM (excluding period when edge effect significantly contributes to average amplitude) and FFTBM-SM clearly show when during the transient the parameter was influential. For all parameters shown in Figure 5 the major influence was during the first 30 seconds when the pressure was dropping. In the case of the S-1 parameter the influence was the largest (see Figure 5(a1)), but still not extremely significant. For parameters S-2, S-3, S-5 and S-12 the total influence is small. The values of average amplitudes up to 0.03 are small. This is confirmed by Figures 3(a2), 3(a3), 3 (a4) and 3 (a5) which show that the reference and sensitive signals for the upper plenum pressure practically match each other.

When looking the output parameter primary side mass inventory, the influence of the sensitive parameters is also quite small. Parameter S-1 is the most influential in the beginning of the transient (see also Figure 3(b1)), while all other shown sensitive parameters (S-2, S-3, S-5 and S-12) become more influential later into the transient. This is in agreement with the Figures 3(b2), 3(b3), 3(b4) and 3(b5), in which the differences in the first 20 seconds are practically not visible.

Finally, when looking the output parameter rod surface temperature, the influence of the sensitive parameters is the largest among the selected output parameters as shown by the plots and the average amplitude trends. The variation of the break flow area (S-1) having the largest influence on the upper plenum pressure has a lower influence on the rod surface temperature than the sensitive parameters S-2, S-3, S-5 and S-12. This is logically as the break area size directly impacts the upper plenum pressure.

From Figure 5(c1) it can be seen that the influence of S-1 on the rod surface temperature is judged to be in the beginning of the transient and at around 60 s. When comparing the sensitive signal to the reference signal in Figure 3(c1), in the beginning for the sensitive signal a slower temperature increase with under predicted peak and earlier temperature decrease (rod quench) at around 60 s can be seen. At other times the trends are similar. In the case of S-2 the temperature is over predicted and the quench is delayed. Therefore besides the initial jump



Figure 5. Participant P-14 influence of S-1, S-2, S-3, S-5, S-11 and S-12 sensitive parameter variations on (a) primary pressure and (b) primary side mass and (c) cladding temperature

the  $AA_m$  is still increasing till 20 s and for the time duration of the rod quench delay. For parameter S-3 it can be seen that its influence is between the S-1 and the S-2 influence, what can be confirmed from Figures 3(c1), 3(c2) and 3(c3). The influence of S-5 on the rod surface temperature is the largest what can be easily confirmed when comparing Figure 3(c4) and Figure 5(c4). The influence of S-11 is smaller than S-1 because S-11 influences only the time of rod quenching. Finally, S-12 shows that the larger discrepancy in the times when the rod quench starts causes also larger values of average amplitudes. Also when comparing the average amplitudes obtained by FFTBM and FFTBM-SM it can be seen that they agree pretty well for the output parameters primary side mass inventory and the rod surface temperature, because the edge present in the periodic signal is relatively smaller from the edge present in the upper plenum pressure periodic signal.

Figure 6(a) shows the comparison of the rod surface temperature reference calculations to experimental data. One may see that the calculations differ and that they do not exactly match the experimental data. Therefore the reader should always keep in mind that the direct comparison of sensitive signals (see Figure 6(b)) obtained by different participants could not answer in which calculation the sensitive parameter is the most influential.



Figure 6. Comparison of (a) reference calculations with experimental value and (b) sensitive runs for S-2 sensitive parameter variation

However, by calculating the average amplitude the sensitive runs by different participants could be compared as it is shown in the Figures 7, 8 and 9 for the output parameters upper plenum pressure, primary side mass inventory and rod surface temperature, respectively. For each of the output parameters the most influential parameters are shown as identified from Tables 4, 5 and 6. Figure 7 for the upper plenum pressure shows that for the majority of calculations the influences of the same sensitive parameter variation are similar. There are only a few calculations significantly deviating, for example P-4 for S-1 variation, P-3 and P-10 for S-13 variation, P-13 for S-6 variation and P-11 for S-4 variation. Figure 8 for the primary side mass inventory shows that the P3 calculation was more sensitive to variations than other

calculations. In the case of the S-4 sensitive parameter variation the P-11 calculation significantly deviates from other calculations and the reason may be that the code model is used outside its validation range [13].

Figure 9 shows that some parameters are more influential in the beginning of the transient (e.g. S-5), some in the middle of the transient (e.g. S-12) and that in the last part normally there is no significant influence (exception is the calculation P-2 for the S-12 sensitive parameter in which the rod surface temperature did not quench due to no accumulator injection when it was supposed to inject).



**Figure 7.** Upper plenum pressure time dependent AA<sub>m</sub> of participants for (a) S-1, (b) S-13, (c) S-6 and (d) S-4 sensitive parameter variations



Figure 8. Primary side mass inventory time dependent  $AA_m$  of participants for (a) S-12, (b) S-1, (c) S-11, (d) S-4, (e) S-13 and (f) S-5 sensitive parameter variations



Figure 9. Rod surface temperature time dependent  $AA_m$  of participants for (a) S-5, (b) S-2, (c) S-3, (d) S-10, (e) S-1 and (f) S-12 sensitive parameter variations

## 4.4. Discussion

In the application for each participant each sensitivity run in the set was compared to his reference calculation and the average amplitude, which is the figure of merit for FFT based approaches, was used to judge how each output parameter is sensitive to the selected input parameter. For brevity reasons, only some examples were given in Figures 6 through 9. Nevertheless, these examples are sufficient to demonstrate that the results for the whole transient interval, shown in Tables 4, 5 and 6 may not be always sufficient for judging the sensitivity. For example, for the output parameter rod surface temperature there is higher interest in the value of the maximum rod surface temperature rather the average influence on the rod surface temperature, therefore it is important to know how the influence changes with time. Also, some parameters are more influential at the beginning and the others later in the calculation.

The results suggest that the FFT based approaches are especially appropriate for a quick sensitivity analysis in which several calculations need to be compared. It is very appropriate also due to the inherent feature, which integrates the contribution of the parameter variation with progressing transient time.

In addition, the average amplitude of participant sensitivity runs for the participants ( $AA_p$  or  $AA_{mp}$ ) and the average amplitude for the same sensitive parameter ( $AA_s$  or  $AA_{ms}$ ) were calculated. These measures could be used for ranking purposes. In this way information on the most influential input parameter and which participant calculation is the most sensitive to variations is obtained. Finally, different output parameters could be compared between each other regarding the influence of input parameters of all participants ( $AA_t$  or  $AA_{mt}$ ). Quantitatively it is judged that the most influenced output parameter is the rod surface temperature and the least influenced the upper plenum pressure.

# 5. Conclusions

The study using FFTBM-SM and FFTBM was performed to show that the FFT based approaches could be used for sensitivity analyses. The LOFT L2-5 test, which simulates the large break loss of coolant accident, was used in the frame of the BEMUSE programme for sensitivity runs. In total 15 sensitivity runs were performed by 14 participants.

It can be concluded that with FFTBM-SM the analyst can get a good picture of the influence of the single parameter variation to the results throughout the transient. Some sensitive parameters are more influential at the beginning and the others later in the calculation. Due to the edge effect FFTBM-SM is advantageous for time dependent sensitivity calculations with respect to FFTBM, while for the whole transient duration (average sensitivity during whole transient) in general also FFTBM gives consistent results. FFT based approaches could be also used to quantify the influence of several parameter variations on the results. However, the influential parameters could not be identified nor the direction of the influence.

The results suggest that the FFT based approaches are especially appropriate for a quick assessment of a sensitivity analysis in which several calculations need to be compared or the influence of single sensitive parameters needs to be ranked. Such a sensitivity analysis could provide information which are the most influential parameters and how influential the input parameters are on the selected output parameters and when they influence during a transient.

# Author details

Andrej Prošek and Matjaž Leskovar

Reactor Engineering Division, Jožef Stefan Institute, Ljubljana, Slovenia

# References

- [1] Perez M, Reventos F, Batet L, Guba A, Toth I, Mieusset T, et al. Uncertainty and sensitivity analysis of a LBLOCA in a PWR Nuclear Power Plant: Results of the Phase V of the BEMUSE programme. Nucl Eng Des. 2011;241(10):4206-4222. PubMed PMID: WOS:000295956100015. English.
- [2] Prošek A, Leskovar M. Application of fast Fourier transform for accuracy evaluation of thermal-hydraulic code calculation. In: S. NG, editor. Fourier transforms - approach to scientific principles. Rijeka: In-Tech; 2011. p. 447-68.
- [3] de Crecy A, Bazin P, Glaeser H, Skorek T, Joucla J, Probst P, et al. Uncertainty and sensitivity analysis of the LOFT L2-5 test: Results of the BEMUSE programme. Nucl Eng Des. 2008;238(12):3561-3578.
- [4] Prošek A, Leskovar M, Mavko B. Quantitative assessment with improved fast Fourier transform based method by signal mirroring. Nucl Eng Des. 2008;238(10): 2668-2677.
- [5] Prošek A, D'Auria F, Mavko B. Review of quantitative accuracy assessments with fast Fourier transform based method (FFTBM). Nucl Eng Des. 2002;217(1-2):179-206.
- [6] Smith SW. The Scientist and Engineer's Guide to Digital Signal Processing. San Diego, California: California Technical Publishing, Second Edition; 1999.
- [7] Lapendes DN. Dictionary of scientific and technical terms. Second Edition ed. New York, St. Louis, San Francisco, Auckland, Bogotá, Düsseldorf, Johannesburg, London, Madrid, Mexico, Montreal, New Delhi, Panama, Paris, Sãn Paulo, Singapore, Sydney, Tokyo, Toronto, : McGraw-Hill Book Company; 1978.

- [8] Kunz RF, Kasmala GF, Mahaffy JH, Murray CJ. On the automated assessment of nuclear reactor systems code accuracy. Nucl Eng Des. 2002; 211(2-3):245-272. PubMed PMID: WOS:000174067600010. English.
- [9] Prošek A, Leskovar M. Improved FFTBM by signal mirroring as a tool for code assessment. Proceedings of the ICAPP, International congress on advances in nuclear power plants: [S. l.]: SFEN; 2007. p. 7121-1-7121-9.
- [10] Prošek A, Mavko B. A tool for quantitative assessment of code calculations with an improved fast Fourier transform based method = Orodje za kvantitativno ocenitev računalniškega izračuna z metodo na podlagi hitre Fourirjeve transformacije. Electrotechnical review. 2003; 70(5):291-296.
- [11] Prošek A. JSI FFTBM Add-in 2007 : users's manual. 2007. IJS work report IJS-DP-9752.
- [12] Prošek A, Mavko B. Quantitative assessment of time trends : influence of time window selection. In: Pevec D, Debrecin N, editors. 5th International Conference Nuclear Option in Countries with Small and Medium Electricity Grids; 16-20 May 2004; Dubrovnik, Croatia. Zagreb: Croatian Nuclear Society; 2004.
- [13] OECD/NEA. BEMUSE Phase VI Report Status report on the area, classification of the methods, conclusions and recommendations. Paris, France: OECD/NEA, 2011 NEA/CSNI/R(2011)4.
- [14] OECD/NEA. BEMUSE Phase III Report, Uncertainty and Sensitivity Analysis of the LOFT L2-5 Test. Paris, France: OECD/NEA, 2007 NEA/CSNI/R(2007)4.
- [15] OECD/NEA. BEMUSE Phase II Report, Re-Analysis of the ISP-13 Exercise, Post Test Analysis of the LOFT L2-5 Test Calculation. Paris, France: OECD/NEA, 2006 NEA/ CSNI/R(2006)2.

# Henstock-Kurzweil Integral Transforms and the Riemann-Lebesgue Lemma

Francisco J. Mendoza-Torres, Ma. Guadalupe Morales-Macías, Salvador Sánchez-Perales and Juan Alberto Escamilla-Reyna

Additional information is available at the end of the chapter

1. Introduction

Let *f* be a function defined on a closed interval [a, b] in the extended real line  $\overline{\mathbb{R}}$ , its Fourier transform at  $s \in \mathbb{R}$  is defined as

$$\hat{f}(s) = \int_{a}^{b} e^{-ixs} f(x) dx.$$
(1)

The classical Riemann-Lebesgue Lemma states that

$$\lim_{s \to \infty} \int_{a}^{b} e^{-ixs} f(x) dx = 0,$$
(2)

whenever  $f \in L^1([a, b])$ .

We consider important to study analogous results about this lemma due to the following reasons:

- The classical Riemann-Lebesgue Lemma is an important tool used when proving several results related with convergence of Fourier Series and Fourier transform. In turn, these theorems have applications in the Harmonic Analysis which has many applications in the physics, biology, engineering and others sciences. For example, it is directly applied to the study of periodic perturbations of a class of resonant problems.
- An important problem is to consider an orthogonal basis, different to the trigonometric basis, and study the Fourier expansion of a function with respect to this basis. In this case, it is obtained an expression in this way



© 2015 The Author(s). Licensee InTech. This chapter is distributed under the terms of the Creative Commons Attribution License (http://creativecommons.org/licenses/by/3.0), which permits unrestricted use, distribution, and eproduction in any medium, provided the original work is properly cited.

$$\int_{a}^{b} h(xs)f(x)dx.$$
(3)

• In some cases the expression (1) exists and the expression (2) is true even if the function *f* is not Lebesgue integrable.

Thus, a variant of the Riemann-Lebesgue Lemma is to get conditions for the functions f and h which ensure that (3) is well defined and satisfies

$$\lim_{|s| \to \infty} \int_{a}^{b} h(xs) f(x) dx = 0.$$
(4)

Some results of this type and related results are found in [1], [2], [3], and [4].

In the space of Henstock-Kurzweil integrable functions over  $\mathbb{R}$ ,  $HK(\mathbb{R})$ , the Fourier transform does not always exist. In [5] was proven that  $e^{-i(\cdot)s}f$  is Henstock-Kurzweil integrable under certain conditions and that, in general, does not satisfy the Riemann-Lebesgue Lemma. Subsequently, it was shown in [6], [3] and [4] that the Fourier transform exists and the equation (2) is true when  $-\infty = a$ ,  $b = \infty$  and f belongs to  $BV_0(\mathbb{R})$ , the space of bounded variation functions that vanish at infinity. A special case arises when f is in the intersection of functions of bounded variation and Henstock-Kurzweil integrable functions.

There exist Henstock-Kurzweil (HK) integrable functions f which  $f \in HK(I) \setminus L^1(I)$  such that (2) is not fulfilled, when I is a bounded interval. In [7], Zygmund exhibited Henstock-Kurzweil integrable functions such that their Fourier coefficients do not tend to zero. In [8] are given necessary and sufficient conditions in order to  $\int_a^b f(x)g_n(x)dx \longrightarrow \int_a^b f(x)g(x)dx$ , for all  $f \in HK([a, b])$ . Thus, we will prove that the Fourier transform has the asymptotic behavior:

$$\hat{f}(s) = o(s)$$
, as  $|s| \to \infty$ ,

where  $f \in HK(I) \setminus L^1(I)$ 

Moreover in [9], Titchmarsh proved that it is the best possible approximation for functions with improper Riemann integral.

This chapter is divided into 5 sections; we present the main results we have obtained in recent years: [3], [4], [6] and [10]. In this section we introduce basic concepts and important theorems about the Henstock-Kurzweil integral and bounded variation functions. In the second part of this study we prove some generalizations about the convergence of integrals of products in the completion of the space HK([a, b]), HK([a, b]), where [a, b]can be a bounded or unbounded interval. As a consequence, some results related to the Riemann-Lebesgue Lemma in the context of the Henstock-Kurzweil integral are proved over bounded intervals. Besides, for elements in the completion of the space of Henstock-Kurzweil integrable functions, we get a similar result to the Riemann-Lebesgue property for the Dirichlet Kernel, as well as the asymptotic behavior of the *n*-th partial sum of Fourier series. In the third section, we consider a complex function g defined on certain subset of  $\mathbb{R}^2$ . Many functions on functional analysis are integrals of the form  $\Gamma(s) = \int_{-\infty}^{\infty} f(t)g(t,s)dt$ . We study the function  $\Gamma$  when f belongs to  $BV_0(\mathbb{R})$  and  $g(t, \cdot)$  is continuous for all t. The integral we use is Henstock-Kurzweil integral. There are well known results about existence, continuity and differentiability of  $\Gamma$ , considering the Lebesgue theory. In the HK integral context there are results about this too, for example, Theorems 12.12 and 12.13 from [11]. But they all need the stronger condition that the function f(t)g(t,s) is bounded by a HK integrable function. We give more conditions for existence, continuity and differentiability of  $\Gamma$ . Finally we give some applications such as some properties about the convolution of the Fourier and Laplace transforms.

In section 4, we exhibit a family of functions in  $HK(\mathbb{R})$  included in  $BV_0(\mathbb{R}) \setminus L^1(\mathbb{R})$ . At the last section we get a version of Riemann-Lebesgue Lemma for bounded variation functions that vanish at infinity. With this result we get properties for the Fourier transform of functions in  $BV_0(\mathbb{R})$ : it is well defined, is continuous on  $\mathbb{R} - \{0\}$ , and vanishes at  $\pm\infty$ , as classical results. Moreover, we obtain a result on pointwise inversion of the Fourier transform.

#### 1.1. Basic concepts and nomenclature

We will refer to a finite or infinite interval if its Lebesgue measure is finite or infinite. Let  $I \subset \mathbb{R}$  be a closed interval, finite or infinite. A *partition* P of I is a increasing finite collection of points  $\{t_0, t_1, ..., t_n\} \subset I$  such that if I is a compact interval [a, b], then  $t_0 = a$  and  $t_n = b$ ; if  $I = [a, \infty)$ ,  $t_0 = a$ ; and if  $I = (-\infty, b]$  then  $t_n = b$ .

Let us consider  $I \subset \mathbb{R}$  as a closed interval finite. A *tagged partition* of I is a set of ordered pairs  $\{[t_{i-1}, t_i], s_i\}_{i=1}^n$  where it is assigned a point  $s_i \in [t_{i-1}, t_i]$ , which is called a *tag* of  $[t_{i-1}, t_i]$ . With this concept we define the Henstock-Kurzweil integral on finite intervals in  $\mathbb{R}$ .

**Definition 1.** The function  $f : [a, b] \to \mathbb{R}$  is Henstock-Kurzweil integrable if there exists  $H \in \mathbb{R}$  which satisfies the following: for each  $\varepsilon > 0$  exists a function  $\gamma_{\varepsilon} : [a, b] \to (0, \infty)$  such that if  $P = \{([t_{i-1}, t_i], s_i)\}_{i=1}^n$  is a tagged partition such that

$$[t_{i-1}, t_i] \subset [s_i - \gamma_{\varepsilon}(s_i), s_i + \gamma_{\varepsilon}(s_i)] \quad \text{for } i = 1, 2, \dots, n.,$$
(5)

then

$$|\Sigma_{i=1}^n f(s_i)(t_i - t_{i-1}) - H| < \varepsilon.$$

*H* is the integral of f over [a, b] and it is denoted as

$$H = \int_{a}^{b} f = \int_{a}^{b} f dt$$

It is said that a tagged partition is called  $\gamma_{\varepsilon}$ -fine if satisfies (5).

This definition can be extended on infinite intervals as follows.

**Definition 2.** Let  $\gamma : [a, \infty] \to (0, \infty)$  be a function, we will say that the tagged partition  $P = \{([t_{i-1}, t_i], s_i)\}_{i=1}^{n+1}$  is  $\gamma$ -fine *if*:

(a)  $t_0 = a, t_{n+1} = \infty$ . (b)  $[t_{i-1}, t_i] \subset [s_i - \gamma_{\varepsilon}(s_i), s_i + \gamma_{\varepsilon}(s_i)]$  for i = 1, 2, ..., n. (c)  $[t_n, \infty] \subset [1/\gamma(\infty), \infty]$ .

Put  $f(\infty) = 0$  and  $f(-\infty) = 0$ . This allows us define the integral of f over infinite intervals.

**Definition 3.** It is said that the function  $f : [a, \infty] \to \mathbb{R}$  is Henstock-Kurzweil integrable if it satisfies the Definition 1, but the partition P must be  $\gamma_{\varepsilon}$ -fine according to Definition 2.

For functions defined on  $[-\infty, a]$  or  $[-\infty, +\infty]$  the integral is defined analogously. We will denote the vector space of Henstock-Kurzweil integrable functions on *I* as HK(I)

The space of Henstock-Kurzweil integrable functions on the interval I = [a, b], finite or infinite interval, is a semi-normed space with the Alexiewicz semi-norm

$$||f||_A = \sup_{a \le x \le b} \left| \int_a^x f(t) dt \right|.$$
(6)

We denote the space of functions in HK([c, d]) for each finite interval [c, d] in I as  $HK_{loc}(I)$ .

**Definition 4.** A function  $f : I \to \mathbb{R}$  is a bounded variation function over I (finite interval) if exists a M > 0 such that

$$\operatorname{Var}(f, I) = \sup\left\{\sum_{i=1}^{n} |f(t_i) - f(t_{i-1})| : P \text{ is a partition of } I\right\} < M.$$

Its total variation over I is Var(f, I). In case I is not finite, for example  $[a, \infty]$ , it is said that  $f : [a, \infty] \to \mathbb{R}$  is a bounded variation function over I if there exists N > 0 such that

$$\operatorname{Var}(f, [a, t]) \leq N$$

for all  $t \ge a$ . The total variation of f on I is equal to

$$\operatorname{Var}(f,[a,\infty)) = \sup\left\{\operatorname{Var}(f,[a,t]): a \le t\right\}.$$
(7)

*For*  $I = (-\infty, b]$  *the considerations are analogous.* 

The set of bounded variation functions over [a, b] is denoted as BV([a, b]) and we will denote the space of functions f such that  $f \in BV([c, d])$  for each compact interval [c, d] in  $\mathbb{R}$  as  $BV_{loc}(\mathbb{R})$ . We will refer to  $BV_0(\mathbb{R})$  as the subspace of functions f belong to  $BV(\mathbb{R})$  such that vanishing at  $\pm \infty$ . At the Lemma 25 we prove that:  $HK(\mathbb{R}) \cap BV(\mathbb{R}) \subset BV_0(\mathbb{R})$ . It is not hard prove that  $BV_0(\mathbb{R}) \nsubseteq L^1(\mathbb{R})$  and  $BV_0(\mathbb{R}) \nsubseteq HK(\mathbb{R})$ . Furthermore, there are functions in  $HK(\mathbb{R})$  or  $L^1(\mathbb{R})$  but they are not in  $BV_0(\mathbb{R})$ . For example, the function f(t) defined by 0 for  $t \in (-\infty, 1)$  and 1/t for  $t \in [1,\infty)$  belongs to  $BV_0(\mathbb{R})$  but does not belong to  $L^1(\mathbb{R})$ , neither in  $HK(\mathbb{R})$ . In addition, other examples are the characteristic function of  $\mathbb{Q}$  on a compact interval and  $g(t) = t^2 \sin(\exp(t^2))$  are in  $HK(\mathbb{R}) \setminus BV_0(\mathbb{R})$ .

We consider the completion of HK([a, b]) as

$$\{[\{f_k\}]: \{f_k\} \text{ is a Cauchy sequence in } HK([a,b])\},\$$

where the convergence is respect Alexiewicz norm, and will be denoted by  $\widehat{HK([a,b])}$ . It is possible to prove that  $\widehat{HK([a,b])}$  is isometrically isomorphic to the subspace of distributions each of which is the distributional derivative of a continuous function, see [12]. The indefinite integral of  $f = [\{f_k\}] \in \widehat{HK([a,b])}$  is defined as

$$\int_a^x f = \lim_{k \to \infty} \int_a^x f_k.$$

Thus, HK([a, b]) is a Banach space with the Alexiewicz norm (6). The completion is also defined in [13]. Besides, basic results of the integral continue being true on the completion. More details see [12].

To facilitate reading, we recall the following results. The first one is a well known result, and it can be found for example in [14] and [15].

**Theorem 5.** Let f be a real function defined on  $\mathbb{N} \times \mathbb{N}$ . If  $\lim_{n \to n_0} f(k, n) = \psi(k)$  exists for each k, and  $\lim_{k \to k_0} f(k, n) = \varphi(n)$  converges uniformly on n, then

$$\lim_{k\to k_0}\lim_{n\to n_0}f(k,n)=\lim_{n\to n_0}\lim_{k\to k_0}f(k,n).$$

**Theorem 6.** [16, Theorem 33.1] Suppose X is a normed space, Y is a Banach space and that  $\{T_n\}$  is a sequence of bounded linear operators from X into Y. Then the conditions: i)  $\{||T_n||\}$  is bounded and ii)  $\{T_n(x)\}$  is convergent for each  $x \in Z$ , where Z is a dense subset on X implies that for each  $x \in X$ , the sequence  $(T_n(x))$  is convergent in Y and the linear operator  $T : X \to Y$  defined by  $T(x) = \lim_{n\to\infty} T_n(x)$  is bounded.

**Theorem 7.** [17] If g is a HK integrable function on  $[a, b] \subseteq \mathbb{R}$  and f is a bounded variation function on [a, b], then fg is HK integrable on [a, b] and

$$\left|\int_{a}^{b} fg\right| \leq \inf_{t \in [a,b]} |f(t)| \left|\int_{a}^{b} g(t)dt\right| + \|g\|_{[a,b]} \operatorname{Var}(f,[a,b]).$$

**Theorem 8.** [11, Hake's Theorem]  $\varphi \in HK([a, \infty])$  if and only if for each b,  $\varepsilon$  such that b > a $b - a > \varepsilon > 0$ , it follows that  $\varphi \in HK([a + \varepsilon, b])$  and  $\lim_{\varepsilon \to 0, b \to \infty} \int_{a+\varepsilon}^{b} \varphi(t) dt$  exists. In this case, this limit is  $\int_{a}^{\infty} \varphi(t) dt$ .

**Theorem 9.** [11, Chartier-Dirichlet's Test] Let f and g be functions defined on  $[a, \infty)$ . Suppose that

- 1.  $g \in HK([a,c])$  for every  $c \ge a$ , and G defined by  $G(x) = \int_a^x g$  is bounded on  $[a,\infty)$ .
- 2. *f* is of bounded variation on  $[a, \infty)$  and  $\lim_{x \to \infty} f(x) = 0$ .

Then  $fg \in HK([a, \infty))$ .

Moreover, by Multiplier Theorem, Hake's Theorem and Chartier-Dirichlet Test, we have the following lemma.

**Lemma 10.** Let  $f, g: [a, \infty] \to \mathbb{R}$ . Suppose that  $f \in BV_0([a, \infty])$ ,  $\varphi \in HK([a, b])$  for every b > a, and  $\Phi(t) = \int_a^t \varphi du$  is bounded on  $[a, \infty)$ . Then  $\varphi f \in HK([a, b])$ ,

$$\int_{a}^{\infty} \varphi f dt = -\int_{a}^{\infty} \Phi(t) df(t)$$

and

$$\left|\int_{a}^{\infty}\varphi fdt\right| \leq \sup_{a < t} |\Phi(t)| \operatorname{Var}(f, [a, \infty]).$$

*Similar results are valid for the cases*  $[-\infty, \infty]$  *and*  $[-\infty, a]$ *.* 

Let I = [a, b] and  $E \subset I$ . We say that the function  $F : I \to \mathbb{R}$  is in  $AC_{\delta}(E)$  if for each  $\epsilon > 0$ there exist  $\eta_{\varepsilon} > 0$  and a gauge  $\delta_{\varepsilon}$  on E such that if  $\{(x_i, y_i)\}_i^N$  is a  $(\delta_{\varepsilon}, E)$ -fine subpartition of E such that  $\sum_i^N (y_i - x_i) < \eta_{\varepsilon}$ , then  $\sum_i^N |F(x_i) - F(y_i)| < \epsilon$ . On the other hand, F belongs to the class  $ACG_{\delta}(I)$  if there exists a sequence  $\{E_n\}_1^{\infty}$  of sets in I such that  $I = \bigcup_{n=1}^{\infty} E_n$  and  $F \in AC_{\delta}(E_n)$  for each  $n \in \mathbb{N}$ . A characterization of this type of functions is the following.

**Theorem 11.** A function  $f \in HK(I)$  if and only if there exists a function  $F \in ACG_{\delta}$  such that F' = f a.e.

**Theorem 12.** [18, Theorem 4] Let  $a, b \in \mathbb{R}$ . If  $h : \mathbb{R} \times [a, b] \to \mathbb{C}$  is such that

- 1.  $h(t, \cdot)$  belongs to  $ACG_{\delta}$  on [a, b] for almost all  $t \in \mathbb{R}$ ;
- 2. and  $h(\cdot, s)$  is a HK integrable function on  $\mathbb{R}$  for all  $s \in [a, b]$ .

Then  $H := \int_{-\infty}^{\infty} h(t, \cdot) dt$  belongs to  $ACG_{\delta}$  on [a, b] and  $H'(s) = \int_{-\infty}^{\infty} D_2h(t, s) dt$  for almost all  $s \in (a, b)$ , iff,

$$\int_{s}^{t} \int_{-\infty}^{\infty} D_{2}h(t,s)dtds = \int_{-\infty}^{\infty} \int_{s}^{t} D_{2}h(t,s)dsdt$$

for all  $[s,t] \subseteq [a,b]$ . In particular,

$$H'(s_0) = \int_{-\infty}^{\infty} D_2 h(t, s_0) dt$$

when  $H_2 := \int_{-\infty}^{\infty} D_2 h(t, \cdot) dt$  is continuous at  $s_0$ .

# 2. Fourier coefficients for functions in the Henstock-Kurzweil completion.

For finite intervals, the Theorem 12.11 of [19] tells us that: In order that  $\int_a^b fg_n \rightarrow \int_a^b fg$ ,  $n \rightarrow \infty$ , whenever  $f \in HK([a,b])$ , it is necessary and sufficient that: i)  $g_n$  is almost everywhere of bounded variation on [a,b] for each n; ii)  $\sup\{||g_n||_{\infty} + ||g_n||_{BV}\} < \infty$ ; iii)  $\int_c^d g_n \rightarrow \int_c^d g$ ,  $n \rightarrow \infty$ , for each interval  $(c,d) \subset (a,b)$ . The Theorem 3 of [8] proves that above theorem is valid for infinite intervals. In this section we show that [19, Theorem 12.11] and [8, Theorem 3] are true for functions belonging to the completion of the Henstock-Kurzweil space. First, we need to prove the next lemma. The class of step functions on [a, b] will be denoted as K([a, b]).

**Lemma 13.** Let [a,b] be an infinite interval. The set K([a,b]) is dense in HK([a,b]).

*Proof.* Let  $f \in HK([a, \infty])$  and  $\epsilon > 0$  be given. By Hake's Theorem, exists  $N \in \mathbb{N}$  such that for each  $x \ge N$ ,

$$\left|\int_{x}^{\infty} f\right| < \frac{\epsilon}{2}.$$
(8)

Since K([a, N]) is dense in HK([a, N]), by Theorem 7 of [20], there exists a function  $h \in K([a, N])$  such that

$$||f-h||_{A,[a,N]} = \sup_{x \in [a,N]} \left| \int_{a}^{x} (f-h) \right| < \frac{\epsilon}{2}.$$
 (9)

Defining  $h_0 \in K([a, \infty])$  as

$$h_0(x) = \begin{cases} h(x) \text{ if } x \in [a, N] \\ 0 \text{ if } x \in (N, \infty]. \end{cases}$$

It follows, by (8) and (9), that

$$||f - h_0||_A \le \epsilon$$

Similar arguments apply for intervals as  $[-\infty, a]$  or  $[-\infty, \infty]$ .

#### 2.1. The convergence of integrals of products in the completion

The following result appears in [3]. Here, we present a detailed proof.

**Theorem 14.** Let  $[a,b] \subset \overline{\mathbb{R}}$ . In order that

$$\int_{a}^{b} fg_{n} \to \int_{a}^{b} fg, \quad n \to \infty,$$
(10)

whenever  $f \in H\widetilde{K}([a, b])$ , it is necessary and sufficient that: i)  $g_n$  is almost everywhere of bounded variation on [a, b] for each n; ii)  $\sup\{||g_n||_{\infty} + ||g_n||_{BV}\} < \infty$ ; iii)  $\int_c^d g_n \to \int_c^d g$ ,  $n \to \infty$ , for each interval  $(c, d) \subset (a, b)$ .

*Proof.* The necessity follows from [19, Theorem 12.11]. Now we will prove the sufficiency condition. Define the linear functionals  $T, T_n : H\widehat{K([a, b])} \to \mathbb{R}$  by

$$T_n(f) = \int_a^b fg_n \text{ and } T(f) = \int_a^b fg.$$
(11)

Supposing *i*) and *ii*), we have, by Multiplier Theorem, that the sequence  $\{T_n\}$  is bounded by  $\sup\{||g_n||_{\infty} + ||g_n||_{BV}\}$ . Owing to Lemma 13, the space of step functions is dense in HK([a, b]), then considering the Theorem 6 it is sufficient to prove that  $\{T_n(f)\}$  converge to T(f), for each step function *f*. First, let  $f(x) = \chi_{(c,d)}(x)$  be the characteristic function of  $(c, d) \subset [a, b]$ . Thus,

$$T_n(f) = \int_a^b \chi_{(c,d)} g_n = \int_c^d g_n$$

by the hypothesis *iii*), we have that  $\{T_n(\chi_{(c,d)})\}$  converges to  $T(\chi_{(c,d)})$ , as  $n \to \infty$ . Now, let f be a step function. Being that each  $T_n$  is a linear functional, then  $\{T_n(f)\}$  converges to T(f), as  $n \to \infty$ . Thus, the result holds.

**Remark 15.** On HK([a,b]). The hypothesis iii) can be replaced by:  $g_n$  converges pointwise to g, then the result follows from Corollary 3.2 of [21]. The result on the completion holds by Theorem 6. Note that the conditions i), ii) and iii) do not imply converges pointwise from  $\{g_n\}$  to g, see example 2 of [8].

For the case of functions defined on a finite interval we get Theorem 16, and a lemma of Riemann-Lebesgue type for functions in the Henstock-Kurzweil space completion.

**Theorem 16.** Let [a, b] be a finite interval. If i)  $g_n$  converges to g in measure on [a, b], ii) each  $g_n$  is equal to  $h_n$  almost everywhere, a normalized bounded variation function and iii) there is M > 0 such that  $Var(h_n, [a, b]) \le M$ ,  $n \ge 1$ , then for all  $f \in H\widehat{K([a, b])}$ ,

$$\int_a^b fg_n \to \int_a^b fg, \quad n \to \infty.$$

*Proof.* Let  $f \in H\widetilde{K}([a, b])$  be given, where  $f = [\{f_k\}]$ , we want to prove that

$$\lim_{n\to\infty}\lim_{k\to\infty}\int_a^b f_k g_n = \int_a^b fg.$$

Define  $f(k, n) = \int_{a}^{b} f_{k}g_{n}$ . By the hypothesis *i*) about  $(g_{n})$  we have

$$\lim_{n\to\infty}\int_a^b f_k g_n = \int_a^b f_k g.$$

Moreover

$$\lim_{k\to\infty}\lim_{n\to\infty}\int_a^b f_k g_n = \int_a^b fg,$$

by the integral definition on the completion. We will prove that  $\lim_{k\to\infty} f(k,n) = \int_a^b fg_n$  converges uniformly on n. Let  $\epsilon > 0$  be given, there exists  $k_0$  such that  $||f_k - f||_A \le \epsilon$ , if  $k \ge k_0$ . Besides, if  $k \ge k_0$ ,

$$\left|\int_{a}^{b} f_{k}g_{n} - \int_{a}^{b} fg_{n}\right| \leq ||f_{k} - f||_{A} Var(g_{n}, [a, b])$$
$$\leq M\epsilon.$$

Therefore, by Theorem 5,

$$\lim_{n \to \infty} \lim_{k \to \infty} \int_a^b f_k g_n = \int_a^b f g.$$

The following result is a "generalization" of Riemann-Lebesgue Lemma on the completion of the space HK([a, b]), over finite intervals, it also appears in [3].

**Corollary 17.** If  $\varphi : \mathbb{R} \to \mathbb{R}$  such that  $\varphi'$  exists, is bounded and  $\varphi(s) = o(s)$ , as  $|s| \to \infty$ , then for each  $f \in H\widehat{K([a, b])}$  we have the next asymptotic behavior

$$\int_{a}^{b} \varphi(st) f(t) dt = o(s), \quad as \ |s| \to \infty.$$

*Proof.* For each  $s \neq 0$  define  $\varphi_s : \mathbb{R} \to \mathbb{R}$  as  $\varphi_s(t) = \varphi(st)/s$ . In order to prove

$$\lim_{s \to \infty} \int_{a}^{b} \frac{\varphi(st)}{s} f(t) dt = 0$$

it is sufficient to show that  $\varphi_s$  fulfills the hypothesis of Theorem 16. Now, we will check item by item. *i*) Because of  $\varphi(s) = o(s)$ , as  $|s| \to \infty$  and the interval [a, b] is finite, it follows that  $\varphi_s$  converges in measure to 0. *ii*) Owing to  $\varphi'$  is bounded then, by the Mean Value Theorem, we have that  $\varphi_s \in BV([a, b])$ . *iii*)  $Var(\varphi_s, [a, b])$  is bounded uniformly by upper bound of  $\varphi'$ and a - b.

#### 2.2. Riemann-Lebesgue Property

This property establishes that  $\int_{r}^{\pi} f(t)D_{n}(t)dt \to 0$ , for each  $f \in L^{1}[-\pi,\pi]$  and  $r \in (0,\pi]$ , where  $D_{n}(t) = \frac{\sin(n+1/2)t}{\sin(t/2)}$  denotes the n-th Dirichlet Kernel of order *n*. Now, we provide an analogous result concerning the Henstock-Kurzweil completion.

**Theorem 18.** For any  $f \in HK([-\pi, \pi])$ , and  $r \in (0, \pi]$ ,

$$\lim_{n \to \infty} \frac{1}{n} \int_r^{\pi} f(t) D_n(t) dt = 0.$$
(12)

*Proof.* Note that the function  $g(t) = 1/\sin(t/2)$  is in  $BV([r, \pi])$ . Moreover, by Multiplier Theorem we have  $fg \in HK([r, \pi])$ . Hence, by Corollary 17, we get

$$\int_{r}^{\pi} f(t)g(t)\sin(n+1/2)tdt = o(n), \quad |n| \to \infty.$$

Considering an similar argument from above proof, it follows that

$$\int_{r}^{\pi} f(t) \frac{\sin(n+1/2)t}{t/2} dt = o(n), \ |n| \to \infty.$$
(13)

For  $n \in \mathbb{N} \cup \{0\}$ , we define the function  $\Phi_n(t) = \frac{\sin(n+1/2)t}{t/2}$  for  $t \neq 0$  and  $\Phi_n(0) = 2n + 1$ , it is called the discrete Fourier Kernel of order *n*. This kernel provides a very good approximation to the Dirichlet Kernel  $D_n$  for |t| < 2, but  $\Phi_n$  decreases more rapidly than  $D_n$ , see [1].

**Theorem 19.** Let  $f \in HK([0, \pi])$  and  $r \in (0, \pi]$ . Then, assuming that any of next limits exist,

$$\lim_{n \to \infty} \frac{1}{n} \int_0^r f(t) D_n(t) dt = \lim_{n \to \infty} \frac{1}{n} \int_0^r f(t) \frac{\sin(n+1/2)t}{t/2} dt.$$

*Proof.* Define  $g : [0, \pi] \to \mathbb{R}$  by

$$g(t) = \begin{cases} \frac{1}{\sin(t/2)} - \frac{1}{t/2} \text{ for } t \in (0, \pi] \\ 0 \quad \text{for} \quad t = 0. \end{cases}$$

Since  $g \in BV([0, \pi])$ ,  $fg \in H\widehat{K([0, \pi])}$ . By Corollary 17, we have

$$\lim_{n \to \infty} \frac{1}{n} \int_0^\pi f(t) \left( \frac{1}{\sin(t/2)} - \frac{1}{t/2} \right) \sin(n + 1/2) t dt = 0.$$
(14)

Now, by (14), we have

$$\lim_{n \to \infty} \frac{1}{n} \int_0^{\pi} \left( f(t) D_n(t) - f(t) \frac{\sin(n+1/2)t}{t/2} \right) dt = 0.$$

Then

$$\lim_{n \to \infty} \frac{1}{n} \left[ \int_0^r \left( f(t) D_n(t) - f(t) \frac{\sin(n+1/2)t}{t/2} \right) dt + \int_r^\pi \left( f(t) D_n(t) - f(t) \frac{\sin(n+1/2)t}{t/2} \right) dt \right] = 0$$

By Theorem 18 and (13),

$$\lim_{n \to \infty} \frac{1}{n} \int_{r}^{\pi} \left( f(t) D_{n}(t) - f(t) \frac{\sin(n+1/2)t}{t/2} \right) dt = 0.$$

Therefore, assuming that any of the limits exist, we have

$$\lim_{n \to \infty} \frac{1}{n} \int_0^r f(t) D_n(t) dt = \lim_{n \to \infty} \frac{1}{n} \int_0^r f(t) \frac{\sin(n+1/2)t}{t/2} dt.$$

The following result is a characterization of the asymptotic behavior of n - th partial sum of the Fourier series, it can be found in [3].

**Corollary 20.** Let  $f \in H\widehat{K([-\pi, \pi])}$  be  $2\pi$ -periodic. The n-th partial sum of the Fourier series at t has the following asymptotic behavior  $S_n(f, t) = o(n)$ , when  $|n| \to \infty$  iff

$$\int_0^{\pi} [f(t+u) + f(t-u)] \frac{\sin(n+1/2)u}{u} du = o(n),$$

*if*  $|n| \to \infty$ .

*Proof.* Since  $S_n(f,t) = \int_{-\pi}^{\pi} f(t+u)D_n(u)du$ , realizing a change of variable (see section 6 of [13]), then by Theorem 19 we get the result.

## 3. Henstock-Kurzweil integral transform

The results in this section are based for functions in the vector space  $BV_0(\mathbb{R})$ , and they have to [10] as principal reference.

We will introduce some additional terminology in order to facilitate the following results.

If  $g : \mathbb{R} \times \mathbb{R} \to \mathbb{C}$  is a function and  $s_0 \in \mathbb{R}$ , we say that  $s_0$  fulfills hypothesis (**H**) relative to g if:

(H) there exist  $\delta = \delta(s_0) > 0$  and  $M = M(s_0) > 0$ , such that, if  $|s - s_0| < \delta$  then

$$\left|\int_{u}^{v}g(t,s)dt\right|\leq M,$$

for all  $[u, v] \subseteq \mathbb{R}$ .

This condition plays a significant role in the following results. Also, the next theorems can be found in [10].

**Theorem 21.** Let  $f : \mathbb{R} \to \mathbb{R}$  and  $g : \mathbb{R} \times \mathbb{R} \to \mathbb{C}$  be functions. Assume that  $f \in BV_0(\mathbb{R})$ , and  $s_0 \in \mathbb{R}$  fulfills Hypothesis (**H**) relative to g, then

$$\Gamma(s) = \int_{-\infty}^{\infty} f(t)g(t,s)dt$$

is well defined for all s in a neighborhood of  $s_0$ .

Proof. Applying Theorem 9 the result holds.

**Theorem 22.** Let  $f : \mathbb{R} \to \mathbb{R}$  and  $g : \mathbb{R} \times \mathbb{R} \to \mathbb{C}$  be functions assume that

- 1. *f* belongs to  $BV_0(\mathbb{R})$ , *g* is bounded, and
- 2.  $g(t, \cdot)$  is continuous for all  $t \in \mathbb{R}$ .

If  $s_0 \in \mathbb{R}$  fulfills Hypothesis (**H**) relative to g, then the function  $\Gamma$  is continuous at  $s_0$ .

*Proof.* By Hypothesis (**H**), there exist  $\delta_1 > 0$  and M > 0, such that, if  $|s - s_0| < \delta_1$  then

$$\left|\int_{u}^{v} g(t,s)dt\right| \le M \tag{15}$$

for all  $[u, v] \subseteq \mathbb{R}$ . From Theorem 21,  $\Gamma(s)$  exists for all  $s \in B_{\delta_1}(s_0)$ .

Let an arbitrary  $\epsilon > 0$ , by Hake's theorem, there exists  $K_1 > 0$  such that

$$\left| \int_{|t| \ge u} f(t)g(t,s_0)dt \right| < \frac{\epsilon}{3} \tag{16}$$

for all  $u \ge K_1$ . On the other hand, as

$$\lim_{t\to-\infty} \operatorname{Var}(f,(-\infty,t]) = 0 \quad \text{and} \quad \lim_{t\to\infty} \operatorname{Var}(f,[t,\infty)) = 0,$$

there is  $K_2 > 0$  such that for each  $t > K_2$ ,

$$\operatorname{Var}(f, (-\infty, -t]) + \operatorname{Var}(f, [t, \infty)) < \frac{\epsilon}{3M}$$

Let  $K = \max\{K_1, K_2\}$ . From Theorem 7, it follows that for every  $v \ge K$  and every  $s \in B_{\delta_1}(s_0)$ ,

$$\left| \int_{K}^{v} f(t)g(t,s)dt \right| \leq \|g(\cdot,s)\|_{[K,v]} \left[ \inf_{t \in [K,v]} |f(t)| + \operatorname{Var}(f,[K,v]) \right]$$
$$\leq M\left[|f(v)| + \operatorname{Var}(f,[K,\infty))\right],$$

where the second inequality is true due to (15). This implies, since  $\lim_{t\to\infty} |f(t)| = 0$ , that

$$\left|\int_{K}^{\infty} f(t)g(t,s)dt\right| \leq M \cdot \operatorname{Var}(f,[K,\infty)).$$

Analogously we have that

$$\left|\int_{-\infty}^{-K} f(t)g(t,s)dt\right| \le M \cdot \operatorname{Var}(f,(-\infty,-K]).$$

Therefore, for each  $s \in B_{\delta_1}(s_0)$ ,

$$\left| \int_{|t| \ge K} f(t)g(t,s)dt \right| \le M \left[ \operatorname{Var}(f, (-\infty, -K])f + \operatorname{Var}(f, [K, \infty)) \right] < M \frac{\epsilon}{3M} = \frac{\epsilon}{3}.$$
(17)

Since *f* is  $L^1[-K, K]$ , *g* is bounded and  $g(t, \cdot)$  is continuous for all  $t \in \mathbb{R}$ . For example, using Theorem 12.12 of [11], it is easy to show that the function

$$\Gamma_K(s) = \int_{-K}^{K} f(t)g(t,s)dt, \ s \in \mathbb{R},$$

is continuous at  $s_0$ . This implies that there is  $\delta_2 > 0$  such that for every  $s \in B_{\delta_2}(s_0)$ ,

$$\left|\int_{-K}^{K} f(t)[g(t,s) - g(t,s_0)]dt\right| < \frac{\epsilon}{3}.$$
(18)

Let  $\delta = \min{\{\delta_1, \delta_2\}}$ . Then for all  $s \in B_{\delta}(s_0)$ ,

$$\begin{aligned} |\Gamma(s) - \Gamma(s_0)| &\leq \left| \int_{-K}^{K} f(t) [g(t,s) - g(t,s_0)] dt \right| \\ &+ \left| \int_{|t| \geq K} f(t) g(t,s) dt \right| + \left| \int_{|t| \geq K} f(t) g(t,s_0) dt \right| \end{aligned}$$

Thus, from (16), (17) and (18),  $|\Gamma(s) - \Gamma(s_0)| < \frac{\epsilon}{3} + \frac{\epsilon}{3} + \frac{\epsilon}{3} = \epsilon$ , for all  $s \in B_{\delta}(s_0)$ .

**Theorem 23.** Let  $a, b \in \mathbb{R}$ . If  $f : \mathbb{R} \to \mathbb{R}$  and  $g : \mathbb{R} \times [a, b] \to \mathbb{C}$  are functions such that

- 1.  $f \in BV_0(\mathbb{R})$ , g is measurable, bounded and
- 2. for all  $s \in [a, b]$ , s satisfies Hypothesis (**H**) relative to g.

Then

$$\int_{a}^{b} \int_{-\infty}^{\infty} f(t)g(t,s)dtds = \int_{-\infty}^{\infty} \int_{a}^{b} f(t)g(t,s)dsdt$$

*Proof.* From (2) and since [a, b] is compact, there exists M > 0 such that, for every  $s \in [a, b]$  and for all  $[u, v] \subseteq \mathbb{R} : \left| \int_{u}^{v} g(t, s) dt \right| \leq M$ .

For r > 0 and  $s \in [a, b]$ , let  $\Gamma_r(s) = \int_{-r}^r f(t)g(t, s)dt$ . By Theorem 7, we notice that

$$|\Gamma_r(s)| = \left| \int_{-r}^r f(t)g(t,s)dt \right|$$
  

$$\leq \|g(\cdot,s)\|_{[-r,r]} \left[ \inf_{t \in [-r,r]} |f(t)| + V_{[-r,r]}f \right]$$
  

$$\leq M[|f(0)| + Vf]$$

for all  $s \in [a, b]$ .

So, for each r > 0,  $\Gamma_r$  is HK integrable on [a, b] and is bounded for a fixed constant. Moreover, by Theorem 21 and Hake's theorem

$$\lim_{r \to \infty} \Gamma_r(s) = \Gamma(s)$$

for all  $s \in [a, b]$ .

Using the Lebesgue Dominated Convergence Theorem, we have that  $\Gamma$  is HK integrable on [a, b] and

$$\int_a^b \Gamma(s) ds = \lim_{r \to \infty} \int_a^b \Gamma_r(s) ds.$$

Now, because of *f* is Lebesgue integrable on [-r, r]; *g* is measurable and bounded; and by Fubini's theorem, it follows that

$$\int_a^b \int_{-r}^r f(t)g(t,s)dtds = \int_{-r}^r \int_a^b f(t)g(t,s)\,dsdt.$$

Consequently

$$\lim_{r\to\infty}\int_{-r}^{r}\int_{a}^{b}f(t)g(t,s)dsdt=\lim_{r\to\infty}\int_{a}^{b}\Gamma_{r}(s)ds=\int_{a}^{b}\Gamma(s)ds.$$

So by Hake's theorem,

$$\int_{-\infty}^{\infty} \int_{a}^{b} f(t)g(t,s) \, dsdt = \int_{a}^{b} \Gamma(s) ds = \int_{a}^{b} \int_{-\infty}^{\infty} f(t)g(t,s) dtds.$$

**Theorem 24.** Let  $f \in BV_0(\mathbb{R})$  and  $g : \mathbb{R} \times \mathbb{R} \to \mathbb{C}$  be a function such that its partial derivative  $D_2g$  is bounded and continuous on  $\mathbb{R} \times \mathbb{R}$ . If  $s_0 \in \mathbb{R}$  is such that

- 1. there is K > 0 for which  $||g(\cdot, s_0)||_{[u,v]} \leq K$  for all  $[u, v] \subseteq \mathbb{R}$ , and
- 2.  $s_0$  satisfies Hypothesis (**H**) relative to  $D_2g$ .

*Then*  $\Gamma$  *is derivable at*  $s_0$ *, and* 

$$\Gamma'(s_0) = \int_{-\infty}^{\infty} f(t) D_2 g(t, s_0) dt.$$
(19)

*Proof.* Using conditions (1) and (2) and the Mean Value theorem, there exist  $\delta > 0$  and M > 0 such that, for each  $s \in (s_0 - \delta, s_0 + \delta)$ ,

$$\left|\int_{u}^{v} D_2 g(t,s) dt\right| < M \text{ and } \left|\int_{u}^{v} g(t,s) dt\right| < M,$$
(20)

for all  $[u, v] \subseteq \mathbb{R}$ .

Let a, b be real numbers with  $s_0 - \delta < a < s_0 < b < s_0 + \delta$ . We use Theorem 12 to prove (19). The function  $f(t)g(t, \cdot)$  is differentiable on [a, b] for each  $t \in \mathbb{R}$ , therefore  $f(t)g(t, \cdot)$  is  $ACG_{\delta}$  on [a, b] for all  $t \in \mathbb{R}$ . By (20) and Theorem 9,  $f(\cdot)g(\cdot, s)$  is HK-integrable on  $\mathbb{R}$  for all  $s \in [a, b]$ . Then

$$\Gamma'(s_0) = \int_{-\infty}^{\infty} f(t) D_2 g(t, s_0) dt$$

when, if

$$\Gamma_2 := \int_{-\infty}^{\infty} f(t) D_2 g(t, \cdot) dt$$

is continuous at  $s_0$ , and

$$\int_{s}^{t} \int_{-\infty}^{\infty} f(t) D_2 g(t,s) dt ds = \int_{-\infty}^{\infty} \int_{s}^{t} f(t) D_2 g(t,s) ds dt$$

for all  $[s,t] \subseteq [a,b]$ . The first affirmation is true by (20) and Theorem 22, and the second affirmation is true due to (20) and Theorem 23

#### 3.1. Some applications

An important work about the Fourier transform using the Henstock-Kurzweil integral: existence, continuity, inversion theorems etc. was published in [5]. Nevertheless, there are some omissions in that results that use the Lemma 25 (a) of [5]. Also the authors of this book chapter in [6], [3] and [4] have studied existence, continuity and Riemann-Lebesgue lemma about the Fourier transform of functions belong to  $HK(\mathbb{R}) \cap BV(\mathbb{R})$  and  $BV_0(\mathbb{R})$ . Following the line of [6], in Theorem 26 we include some results from them as consequences of theorems above section.

Let *f* and *g* be real-valued functions on  $\mathbb{R}$ . The convolution of *f* and *g* is the function f \* g defined by

$$f * g(x) = \int_{-\infty}^{\infty} f(x - y)g(y)dy$$

 $\square$ 

for all x such that the integral exists. Several conditions can be imposed on f and g to guarantee that f \* g is defined on  $\mathbb{R}$ . For example, if f is HK- integrable and g is of bounded variation.

**Lemma 25.** For  $f \in HK(\mathbb{R}) \cap BV(\mathbb{R})$ ,  $\lim_{|x| \to \infty} f(x) = 0$ .

*Proof.* Since *f* is a bounded variation function on  $\mathbb{R}$  then the limit of f(x), as  $|x| \to \infty$ , exists. Suppose that  $\lim f(x) = \alpha \neq 0$ . Take  $0 < \epsilon < |\alpha|$ . There exists A > 0 such that  $\alpha - \epsilon < f(x)$ ,  $|x| \rightarrow \infty$ for all |x| > A. Observe that f(x) > 0 on  $[A, \infty)$ , so  $f \in L([A, \infty))$ . Therefore the constant function  $\alpha - \epsilon$  is Lebesgue integrable on  $[A, \infty)$ , which is a contradiction.

Observe, as consequence of above Lemma, we have that the vector space  $HK(\mathbb{R}) \cap BV(\mathbb{R})$  is contained in  $BV_0(\mathbb{R})$ . So the next theorem is an immediately consequence of above section.

**Theorem 26.** *If*  $f \in HK(\mathbb{R}) \cap BV(\mathbb{R})$ *, then* 

- 1.  $\hat{f}$  exists on  $\mathbb{R}$ .
- 2.  $\hat{f}$  is continuous on  $\mathbb{R} \setminus \{0\}$ .
- 3. If g(t) = tf(t) and  $g \in HK(\mathbb{R}) \cap BV(\mathbb{R})$ , then  $\hat{f}$  is differentiable on  $\mathbb{R} \setminus \{0\}$ , and

$$\widehat{f}'(s) = -i\widehat{g}(s)$$
, for each  $s \in \mathbb{R} \setminus \{0\}$ .

4. For  $h \in L^1(\mathbb{R}) \cap BV(\mathbb{R})$ ,  $\widehat{f * h}(s) = \widehat{f}(s)\widehat{h}(s)$  for all  $s \in \mathbb{R}$ .

Proof. We observe that

$$\left|\int_{u}^{v} e^{-its} dt\right| \leq \frac{2}{|s|},\tag{21}$$

for all  $[u, v] \subseteq \mathbb{R}$ . Thus, each  $s_0 \neq 0$  satisfies Hypothesis (**H**) relative to  $e^{-its}$ .

(a) Theorem 21 implies that  $\hat{f}(s_0)$  exists for all  $s_0 \neq 0$  and, since  $f \in HK(\mathbb{R})$ ,  $\hat{f}(0)$  exists. Therefore  $\hat{f}$  exists on  $\mathbb{R}$ .

- (b) By Theorem 22,  $\hat{f}$  is continuous at  $s_0$ , for all  $s_0 \neq 0$ .
- (c) It follows by Theorem 12 in similar way to the proof of Theorem 24.

(*d*) Let  $k(x, y) = f(y - x)e^{-iys}$ , where *s* is a fixed real number. We get, for each  $y \in \mathbb{R}$  and all  $[u,v] \subseteq \mathbb{R},$ 

$$\left| \int_{u}^{v} k(x,y) dx \right| = \left| \int_{u}^{v} f(y-x) dx \right|$$
$$= \left| \int_{y-u}^{y-v} f(z) dz \right| \leq ||f||_{A}.$$

So, every real number *y* satisfies Hypothesis (**H**) relative to *k*. Now, observe that  $h \in BV_0(\mathbb{R})$  and *k* is measurable and bounded. Thus, by Theorem 23,

$$\int_{-a}^{a} \int_{-\infty}^{\infty} h(x)k(x,y)dxdy = \int_{-\infty}^{\infty} \int_{-a}^{a} h(x)k(x,y)dydx,$$
(22)

for all a > 0.

On the other hand,

$$\begin{aligned} \left| h(x) \int_{-a}^{a} f(y-x) e^{-iys} dy \right| &\leq |h(x)| \left| \int_{-a-x}^{a-x} f(z) e^{-izs} dz \right| \\ &\leq |h(x)| \| f(\cdot) e^{-i(\cdot)s} \|_{A}. \end{aligned}$$

Since  $h \in L(\mathbb{R})$ , using Dominated Convergence theorem, it follows that

$$\widehat{f}(s)\widehat{h}(s) = \int_{-\infty}^{\infty} h(x) \int_{-\infty}^{\infty} f(y-x)e^{-iys} dy dx$$
$$= \lim_{a \to \infty} \int_{-\infty}^{\infty} h(x) \int_{-a}^{a} f(y-x)e^{-iys} dy dx.$$

Moreover, from (22), we have

$$\widehat{f}(s)\widehat{h}(s) = \lim_{a \to \infty} \int_{-a}^{a} \int_{-\infty}^{\infty} h(x)f(y-x)e^{-iys}dxdy$$
$$= \lim_{a \to \infty} \int_{-a}^{a} (f * h)(y)e^{-iys}dy.$$

We conclude, by Hake's theorem, that

$$\widehat{f * h}(s) = \widehat{f}(s)\widehat{h}(s).$$

Recall that the Laplace transform, at  $z \in \mathbb{C}$ , of a function  $f : [0, \infty) \to \mathbb{R}$  is defined as

$$L(f)(z) = \int_0^\infty f(t)e^{-zt}dt.$$

**Theorem 27.** If  $f \in HK([0,\infty)) \cap BV([0,\infty))$ , then

- 1. L(f)(z) exists for all  $z \in \mathbb{C}$ .
- 2. If F(x, y) = L(f)(x + iy), then  $F(\cdot, y)$  is continuous on  $\mathbb{R}$  for all  $y \neq 0$ , and  $F(x, \cdot)$  is continuous on  $\mathbb{R}$  for all  $x \neq 0$ .
# **4.** A set of functions in $HK(\mathbb{R}) \cap BV_0(\mathbb{R}) \setminus L^1(\mathbb{R})$

Taking into account Lemma 25, the set  $HK(\mathbb{R}) \cap BV(\mathbb{R})$  is included in  $BV_0(\mathbb{R})$  and does not have inclusion relations with  $L^1(\mathbb{R})$ . Since the step functions belong to  $HK(\mathbb{R}) \cap BV(\mathbb{R})$ , then by Lemma 13, we have that  $HK(\mathbb{R}) \cap BV(\mathbb{R})$  is dense in  $HK(\mathbb{R})$ . In this section we exhibit a set of functions in  $HK(\mathbb{R}) \cap BV_0(\mathbb{R}) \setminus L^1(\mathbb{R})$ .

**Proposition 28.** Let b > a > 0. Suppose that  $f : [a, \infty) \to \mathbb{R}$  is not identically zero, is continuous and periodic with period b - a. Let  $F(x) = \int_a^x f(t)dt$  be bounded on  $[a, \infty)$ . Moreover, assume that  $\varphi : [a, \infty) \to \mathbb{R}$  is a nonnegative and monotone decreasing function which satisfies the next conditions:

- (i)  $\lim_{t\to\infty} \varphi(t) = 0$ ,
- (*ii*)  $\varphi \notin HK([a, \infty))$ .

Then the product  $\varphi f \in HK([a,\infty)) \setminus L^1([a,\infty))$ .

*Proof.* We take  $t_o \in (a, b)$ ,  $\delta_o > 0$  and  $\gamma > 0$  such that

$$\gamma \leq |f(t)|$$
 for each  $t \in [t_o - \delta_o, t_o + \delta_o] \subset (a, b).$ 

Periodicity of f gives

 $\gamma \leq |f(t)|$ 

for each  $t \in \bigcup_{k=0}^{\infty} [t_o - \delta_o + k(b-a), t_o + \delta_o + k(b-a)]$ . Therefore,

$$\int_{a}^{b+n(b-a)} \varphi(t)|f(t)|dt \geq \gamma \sum_{k=0}^{n} \int_{t_{o}-\delta_{o}+k(b-a)}^{t_{o}+\delta_{o}+k(b-a)} \varphi(t)dt$$
$$\geq \gamma \sum_{k=0}^{n} \int_{t_{o}-\delta_{o}+k(b-a)}^{t_{o}+\delta_{o}+k(b-a)} \varphi(t_{o}+\delta_{o}+k(b-a))dt$$
$$= \gamma(2\delta_{o}) \sum_{k=0}^{n} \varphi(t_{o}+\delta_{o}+k(b-a)).$$
(23)

Also,

$$\int_{a}^{b+n(b-a)} \varphi(t)dt \leq \sum_{k=0}^{n} \int_{a+k(b-a)}^{b+k(b-a)} \varphi(t)dt$$

$$\leq \sum_{k=0}^{n} \varphi(a+k(b-a)) \int_{a+k(b-a)}^{b+k(b-a)} dt$$

$$\leq (b-a)\varphi(a) \qquad (24)$$

$$+(b-a) \sum_{k=1}^{n} \varphi(t_{o}+\delta_{o}+(k-1)(b-a)).$$

Because of  $\varphi \notin HK([a,\infty])$ , we get  $\lim_{n\to\infty} \int_a^{b+n(b-a)} \varphi(t)dt = \infty$ . Thus, equations (23) and (24) imply  $\varphi f \notin L^1([a,\infty)]$ . On the other hand, by Chartier-Dirichlet's Test of [11], the function  $\varphi f$  belongs to  $HK([a,\infty))$ .

**Corollary 29.** Let  $\alpha$ ,  $\beta$  be positive numbers such that  $\alpha + \beta > 1$  with  $\beta \le 1$ . Suppose a > 0 and  $f : [a, \infty) \to \mathbb{R}$  obeys the hypotheses of Proposition 28. Then, the function  $f_{\alpha,\beta} : [a^{1/\alpha}, \infty) \to \mathbb{R}$  defined by

$$f_{\alpha,\beta}(t) = \frac{f(t^{\alpha})}{t^{\beta}}$$
(25)

is in  $HK([a^{1/\alpha},\infty)) \setminus L^1([a^{1/\alpha},\infty))$ .

*Proof.* The change of variable  $u = t^{\alpha}$  gives,

$$\int_{a^{\frac{1}{\alpha}}}^{\infty} \frac{f(t^{\alpha})}{t^{\beta}} dt = \int_{a}^{\infty} \frac{f(u)}{u^{\frac{\beta-1}{\alpha}+1}} du.$$
(26)

The hypotheses for  $\alpha$ ,  $\beta$  imply that the function  $\varphi(u) = u^{-[\frac{(\beta-1)}{\alpha}+1]}$  satisfies the conditions of Proposition 28. Then,  $\varphi f \in HK([a,\infty) \setminus L^1([a,\infty))$ , satisfying the statement of the corollary.

**Proposition 30.** Let  $\beta > \alpha > 0$  be fixed with  $\beta + \alpha > 1$ . Suppose  $f : [a, \infty) \to \mathbb{R}$  is a bounded and continuous function, with bounded derivative. Then the function  $f_{\alpha,\beta} : [a^{1/\alpha}, \infty) \to \mathbb{R}$ , defined by  $f_{\alpha,\beta}(t) = f(t^{\alpha})/t^{\beta}$ , belongs to the space  $BV([a^{1/\alpha}, \infty))$ .

*Proof.* Let  $M_1$  and  $M_2$  be bounds for f and f', respectively. We have,

$$f'_{\alpha,\beta}(t) = rac{lpha f'(t^{lpha})}{t^{eta-lpha+1}} - rac{eta f(t^{lpha})}{t^{eta+1}},$$

which gives

$$\left|f_{\alpha,\beta}'(t)\right| \leq \frac{\alpha M_2}{t^{\beta-\alpha+1}} + \frac{\beta M_1}{t^{\beta+1}}.$$

Now, take  $x > a^{\frac{1}{\alpha}}$ . Since  $\beta - \alpha > 0$ , then

$$\frac{\alpha M_2}{t^{\beta-\alpha+1}} + \frac{\beta M_1}{t^{\beta+1}} \in L^1([a^{\frac{1}{\alpha}}, x))$$

A straightforward application of the Theorem 7.7 of [11] implies  $f'_{\alpha,\beta} \in L^1([a^{1/\alpha},x))$ . Moreover

$$\begin{split} \int_{a^{\frac{1}{\alpha}}}^{x} |f_{\alpha,\beta}'(t)| dt &\leq \alpha M_2 \int_{a^{\frac{1}{\alpha}}}^{x} t^{-\beta+\alpha-1} dt \\ &+\beta M_1 \int_{a^{\frac{1}{\alpha}}}^{x} t^{-\beta-1} dt \\ &= -\frac{\alpha M_2}{\beta-\alpha} \left(\frac{1}{x^{\beta-\alpha}} - \frac{1}{a^{\frac{\beta-\alpha}{\alpha}}}\right) \\ &-M_1 \left(\frac{1}{x^{\beta}} - \frac{1}{a^{\frac{\beta}{\alpha}}}\right) \\ &\leq \frac{\alpha M_2}{\beta-\alpha} \frac{1}{a^{\frac{\beta-\alpha}{\alpha}}} + \frac{M_1}{a^{\frac{\beta}{\alpha}}} \,. \end{split}$$

These estimates together with the Theorem 7.5 of [11] imply,

$$V(f_{\alpha,\beta}; [a^{\frac{1}{\alpha}}, x)) \le \frac{\alpha M_2}{\beta - \alpha} \frac{1}{a^{\frac{\beta - \alpha}{\alpha}}} + \frac{M_1}{a^{\frac{\beta}{\alpha}}}.$$
(27)

If *x* tends to  $\infty$ , one gets  $f_{\alpha,\beta} \in BV([a^{1/\alpha},\infty))$ .

Corollary 29 and Proposition 30 provide us Henstock-Kurzweil integrable functions defined on unbounded intervals which are not Lebesgue integrable.

**Corollary 31.** Let a,  $\alpha$ ,  $\beta$  be such that: 0 < a,  $0 < \alpha < \beta \le 1$  and  $1 < \beta + \alpha$ . Suppose that  $f : [a, \infty) \to \mathbb{R}$  satisfies both the hypotheses of Corollary 29 and Proposition 30. Then, the function  $f_{\alpha,\beta}$  belongs to  $HK([a^{1/\alpha},\infty)) \cap BV([a^{1/\alpha},\infty)) \setminus L^1([a^{1/\alpha},\infty))$ .

Taking into account the above functions we have the following corollary.

**Corollary 32.** Let a,  $\alpha$ ,  $\beta$  be such that: 0 < a,  $0 < \alpha < \beta \le 1$  and  $1 < \beta + \alpha$ , and let h in  $BV([-a^{1/\alpha}, a^{1/\alpha}])$ . Suppose that  $f : [a, \infty) \to \mathbb{R}$  satisfies both the hypotheses of Corollary 29 and Proposition 30. Then  $f : \mathbb{R} \to \mathbb{R}$  defined by

$$g(t) = \begin{cases} h(t) & \text{if } t \in (-a^{1/\alpha}, a^{1/\alpha}), \\ \frac{f(|t|^{\alpha})}{|t|^{\beta}} & \text{if } f \in (-\infty, -a^{1/\alpha}] \cup [a^{1/\alpha}, \infty) \end{cases}$$

is in  $HK(\mathbb{R}) \cap BV(\mathbb{R}) \setminus L(\mathbb{R})$ .

**Example 33.** Let us consider the trigonometric functions sin(t) and cos(t). Then the following family of functions satisfies the hypotheses of Theorem 34.

$$\begin{aligned} \sin^{\alpha}_{\beta} : \mathbb{R} \to \mathbb{R}; \quad \sin^{\alpha}_{\beta}(t) = \chi_{1,\alpha}(t) \frac{\sin(t^{\alpha})}{t^{\beta}}, \\ \cos^{\alpha}_{\beta} : \mathbb{R} \to \mathbb{R}; \quad \cos^{\alpha}_{\beta}(t) = \chi_{2,\alpha}(t) \frac{\cos(t^{\alpha})}{t^{\beta}}. \end{aligned}$$

Here  $\chi_{1,\alpha}$  and  $\chi_{2,\alpha}$  are the characteristic functions of the intervals  $[\pi^{1/\alpha},\infty)$  and  $[(\pi/2)^{1/\alpha},\infty)$ , respectively. The numbers  $\alpha$ ,  $\beta$  are taken as in Corollary 31.

From the above example belongs to  $HK(\mathbb{R}) \cap BV(\mathbb{R}) \setminus L(\mathbb{R})$ . By the Multiplier theorem it follows that  $HK(\mathbb{R}) \cap BV(\mathbb{R}) \subset L^2(\mathbb{R})$ , so the above function is in  $BV_0(\mathbb{R}) \cap L^2(\mathbb{R}) \setminus L(\mathbb{R})$ . Therefore, there exist functions in  $L^2(\mathbb{R}) \setminus L(\mathbb{R})$  such that their Fourier transforms exist as in (1), as an integral in HK sense.

# **5.** The Riemann-Lebesgue Lemma and the Dirichlet-Jordan Theorem for $BV_0$ functions

The Riemann-Lebesgue lemma is a fundamental result of the Harmonic Analysis. An novel aspect is the validity of this lemma for functions which are not Lebesgue integrable, since this fact could help to expand the space of functions where the inversion of the Fourier transform is possible. In this section we prove a generalization of the Riemann-Lebesgue Lemma for functions of bounded variation which vanish at infinity. As consequence, it is obtained a proof of the Dirichlet-Jordan theorem for this kind of functions. This theorem provides a pointwise inversion of the Fourier transform.

We observe that the implications 1 and 2 of Theorem 26 are particularizations of the next result.

**Theorem 34** (Generalization of Riemann-Lebesgue Lemma). Let  $\varphi \in HK_{loc}(\mathbb{R})$  be a function such that  $\Phi(t) = \int_0^t \varphi(x) dx$  is bounded function on  $\mathbb{R}$ . If  $f \in BV_0(\mathbb{R})$ , then the function  $H(w) = \int_{-\infty}^{\infty} f(t)\varphi(wt) dt$  is defined on  $\mathbb{R} \setminus \{0\}$ , it is continuous and

$$\lim_{|w|\to\infty}H(w)=0$$

*Proof.* Given  $w \in \mathbb{R}$ , we define  $\varphi_w(t) = \varphi(wt)$ . Because of  $\varphi \in HK_{loc}(\mathbb{R})$ , then  $\varphi$  and  $\varphi_w$  are in HK([0, b]), for b > 0. By Jordan decomposition, there exist functions  $f_1$  and  $f_2$  which are nondecreasing functions belonging to  $BV_0(\mathbb{R})$  such that  $f = f_1 - f_2$ . Hence, by Chartier-Dirichlet's Test,  $f\varphi_w \in HK([0, \infty])$ . By applying the Multiplier Theorem and supposing  $w \neq 0$ , it follows

$$\int_{0}^{\infty} f(t)\varphi(wt)dt = -\int_{0}^{\infty} \frac{\Phi(wt)}{w} df(t)$$

$$= -\int_{0}^{\infty} \frac{\Phi(wt)}{w} df_{1}(t)$$

$$+ \int_{0}^{\infty} \frac{\Phi(wt)}{w} df_{2}(t),$$
(28)

where  $df_i(t)$  is the Lebesgue-Sieltjes measure generated by  $f_i$ , i = 1, 2. Let  $\beta$  a positive number and let M the upper bound of  $|\Phi|$ . For  $w \in [\beta, \infty)$  we have that

$$\left|\frac{\Phi(wt)}{w}\right| \le \frac{M}{\beta}.$$
(29)

Since  $\Phi(wt)/w$  is continuous over  $[\beta, \infty)$  and the measures  $df_i(t)$  are finite, then by the Dominated Convergence Theorem applied to right side integrals in (28), it follows that

$$\lim_{w\to w_0} H(w) = H(w_0),$$

for each  $w_0 \in [\beta, \infty)$ . Since  $\beta$  is arbitrary, we obtain the continuity of H on  $(0, \infty)$ . Moreover, by (28), we have for  $w \in (0, \infty)$  that

$$\left|\int_0^\infty f(t)\varphi(wt)dt\right| \leq \frac{M}{|w|} Var(f;[0,\infty]).$$

Thus, we conclude that

$$\lim_{|w|\to\infty}\int_0^\infty f(t)\varphi(wt)dt=0.$$

To complete the proof, we use similar arguments for the interval  $(-\infty, 0]$ .

The above theorem confirms that  $H \in C_0(\mathbb{R} \setminus \{0\})$ , for each  $f \in BV_0(\mathbb{R})$ . As corollary we have the Riemann-Lebesgue Lemma.

**Corollary 35.** If  $f \in BV_0(\mathbb{R})$ , then  $\hat{f} \in C_0(\mathbb{R} \setminus \{0\})$ .

We know that if  $g, h \in BV([a, \infty])$  then  $gh \in BV([a, \infty])$ . Employing this fact and Theorem 34 we get the following corollary.

**Corollary 36.** Suppose that  $\delta, \alpha > 0$  and  $f \in BV(\mathbb{R})$ , then

$$\lim_{M \to \infty} \int_{\delta}^{\infty} \frac{f(t)}{t^{\alpha}} e^{-iMt} dt = 0.$$

The Sine Integral is defined as

$$Si(x) = \frac{2}{\pi} \int_0^x \frac{\sin t}{t} dt,$$

which has the properties:

- 1. Si(0) = 0,  $\lim_{x \to \infty} Si(x) = 1$  and
- 2.  $Si(x) \leq Si(\pi)$  for all  $x \in [0, \infty]$ .

We use the Sine Integral function in the proof of the following lemma.

**Lemma 37.** Let  $\delta > 0$ . If  $f \in BV_0(\mathbb{R})$ , then

$$\lim_{\varepsilon \to 0} \int_{\delta}^{\infty} f(t) \frac{\sin \varepsilon t}{t} dt = 0.$$

Proof. By Lemma 10 we have

$$\left| \int_{\delta}^{\infty} \frac{\sin \varepsilon t}{t} f(t) dt \right| \le \left| \int_{\delta}^{\infty} \left( \int_{\delta \varepsilon}^{t\varepsilon} \frac{\sin u}{u} du \right) df(t) \right|.$$
(30)

Since for each  $t \in [a, \infty)$ :  $\lim_{\varepsilon \to 0} \int_{\delta\varepsilon}^{t\varepsilon} \frac{\sin u}{u} du = 0$  and  $\left| \int_{\delta\varepsilon}^{t\varepsilon} \frac{\sin u}{u} du \right| \le \pi Si(\pi)$  for all  $\varepsilon > 0$ . Then, we obtain the result applying the Lebesgue Dominated Convergence theorem to the integral on the right in (30).

**Lemma 38.** Suppose that  $0 < \alpha < \beta$  or  $\alpha < \beta < 0$ . If  $f \in BV_0(\mathbb{R})$ , then for all  $s \in [\alpha, \beta]$  we have

$$\lim_{\substack{a \to -\infty \\ b \to \infty}} \int_{\alpha}^{\beta} e^{ixs} \int_{a}^{b} f(t) e^{-ist} dt ds = \int_{\alpha}^{\beta} e^{ixs} \int_{-\infty}^{\infty} f(t) e^{-ist} dt ds.$$
(31)

*Proof.* We will do the proof for  $0 < \alpha < \beta$ . Let  $\widehat{f}_{0b}(s) = \int_0^b f(t)e^{-ist}dt$  and  $\widehat{f}_0(s) = \int_0^\infty f(t)e^{-ist}dt$ , which are continuous on  $\mathbb{R} \setminus \{0\}$ . Therefore the integrals in (31) exist. We know that there is R > 0 such that  $|f(t)| \leq R$  for all  $t \in \mathbb{R}$ , and that for any b > 0:  $V(f; [0, b]) \leq V(f; [0, \infty))$ . For each  $s \in [\alpha, \beta]$  the Multiplier theorem implies

$$\left|\widehat{f}_{0b}(s)\right| \leq \frac{2}{\alpha} \left\{ R + V(f; [0, \infty)) \right\} = N.$$

This inequality implies that for any b > 0 and all  $s \in [\alpha, \beta] : |e^{ixs} \hat{f}_{0b}(s)| \le N$ , for each  $x \in \mathbb{R}$ . Applying the theorem of Hake we have:  $\lim_{b\to\infty} \hat{f}_{0b}(s) = \hat{f}_0(s)$ . Then, by the Lebesgue Dominated Convergence theorem,

$$\lim_{b\to\infty}\int_{\alpha}^{\beta}e^{ixs}\widehat{f}_{0b}(s)ds=\int_{\alpha}^{\beta}e^{ixs}\widehat{f}_{0}(s)ds.$$

To conclude the proof, we follow a similar process over the interval [a, 0] leading a to minus infinity.

To obtain the Dirichlet-Jordan theorem we state the following lemma [22, Theorem 11.8].

**Lemma 39.** Let  $\delta > 0$ . If g is of bounded variation on  $[0, \delta]$ , then

$$\lim_{M \to \infty} \frac{2}{\pi} \int_0^{\delta} g(t) \frac{\sin Mt}{t} dt = g(0+)$$

**Theorem 40** (Dirichlet-Jordan Theorem). *If* f *is a function in*  $BV_0(\mathbb{R})$ *, then, for each*  $x \in \mathbb{R}$ *,* 

$$\lim_{\substack{M\to\infty\\\varepsilon\to 0}} \frac{1}{2\pi} \int_{\substack{\varepsilon<|s|< M}} e^{ixs} \widehat{f}(s) ds = \frac{1}{2} \{ f(x+0) + f(x-0) \}.$$
(32)

*Proof.* Let g(x,t) = f(x-t) + f(x+t) and suppose that  $\delta > 0$ . By Fubini's theorem for the Lebesgue integral [22, Theorem 15.7] at  $[-M, -\varepsilon] \times [a, b]$  and  $[\varepsilon, M] \times [a, b]$  and Lema 38, we have

$$\int_{\varepsilon <|s| < M} e^{ixs} \int_{-\infty}^{\infty} f(t)e^{-ist}dtds = \lim_{\substack{a \to -\infty \\ b \to \infty}} \left( \int_{-M}^{-\varepsilon} + \int_{\varepsilon}^{M} \right) e^{ixs} \int_{a}^{b} f(t)e^{-ist}dtds$$
$$= \lim_{\substack{a \to -\infty \\ b \to \infty}} \int_{a}^{b} f(t) \left( \int_{-M}^{-\varepsilon} + \int_{\varepsilon}^{M} \right) e^{is(x-t)}dsdt$$
$$= \int_{-\infty}^{\infty} f(t) \left( \int_{-M}^{-\varepsilon} + \int_{\varepsilon}^{M} \right) e^{is(x-t)}dsdt$$
$$= 2 \int_{0}^{\infty} \frac{g(x,t)}{t} (\sin M t - \sin \varepsilon t)dt$$
$$= 2 \int_{0}^{\delta} \frac{g(x,t)}{t} (\sin M t - \sin \varepsilon t)dt$$
$$+ 2 \int_{0}^{\delta} \frac{g(x,t)}{t} (\sin M t - \sin \varepsilon t)dt.$$

In  $[\delta, \infty]$ , by Corollary 36 and Lemma 37, we get

$$\lim_{M \to \infty, \varepsilon \to 0} \int_{\delta}^{\infty} \frac{g(x, t)}{t} (\sin M \ t - \sin \varepsilon t) dt = 0.$$
(33)

In  $[0, \delta]$ , applying the Lebesgue Dominate Convergence theorem,

$$\lim_{\varepsilon \to 0} \int_0^{\delta} \frac{g(x,t)}{t} \sin \varepsilon t dt = 0.$$
(34)

Now, by Lemma 39,

$$\lim_{M \to \infty} \int_0^{\delta} g(x,t) \frac{\sin Mt}{t} dt = g(x,0+) = \frac{\pi}{2} \left[ f(x-0) + f(x+0) \right].$$

 $\square$ 

We conclude the proof combining (33), (34) and the above expression.

We observe that the classical theorem of Dirichlet-Jordan on  $L(\mathbb{R})$  is a particular case of Theorem 40. Taking into account that  $HK(\mathbb{R}) \cap BV(\mathbb{R}) \subset BV_0(\mathbb{R})$ , then from Theorem 34 and Theorem 40 we get that if  $f \in HK(\mathbb{R}) \cap BV(\mathbb{R})$ , then its Fourier transform  $\hat{f}(s)$  exists in each  $s \in \mathbb{R}$ ;  $\hat{f} \in C_0(\mathbb{R} \setminus \{0\})$ , and the expression (32) holds for each  $x \in \mathbb{R}$ .

**Corollary 41.** There exist functions in  $L^2(\mathbb{R}) \setminus L(\mathbb{R})$  such that their Fourier transforms exist as in (1) and, for each  $x \in \mathbb{R}$ , the expression (32) is true.

#### 6. Conclusions

We present theorems about convergence of integrals of products in the completion of HK(I), which those we have a version of Riemann-Lebesgue Lemma (over compact intervals) and analogous results at Riemann-Lebesgue property, a characterization of behavior of *n*-th partial sum of the Fourier series. Moreover, we have gotten basic properties (existence as integral, continuity, asymptotic behavior) about Fourier transform using Henstock-Kurzweil Integral, for this was necessary to get a generalization of Riemann-Lebesgue Lemma over  $BV_0(\mathbb{R})$ , in particular those characteristics are valid over  $HK(\mathbb{R}) \cap BV(\mathbb{R})$ . This intersection does not have relation inclusion with Lebesgue integrable functions space, we give a set of functions such that it belongs to  $HK(\mathbb{R}) \cap BV(\mathbb{R}) \setminus L(\mathbb{R})$ . Finally we have a generalization of Dirichlet-Jordan over  $BV_0(\mathbb{R})$ .

#### Acknowledgments

The authors acknowledge the support provided by the VIEP-BUAP, Puebla, Mexico.

#### Author details

Francisco J. Mendoza-Torres<sup>1</sup>, Ma. Guadalupe Morales-Macías<sup>2</sup>, Salvador Sánchez-Perales<sup>3</sup>, and Juan Alberto Escamilla-Reyna<sup>1</sup>

1 Facultad de Ciencias Físico-Matemáticas, Benemérita Universidad Autónoma de Puebla, Puebla, Mexico

2 Departamento de Matemáticas, Universidad Autónoma Metropolitana-Iztapalapa, México, D. F., Mexico

3 Instituto de Física y Matemáticas, Universidad Tecnológica de la Mixteca, Oaxaca, Mexico

#### References

- [1] Bachman G, Narici L, Beckenstein E. Fourier and Wavelet Analysis. New York: Springer-Verlag; 1991.
- [2] Kahane Ch. Generalizations of the Riemann-Lebesgue and Cantor-Lebesgue lemmas. Czech. Math. J. 1980;30(1):108-117. Available from: http://tinyurl.com/myrs3wp
- [3] Mendoza-Torres FJ, Morales-Macías MG, Escamilla-Reyna JA, Arredondo-Ruiz JH. Several aspects around the Riemann-Lebesgue Lemma. J. Adv. Res. Pure Math. 2012 Nov; 5(3), 33-46.
- [4] Mendoza-Torres FJ, On pointwise inversion of the Fourier transform of  $BV_0$  functions, Ann. Funct. Anal. 2010 Dic; 1 2010(2); 112-120. Available from: http://tinyurl.com/kgtq3vd
- [5] Talvila E. Henstock-Kurzweil Fourier transforms. Illinois J. Math. 2002; 46: 1207-1226. Available from: http://tinyurl.com/kbf2llg
- [6] Mendoza-Torres FJ, Escamilla Reyna JA, Sánchez-Perales S. Some results about the Henstock-Kurzweil Fourier transform. Math. Bohem. 2009; 134(4): 379–386. Available from: http://tinyurl.com/pwtsekm
- [7] Zygmund A. Trigonometric Series: Vols. 1 and 2. London-New York: Cambridge University Press; 1968.
- [8] Mohanty P, Talvila E. A product convergence theorem for Henstock-Kurzweil integral. Real Anal. Exch. 2003-2004;29(1): 199-204. Available from: http://tinyurl.com/nb5c7a6
- [9] E.C. Titchmarsh. The order of magnitude of the coefficients in a generalized Fourier series. Proc. Lond. Math. Soc. (2) 1923-1924; 22: xxv-xxvi, doi:10.1112/plms/s2-22.1.1-s
- [10] Sánchéz-Perales S. et al. Henstock-Kurzweil integral transforms. Int. J. Math. Math. Sci. 2012(2012), Article ID 209462, 11 pages. Available from: http://www.hindawi.com/journals/ijmms/2012/209462/ref/
- [11] Bartle R. A Modern Theory of Integration. Graduate Studies in Mathematics, Vol. 32. Providence: American Mathematical Society; 2001.
- [12] Bongiorno B., Panchapagesan TV. On the Alexiewicz topology of the Denjoy space. Real Anal. Exch. 1995-1996;21(2): 604–614. Avialable from: http://tinyurl.com/m2rbdr4
- [13] Talvila E. The Distributional Denjoy integral. Real Anal. Exch. 2007;33(1): 51-84. Available from: http://tinyurl.com/m4zjn9b
- [14] Kadelburg Z, Marjanović M. Interchanging two limits. Enseign. Math. 2005(8); 15-29. Availabre from: http://tinyurl.com/kyjy6p2
- [15] Rudin W. Principles of Mathematical Analysis. United States of America: McGraw Hill; 1964

- [16] Heuser H. Functional Analysis. New York: John Wiley and Sons; 1982.
- [17] Riesz M, Livingston AE. A Short Proof of a Classical Theorem in the Theory of Fourier Integrals. Amer. Math. Monthly 62(6) Jun. - Jul. 1955, 434-437. Available from: http://www.jstor.org/stable/2307003?seq=1
- [18] Talvila E. Necessary and sufficient conditions for differentiating under the integral sign. Amer. Math. Monthly 2001(108): 544-548. Available from: http://arxiv.org/pdf/math/0101012.pdf
- [19] Peng-Yee L. Lanzhou Lectures on Henstock Integration. Series in Real Analysis Vol.2. Singapore: World Scientific; 1989.
- [20] Swartz Ch. Introduction to Gauge Integrals. Singapore: World Scientific; 2001.
- [21] Talvila E. Limits and Henstock integrals of products. Real Anal. Exch. 1999/00;25(2): 907-918. Available from: http://tinyurl.com/ke4gfkh
- [22] Apostol T. Mathematical Analysis. Massachusetts: Addison-Wesley Publishing Company Reading; 1974.

# **Double Infinitesimal Fourier Transform**

# Takashi Gyoshin Nitta

Additional information is available at the end of the chapter

http://dx.doi.org/10.5772/59963

# 1. Introduction

For Fourier transform theory, one of the most important and difficult things is how to treat the Dirac delta function and how to define it. In 1930, the Dirac delta function was defined originally by Paul A.M. Dirac([1]) in order to create the quantum mechanical theory in Physics. In classical mechanics, there is the beautiful Newton's law. Under it, it is assumed that a particle is a point with a mass. For the investigation of a small world for example, elementary particles, it should be changed to the quantum mechanical theory where particles are not already only points as in Mathematics but also some area with infinitesimal length for us. They have some properties like waves. The Dirac delta function is defined to be realized the image of the particle in the small world. The particle changed to be the moving wave, and it becomes a set of such waves. It is called field in Physics and we need the second quantization . The quantum mechanics is developed to the quantum field theory where the delta function is much complicated to treat in the standard mathematical theory.

The delta function is usually defined as the delta measure in the functional analysis. Under the basic definition, the functional analysis is developed in the functional space for example Banach space, Hilbert space. These theory is applied to the existence problem of solutions for the ordinary and partial differential equations. On the other hand, the delta function is also defined just as a function in the extension of the real number field ([3],[4],[5],[18]) in 1962. The idea is that firstly the real and complex number fields are extended to the nonstandard universe, secondly the delta function is defined as a function in the extended universe (cf. [3]).

In this chapter the real number field and complex number field are extended twice and a higher degree of delta function is defined as a function on the space of functions. By using the secondly extended delta function, the Fourier transform theory is considered, that is called " double infinitesimal Fourier transform ". In the theory, the Poisson summation formula is also satisfied, and some important examples are calculated. The Fourier transforms of  $\delta$ ,  $\delta^2$ , ..., and  $\sqrt{\delta}$ , ..., can be calculated, which are constant functions as 1, infinite, ..., and infinitesimal, ...,



© 2015 The Author(s). Licensee InTech. This chapter is distributed under the terms of the Creative Commons Attribution License (http://creativecommons.org/licenses/by/3.0), which permits unrestricted use, distribution, and eproduction in any medium, provided the original work is properly cited. Then the Fourier transform of the gaussian functional is also calculated. The gaussian functional means that the standard part of the image for  $\alpha \in L^2$  is  $\exp\left(-\pi\xi \int_{-\infty}^{\infty} \alpha^2(t)dt\right)$ , for  $\xi \in \mathbf{C}$  with  $\operatorname{Re}(\xi) > 0$ . The double infinitesimal Fourier transform is calculated as  $C_{\xi} \exp\left(-\pi\xi^{-1} \int_{-\infty}^{\infty} \alpha^2(t)dt\right)$  for  $\alpha \in L^2(\mathbf{R})$ , in which  $C_{\xi}$  is a constant independent of  $\alpha$ .

Finally a sort of functional is constructed in the theory that associates to Riemann's zeta function. The path integral is defined for the application in the theory, and it is shown that the path integral of the functional  $Z_s$  corresponds to Riemann's zeta function in the case that Re(s) > 1. By using the Poisson summation formula for the functional, a relationship appears between the functional and Riemann's zeta function.

#### 2. Infinitesimal Fourier transform

The usual universe is extended, in order to treat many stages of delta functions and functions on the space of functions. For the extension, there exists two methods, one is the second extension of the universe in the nonstandard analysis ([8],[9]) and the other is the Relative set theory in the axiomatic set theory ([13]). The first one ([8],[9]) is explained here, by using an ultrafilter .

#### 2.1. First extension of the universe

Let  $\Lambda$  be an infinite set. Let F be a nonprincipal ultrafilter on  $\Lambda$ . For each  $\lambda \in \Lambda$ , let  $S_{\lambda}$  be a set. An equivalence relation  $\sim$  is induced from F on  $\prod_{\lambda \in \Lambda} S_{\lambda}$ . For  $\alpha = (\alpha_{\lambda}), \beta = (\beta_{\lambda}) \ (\lambda \in \Lambda)$ ,

$$\alpha \sim \beta \Longleftrightarrow \{\lambda \in \Lambda \,|\, \alpha_{\lambda} = \beta_{\lambda}\} \in F.$$
<sup>(1)</sup>

The set of equivalence classes is called *ultraproduct* of  $S_{\lambda}$  for *F* with respect to  $\sim$ . If  $S_{\lambda} = S$  for  $\lambda \in \Lambda$ , then it is called *ultraproduct* of *S* for *F* and it is written as \**S*. The set *S* is naturally embedded in \**S* by the following mapping :

$$s \ (\in S) \mapsto [(s_{\lambda} = s), \lambda \in \Lambda] \ (\in {}^*S)$$
 (2)

where [ ] denotes the equivalence class with respect to the ultrafilter *F*. The mapping is written as \*, and call it naturally elementary embedding. From now on, we identify the image \*(S) as *S*.

#### Definition 2.1.1.

Let  $H \ (\in \ ^*\mathbf{Z})$  be an infinite even number. The infinite number H is even, when for  $H = [(H_{\lambda}), \lambda \in \Lambda], \ \{\lambda \in \Lambda \mid H_{\lambda} \text{ is even}\} \in F$ . The number  $\frac{1}{H}$  is written as  $\varepsilon$ . We define an infinitesimal lattice space  $\mathbf{L}$ , an infinitesimal lattice subspace L and a space of functions R(L) on L as follows :

$$\mathbf{L} := \varepsilon^* \mathbf{Z} = \{ \varepsilon z \mid z \in {}^* \mathbf{Z} \},\$$
$$L := \left\{ \varepsilon z \mid z \in {}^* \mathbf{Z}, -\frac{H}{2} \le \varepsilon z < \frac{H}{2} \right\} (\subset \mathbf{L}),\$$

 $R(L) := \{ \varphi \mid \varphi \text{ is an internal function from } L \text{ to }^*\mathbf{C} \}.$ 

The space R(L) is extended to the space of periodic functions on **L** with period *H*. We write the same notation R(L) for the space of periodic functions.

Gaishi Takeuchi([18]) introduced an infinitesimal  $\delta$  function. Furthermore Moto-o Kinoshita ([4],[5]) constructed an infinitesimal Fourier transformation theory on R(L). It is explained briefly.

#### Definition 2.1.2.

For  $\varphi$ ,  $\psi \in R(L)$ , the infinitesimal  $\delta$  function, the infinitesimal Fourier transformation  $F\varphi$  ( $\in R(L)$ ), the inverse infinitesimal Fourier transformation  $\overline{F}\varphi$  ( $\in R(L)$ ) and the convolution  $\varphi * \psi (\in R(L))$  are defined as follows :

$$\delta \in R(L), \ \delta(x) := \begin{cases} H & (x=0) \\ 0 & (x \neq 0) \end{cases}$$
(3)

$$(F\varphi)(p) := \sum_{x \in L} \varepsilon \exp\left(-2\pi i p x\right) \varphi(x) \tag{4}$$

$$(\overline{F}\varphi)(p) := \sum_{x \in L} \varepsilon \exp(2\pi i p x) \varphi(x)$$
(5)

$$(\varphi * \psi)(x) := \sum_{y \in L} \varepsilon \varphi(x - y) \psi(y).$$
(6)

The definition implies the following theorem as same as the Fourier transform for the finite discrete abelian group.

#### Theorem 2.1.3.

- (1)  $\delta = F1 = \overline{F}1$ , (2) *F* is unitary,  $F^4 = 1, \overline{F}F = F\overline{F} = 1$ ,
- (3)  $f * \delta = \delta * f = f$ , (4) f \* g = g \* f,
- (5) F(f \* g) = (Ff)(Fg), (6)  $\overline{F}(f * g) = (\overline{F}f)(\overline{F}g)$ ,
- (7) F(fg) = (Ff) \* (Fg), (8)  $\overline{F}(fg) = (\overline{F}f) * (\overline{F}g)$ .

The definition implies the following proposition by the simple calculation:

#### Proposition 2.1.4.

If  $l \in \mathbf{R}$ , then

$$F\delta^l = (H)^{(l-1)}.\tag{7}$$

Examples of the infinitesimal Fourier transform for functions

The infinitesimal Fourier transforms of the gaussian function  $\varphi_{\xi}$ ,  $\varphi_{im} \in R(L)$  are calculated as follows:  $\varphi_{\xi}(x) = \exp(-\xi \pi x^2)$ , where  $\xi \in \mathbf{C}$ ,  $\operatorname{Re}(\xi) > 0$ ,

$$\varphi_{im}(x) = \exp(-im\pi x^2)$$
, where  $m \in \mathbb{Z}$ .

For  $\varphi_{\xi}$ , we obtain :

#### Proposition 2.1.5.

 $(F\varphi_{\xi})(p) = c_{\xi}(p)\varphi_{\xi}(\frac{p}{\xi})$ , where  $c_{\xi}(p) = \sum_{x \in L} \varepsilon \exp(-\xi \pi (x + \frac{i}{\xi}p)^2)$  and p is an element of the lattice L.

If *p* is finite, then  $st(c_{\xi}(p)) = \frac{1}{\sqrt{\xi}}$ .

**Proof.** The infinitesimal Fourier transforms of  $\varphi_{\xi}$  is :

$$(F\varphi_{\xi})(p) = \sum_{x \in L} \varepsilon \exp(-2\pi i p x) \exp(-\xi \pi x^{2})$$
$$= \left(\sum_{x \in L} \varepsilon \exp(-\xi \pi (x + \frac{i}{\xi}p)^{2})\right) \exp(-\pi \frac{1}{\xi}p^{2}) = c_{\xi}(p)\varphi_{\xi}(\frac{p}{\xi})$$
(8)

where  $c_{\xi}(p) = \sum_{x \in L} \varepsilon \exp(-\xi \pi (x + \frac{i}{\xi}p)^2)$ . If p is finite, then  $\operatorname{st}(c_{\xi}(p)) = \int_{-\infty}^{\infty} \exp\left(-\xi \pi \left(t + \frac{i}{\xi}\operatorname{st}(p)\right)^2\right) dt = \frac{1}{\sqrt{\xi}}$ .

Theorem 2.1.3 (8) implies the following for  $c_{\xi}$ :

Proposition 2.1.6.

$$\varphi_{\xi}(x') = \left(\overline{F}c_{\xi}(p) * \left(c_{\frac{1}{\xi}}(-x)\varphi_{\xi}(x)\right)\right)(x').$$
(9)

**Proof.** It is obtained :  $(F\varphi_{\xi})(p) = c_{\xi}(p)\varphi_{\xi}(\frac{p}{\xi})$ , and put  $\overline{F}$  to the above :  $(\overline{F}(F\varphi_{\xi}))(x) = (\overline{F}(c_{\xi}(p)\varphi_{\xi}(\frac{p}{\xi})))(x)$   $= (\overline{F}c_{\xi}(p) * \overline{F}\varphi_{\xi}(\frac{p}{\xi}))(x)$ , that is,  $\varphi_{\xi}(x) = (\overline{F}c_{\xi}(p) * \overline{F}\varphi_{\xi}(\frac{p}{\xi}))(x)$ . Now  $(\overline{F}\varphi_{\xi}(\frac{p}{\xi}))(x) = \sum_{p \in L} \varepsilon \exp(-2\pi i p x) \exp(-\xi(\frac{p}{\xi})^2 \pi)$   $= \sum_{p \in L} \varepsilon \exp(-\pi \frac{1}{\xi}(p^2 - 2\pi i \xi p x)) = \left(\sum_{p \in L} \varepsilon \exp(-\frac{\pi}{\xi}(p - i \xi x)^2)\right) \varphi_{\xi}(x)$ . By the definition :  $c_{\xi}(p) = \sum_{x \in L} \varepsilon \exp(-\pi \xi(x + i \frac{1}{\xi}p)^2)$ , the sum  $\sum_{p \in L} \varepsilon \exp(-\frac{\pi}{\xi}(p - i \xi x)^2)$  is  $c_{\frac{1}{\xi}}(-x)$ . Hence

$$\varphi_{\xi}(x') = \left(\overline{F}c_{\xi}(p) * \left(c_{\frac{1}{\xi}}(-x)\varphi_{\xi}(x)\right)\right)(x').$$
(10)

For the following proposition 2.1.7, the Gauss sum is recalled (cf.[15]) : For  $z \in \mathbf{N}$ , the Gauss sum  $\sum_{l=0}^{z-1} \exp(-i\frac{2\pi}{z}l^2)$  is equal to  $\sqrt{z}\frac{1+(-i)^z}{1-i}$ .

**Proposition 2.1.7.** If  $m|2H^2$  and  $m|\frac{p}{\epsilon}$ , then

$$(F\varphi_{im})(p) = c_{im}(p)\exp(i\pi\frac{1}{m}p^2)$$
(11)

where  $c_{im}(p) = \sqrt{\frac{m}{2}} \frac{1+i\frac{2H^2}{m}}{1+i}$  for positive *m* and  $c_{im}(p) = \sqrt{\frac{-m}{2}} \frac{1+(-i)\frac{2H^2}{-m}}{1-i}$  for negative *m*. **Proof.**  $(F\varphi_{im})(p) = \sum_{x \in L} \varepsilon \exp(-im\pi x^2) \exp(-2\pi i x p)$  $= c_{im}(p) \exp(i\pi \frac{1}{m}p^2)$ , where  $c_{im}(p) = \sum_{x \in L} \varepsilon \exp(-im\pi (x + \frac{p}{m})^2)$ .

Since  $m|\frac{p}{\varepsilon}$ , the element  $\frac{p}{m}$  is in *L*. It is remarked that  $\exp(-i\pi mx^2) = \exp(-i\pi m(x+H)^2)$ . For positive *m*,

$$c_{im}(p) = \sum_{x \in L} \varepsilon \exp(-im\pi x^2) = \frac{m}{2} \overline{\left(\varepsilon \sqrt{\frac{2H^2}{m}} \frac{1 + (-i)^{\frac{2H^2}{m}}}{1 - i}\right)}$$
(12)

by the above Gauss sum. Hence  $c_{im}(p) = \sqrt{\frac{m}{2} \frac{1+i^{\frac{2H^2}{m}}}{1+i}}$ . For negative *m*, the proof is as same as the above.

#### 2.2. Second extension of the universe

To treat a \*-unbounded functional f in the nonstandard analysis, we need a second nonstandardization. Let  $F_2 := F$  be a nonprincipal ultrafilter on an infinite set  $\Lambda_2 := \Lambda$  as above. Denote the ultraproduct of a set S with respect to  $F_2$  by \*S as above. Let  $F_1$  be another nonprincipal ultrafilter on an infinite set  $\Lambda_1$ . Take the \*-ultrafilter \* $F_1$  on \* $\Lambda_1$ . For an internal set S in the sense of \*-nonstandardization, let \*S be the \*-ultraproduct of S with respect to \* $F_1$ . Thus, a double ultraproduct \*(\* $\mathbf{R}$ ), \*(\* $\mathbf{Z}$ ), etc are defined for the set  $\mathbf{R}$ ,  $\mathbf{Z}$ , etc. It is shown easily that

$$^{\star}(^{*}\mathbf{S}) = S^{\Lambda_{1} \times \Lambda_{2}} / F_{1}^{F_{2}}, \tag{13}$$

where  $F_1^{F_2}$  denotes the ultrafilter on  $\Lambda_1 \times \Lambda_2$  such that for any  $A \subset \Lambda_1 \times \Lambda_2$ ,  $A \in F_1^{F_2}$  if and only if

$$\{\lambda \in \Lambda_1 \mid \{\mu \in \Lambda_2 \mid (\lambda, \mu) \in A\} \in F_2\} \in F_1.$$
(14)

The work is done with this double nonstandardization. The natural imbedding \*S of an internal element *S* which is not considered as a set in \*-nonstandardization is often denoted simply by *S*.

An infinite number in  $*(*\mathbf{R})$  is defined to be greater than any element in  $*\mathbf{R}$ . We remark that an infinite number in  $*\mathbf{R}$  is not infinite in  $*(*\mathbf{R})$ , that is, the word "an infinite number in  $*(*\mathbf{R})$ " has a double meaning. An infinitesimal number in  $*(*\mathbf{R})$  is also defined to be nonzero and whose absolute value is less than each positive number in  $*\mathbf{R}$ .

#### Definition 2.2.1.

Let  $H(\in {}^{*}\mathbf{Z})$ ,  $H'(\in {}^{*}({}^{*}\mathbf{Z}))$  be even positive numbers such that H' is larger than any element in  ${}^{*}\mathbf{Z}$ , and let  $\varepsilon(\in {}^{*}\mathbf{R})$ ,  $\varepsilon'(\in {}^{*}({}^{*}\mathbf{R}))$  be infinitesimals satisfying  $\varepsilon H = 1$ ,  $\varepsilon' H' = 1$ . We define as follows :

$$\begin{split} \mathbf{L} &:= \varepsilon^* \mathbf{Z} = \{ \varepsilon z \, | \, z \in \, ^* \mathbf{Z} \}, \ \mathbf{L}' := \varepsilon'^* (\, ^* \mathbf{Z}) = \{ \varepsilon' z' \, | \, z' \in \, ^* (\, ^* \mathbf{Z}) \}, \\ L &:= \left\{ \varepsilon z \, \left| \, z \in \, ^* \mathbf{Z}, \, -\frac{H}{2} \le \varepsilon z < \frac{H}{2} \right\} \, (\subset \mathbf{L}), \\ L' &:= \left\{ \varepsilon' z' \, \left| \, z' \in \, ^* (\, ^* \mathbf{Z}), \, -\frac{H'}{2} \le \varepsilon' z' < \frac{H'}{2} \right\} \, (\subset \mathbf{L}'). \end{split} \end{split}$$

Here *L* is an ultraproduct of lattices

$$L_{\mu} := \left\{ \varepsilon_{\mu} z_{\mu} \mid z_{\mu} \in \mathbf{Z}, \ -\frac{H_{\mu}}{2} \le \varepsilon_{\mu} z_{\mu} < \frac{H_{\mu}}{2} \right\} \ (\mu \in \Lambda_{2})$$

in **R**, and L' is also an ultraproduct of lattices

$$L'_{\lambda} := \left\{ \varepsilon'_{\lambda} z'_{\lambda} \mid z'_{\lambda} \in {}^{*}\mathbf{Z}, -\frac{H'_{\lambda}}{2} \le \varepsilon'_{\lambda} z'_{\lambda} < \frac{H'_{\lambda}}{2} \right\} \ (\lambda \in \Lambda_{1})$$

in \***R** that is an ultraproduct of

$$L'_{\lambda\mu} := \left\{ \varepsilon'_{\lambda\mu} z'_{\lambda\mu} \ \left| \ z'_{\lambda\mu} \in \mathbf{Z}, \ -\frac{H'_{\lambda\mu}}{2} \le \varepsilon'_{\lambda\mu} z'_{\lambda\mu} < \frac{H'_{\lambda\mu}}{2} \right\} \ (\mu \in \Lambda_2). \right.$$

A latticed space of functions X is defined as follows,

$$X := \{a \mid a \text{ is an internal function with double meanings, from }^{\star}L \text{ to } L'\}$$
$$= \{[(a_{\lambda}), \lambda \in \Lambda_1] \mid a_{\lambda} \text{ is an internal function from } L \text{ to } L'_{\lambda}\}$$
(15)

where  $a_{\lambda}: L \to L'_{\lambda}$  is  $a_{\lambda} = [(a_{\lambda\mu}), \mu \in \Lambda_2], a_{\lambda\mu}: L_{\mu} \to L'_{\lambda\mu}$ .

Three equivalence relations  $\sim_{H}$ ,  $\sim_{\star(H)}$  and  $\sim_{H'}$  are defined on L,  $\star(L)$  and L':

$$\begin{aligned} x \sim_H y &\iff x - y \in H^* \mathbf{Z}, \ x \sim_{\star(H)} y &\iff x - y \in \star(H)^* (* \mathbf{Z}), \\ x \sim_{H'} y &\iff x - y \in H'^* (* \mathbf{Z}). \end{aligned}$$

Then  $\mathbf{L}/\sim_{H}$ ,  $*(\mathbf{L})/\sim_{*(H)}$  and  $\mathbf{L}'/\sim_{H'}$  are identified as L, \*(L) and L'. Since \*(L) is identified with L, the set  $*(\mathbf{L})/\sim_{*(H)}$  is identified with  $\mathbf{L}/\sim_{H}$ . Furthermore X is represented as the following internal set :

$$\{a \mid a \text{ is an internal function from }^{\star}(\mathbf{L}) / \sim_{\star(H)} \text{ to } \mathbf{L}' / \sim_{H'} \}.$$
 (16)

The same notation is used as a function from \*(L) to L' to represent a function in the above internal set. The space *A* of functionals is defined as follows:

 $A := \{f \mid f \text{ is an internal function with a double meaning from X to }^{\star}(^{*}\mathbf{C})\}.$ (17)

An infinitesimal delta function  $\delta(a) (\in A)$ , an infinitesimal Fourier transform of  $f (\in A)$ , an inverse infinitesimal Fourier transform of f and a convolution of f,  $g (\in A)$ , are defined by the following :

Definition 2.2.2. The delta function

$$\delta(a) := \begin{cases} (H')^{(*H)^2} & (a=0)\\ 0 & (a\neq 0) \end{cases}$$
(18)

and, with  $\varepsilon_0 := (H')^{-(*H)^2} \in *(*\mathbf{R})$ ,

$$(Ff)(b) := \sum_{a \in X} \varepsilon_0 \exp\left(-2\pi i \sum_{k \in L} a(k)b(k)\right) f(a)$$
(19)

$$(\overline{F}f)(b) := \sum_{a \in X} \varepsilon_0 \exp\left(2\pi i \sum_{k \in L} a(k)b(k)\right) f(a)$$
(20)

$$(f * g)(a) := \sum_{a' \in X} \varepsilon_0 f(a - a') g(a').$$
(21)

The inner product on *A* is defined as:

$$(f,g) := \sum_{b \in X} \varepsilon_0 \overline{f(b)} g(b),$$
(22)

where  $\overline{f(b)}$  is the complex conjugate of f(b). In the section 3, Riemann's zeta function is written down as a nonstandard functional in Definition 2.2.2. In general,  $\sum_{k \in L} a^2(k)$  is infinite, and it is difficult to consider the meaining of F,  $\overline{F}$  in Definition 2.2.2 as standard objects. They are defined only algebraically. In order to understand Definition 2.2.2 analytically for a standard one, we change the definition briefly, to Definition 2.2.3. By replacing the definitions of L',  $\delta$ ,  $\varepsilon_0$ , F,  $\overline{F}$  in Definition 2.2.2 as the following, another type of infinitesimal Fourier transformation is defined later. The different point is only the definition of an inner product of the space of functions X. In Definition 2.2.2, the inner product of  $a, b(\in X)$  is  $\sum_{k \in L} a(k)b(k)$ , and in the following definition, it is  $*\varepsilon \sum_{k \in L} a(k)b(k)$ . **Definition 2.2.3.**  $L' := \left\{ \varepsilon' z' \mid z' \in *(*\mathbf{Z}), -*H\frac{H'}{2} \leq \varepsilon' z' < *H\frac{H'}{2} \right\}$ ,

$$\delta(a) := \begin{cases} (*H)^{\frac{(*H)^2}{2}} H'^{(*H)^2} & (a=0), \\ 0 & (a\neq 0) \end{cases}$$
(23)

and, with  $\varepsilon_0 := ({}^{\star}H)^{-\frac{({}^{\star}H)^2}{2}}H'^{-({}^{\star}H)^2}$ 

$$(Ff)(b) := \sum_{a \in X} \varepsilon_0 \exp\left(-2\pi i^* \varepsilon \sum_{k \in L} a(k)b(k)\right) f(a)$$
(24)

$$(\overline{F}f)(b) := \sum_{a \in X} \varepsilon_0 \exp\left(2\pi i^* \varepsilon \sum_{k \in L} a(k)b(k)\right) f(a).$$
(25)

Then the lattice  $L'_{\lambda\mu}$  is an abelian group for each  $\lambda\mu$ . The following theorem is obtained as same as the case of the discrete abelian group :

#### Theorem 2.2.4.

(1)  $\delta = F1 = \overline{F}1$ , (2) *F* is unitary,  $F^4 = 1, \overline{F}F = F\overline{F} = 1$ ,

(3) 
$$f * \delta = \delta * f = f$$
, (4)  $f * g = g * f$ ,

- (5) F(f \* g) = (Ff)(Fg), (6)  $\overline{F}(f * g) = (\overline{F}f)(\overline{F}g)$ ,
- (7) F(fg) = (Ff) \* (Fg), (8)  $\overline{F}(fg) = (\overline{F}f) * (\overline{F}g)$ .

The definition directly implies the following proposition :

**Proposition 2.2.5.** If  $l \in \mathbf{R}^+$ , then

$$F\delta^{l} = (H')^{(l-1)(*H)^{2}}.$$
(26)

If there exists  $\alpha$ ,  $\beta \in L^2(\mathbf{R})$  so that  $a = {}^*\alpha|_L$ ,  $b = {}^*\beta|_L$ , that is,  $a(k) = \star ({}^*\alpha(k))$ ,  $b(k) = \star ({}^*\beta(k))$ , then  $\operatorname{st}(\operatorname{st}({}^*\varepsilon\sum_{k\in L}a(k)b(k))) = \int_{-\infty}^{\infty}\alpha(x)b(x)dx$ . Definition 2.2.3 is easier understanding than Definition 2.2.2 for a standard meaning in analysis. For the reason, we consider mainly Definition 2.2.3 about several examples. However Definition 2.2.2 is also treated algebraically, as algebraically defined functions are not always  $L^2$ -functions on **R**. The two types of Fourier transforms are different in a standard meaning.

#### Examples of the double infinitesimal Fourier transform

It is defined: an equivalence relation  $\sim_{*HH'}$  in **L**' by  $x \sim_{*HH'} y \Leftrightarrow x - y \in {*HH' * (*\mathbf{Z})}$ . The quotient space  $\mathbf{L}' / \sim_{*HH'}$  is defined with L'. Let

 $X_{H,*HH'} := \{a' | a' \text{ is an internal function with a double meaning, from *L/ <math>\sim_{\star(H)}$  to  $\mathbf{L}' / \sim_{\star(H)} \{a' | a' \in \mathbb{R}\}$ 

and let **e** be a mapping from X to  $X_{H,*HH'}$ , defined by  $(\mathbf{e}(a))([k]) = [a(\hat{k})]$ , where [ ] on the left-hand side represents the equivalence class for the equivalence relation  $\sim_{\star(H)}$  in \***L**,  $\hat{k}$  is a representative in \*(*L*) satisfying  $k \sim_{\star(H)} \hat{k}$ , and [ ] on the right-hand side represents the equivalence class for the equivalence relation  $\sim_{\star HH'} \hat{k}$  in **L**'. Furthermore f(a') is identified to be  $f(\mathbf{e}^{-1}(a'))$ .

### The double infinitesimal Fourier transform of $\exp\left(-\pi \star \varepsilon \xi \sum_{k \in L} a^2(k)\right)$

The double infinitesimal Fourier transform of

$$g_{\xi}(a) = \exp\left(-\pi^{\star} \varepsilon \xi \sum_{k \in L} a^2(k)\right), \qquad (27)$$

where  $\xi \in \mathbf{C}$ ,  $\operatorname{Re}(\xi) > 0$ ,

is calculated in the space *A* of functionals, for Definition 2.2.3. It is identified  $*(*\xi) \in \mathbf{C}$  with  $\xi \in \mathbf{C}$ .

**Theorem 2.2.6.**  $F(g_{\xi})(b) = C_{\xi}(b)g_{\xi}(\frac{b}{\xi})$ , where  $b \in X$  and

$$C_{\xi}(b) = \sum_{a \in X} \varepsilon_0 \exp\left(-\pi^* \varepsilon \xi \sum_{k \in L} (a(k) + i\frac{1}{\xi}b(k))^2\right).$$
(28)

**Proof.** The infinitesimal Fourier transform of  $g_{\xi}(a)$  is done.

$$\begin{aligned} F(g_{\xi})(b) &= F\left(\exp\left(-\pi \star \varepsilon \xi \sum_{k \in L} a^2(k)\right)\right)(b) \\ &= \sum_{a \in X} \varepsilon_0 \exp\left(-2i\pi \star \varepsilon \sum_{k \in L} a(k)b(k)\right) \exp\left(-\pi \star \varepsilon \xi \sum_{k \in L} a^2(k)\right) \\ &= C_{\xi}(b)g_{\xi}(\frac{b}{\xi}). \end{aligned}$$

Let  $\star \circ * : \mathbf{R} \to \star(*\mathbf{R})$  be the natural elementary embedding and let  $\mathbf{st}(c)$  for  $c \in \star(*\mathbf{R})$  be the standard part of *c* with respect to the natural elementary embedding  $\star \circ *$ . Let  $\mathbf{st}(c)$  be the standard part of *c* with respect to the natural elementary embedding  $\star$  and \*. Then  $\mathbf{st} = st \circ st$ .

**Theorem 2.2.7.** If the image of  $b \in (X)$  is bounded by a finite value of  $*\mathbf{R}$ , that is, there exists  $b_0 \in *\mathbf{R}$  such that  $k \in L \Rightarrow |b(k)| \leq \star(b_0)$ , then

$$\operatorname{st}(C_{\xi}(b)) = \left(\ast \left(\frac{1}{\sqrt{\xi}}\right)\right)^{H^2} \ (\in \ {}^{\ast}\mathbf{R}), \ \operatorname{st}\left(\frac{C_{\xi}(b)}{\star \left(\left(\ast \left(\frac{1}{\sqrt{\xi}}\right)\right)^{H^2}\right)}\right) = 1.$$
(29)

**Proof.**  $\operatorname{st}(C_{\xi}(b)) = \operatorname{st}(\sum_{a \in X} \prod_{k \in L} \sqrt{\varepsilon} \varepsilon' \exp\left(-\pi \xi \{\sqrt{\varepsilon}(a(k)) + i\sqrt{\varepsilon} \frac{1}{\xi}(b(k))\}^2\right))$  $= \prod_{k \in L} \int_{-\infty}^{+\infty} \exp\left(-\pi \xi \{x + i\sqrt{\varepsilon} \frac{1}{\xi} \operatorname{st}_2(b(k))\}^2\right) dx$   $= \prod_{k \in L} \int_{-\infty}^{+\infty} \exp\left(-\pi \xi x^2\right) dx.$ 

The argument is same about the infinitesimal Fourier transform of  $g'_{\xi}(a) = \exp(-\pi\xi \sum_{k\in L} a^2(k))$ , for Definition 2.2.2, as the above.

Theorem 2.2.8.

$$F(g'_{\xi})(b) = B_{\xi}(b)g'_{\xi}(\frac{b}{\xi}),$$
(30)

where  $b \in X$  and

 $B_{\xi}(b) = \sum_{a \in X} \varepsilon_0 \exp\left(-\pi \xi \sum_{k \in L} (a(k) + i\frac{1}{\xi}b(k))^2\right)$ . Furthermore, if the image of  $b \ (\in X)$  is bounded by a finite value of  $*\mathbf{R}$ , that is,  $\exists b_0 \in *\mathbf{R}$  s.t.  $k \in L \Rightarrow |b(k)| \le \star(b_0)$  then

$$\operatorname{st}(B_{\xi}(b)) = \left(\ast \left(\frac{1}{\sqrt{\xi}}\right)\right)^{H^2} \ (\in \ ^*\mathbf{R}), \ \operatorname{st}\left(\frac{B_{\xi}(b)}{\star \left(\left(\ast \left(\frac{1}{\sqrt{\xi}}\right)\right)^{H^2}\right)}\right) = 1.$$
(31)

The double infinitesimal Fourier transform of  $\exp(-i\pi m^{\star} \varepsilon \sum_{k \in L} a^2(k))$ 

The double infinitesimal Fourier transform of  $g_{im}(a) = \exp(-i\pi m \star \varepsilon \sum_{k \in L} a^2(k))$ , where  $m \in \mathbb{Z}$ , is calculated for Definition 2.2.3.

**Proposition 2.2.9.**  $F(g_{im})(b)$  is written as  $C_{im}(b)g_{\frac{1}{im}}(b)$ .

If  $m|2^*HH'^2$  and  $m|\frac{b(k)}{\varepsilon'}$  for an arbitrary k in L, then  $F(g_{im})(b) = C_{im}(b)g_{\frac{1}{im}}(b)$ , where  $C_{im}(b) = \left(\sqrt{\frac{m}{2}}\frac{1+i\frac{2^*HH'^2}{1+i}}{1+i}\right)^{(^*H)^2}$  for a positive m and  $C_{im}(b) = \left(\sqrt{\frac{-m}{2}}\frac{1+(-i)\frac{2^*HH'^2}{-m}}{1-i}}\right)^{(^*H)^2}$  for a negative m.

Proof.

$$F(g_{im})(b) = C_{im}(b)g_{\frac{1}{im}}(b), \text{ where } C_{im}(b) = \sum_{a \in X} \varepsilon_0 \exp(-i\pi m \star \varepsilon \sum_{k \in L} (a(k) + \frac{1}{m}b(k))^2).$$
  
When  $a(k)$ ,  $b(k)$  are denoted as  $\varepsilon' n'$ ,  $\varepsilon' l'$ ,  
$$\sum_{-\star H \frac{H'^2}{2} \le a(k) < \star H \frac{H'^2}{2}} \exp(-i\pi m \star \varepsilon \sum_{k \in L} (a(k) + \frac{1}{m}b(k))^2)$$

$$= \sum_{-*H\frac{H'^2}{2} \le \varepsilon' n' < *H\frac{H'^2}{2}} \exp(-i\pi m^* \varepsilon \sum_{k \in L} (\varepsilon' n' + \varepsilon' \frac{n'}{m})^2).$$
(32)

Since  $m | \frac{b(k)}{\epsilon'}$ , for a positive *m*, it is equal to

$$\sum_{-*H\frac{H'^2}{2} \le \epsilon' n' < *H\frac{H'^2}{2}} \exp(-i\pi m^* \epsilon \epsilon'^2 n'^2) = \frac{m}{2} \sqrt{\frac{2^* H H'^2}{m}} \frac{1 + i^{\frac{2^* H H'^2}{m}}}{1 + i}$$
(33)

by Proposition 2.1.5. Hence  $C_{im} = \left(\sqrt{\frac{m}{2}} \frac{1+i^{\frac{2^*HH'^2}{m}}}{1+i}\right)^{(*H)^2}$  for a positive *m*. For a negative *m*, the proof is as same as the above.

The argument for the infinitesimal Fourier transform of  $g'_{im}(a) = \exp(-i\pi m \sum_{k \in L} a^2(k))$ , for Definition 2.2.2, is as same as the above one of  $g_{im}$  for Definition 2.2.3.

**Proposition 2.2.10.** If  $m|2^*HH'^2$  and  $m|\frac{b(k)}{\epsilon'}$  for an arbitrary k in L, then  $(F((g'_{im}))(b) = B_{im}(b)g'_{\frac{1}{im}}(b)$ , where  $B_{im}(b) = \left(\sqrt{\frac{m}{2}}\frac{1+i\frac{2H'^2}{m}}{1+i}\right)^{\binom{*}{2}}$  for a positive m and  $B_{im}(b) = \left(\sqrt{\frac{-m}{2}}\frac{1+(-i)\frac{2H'^2}{-m}}{1-i}\right)^{\binom{*}{2}}$  for a negative m.

#### 2.3. The meaning of the double infinitesimal Fourier transform

There exists a natural injection from a space of standard functions to X as

$$\alpha \mapsto (a: k \in L \mapsto \star(^*\alpha(k)) \in L').$$
(34)

Hence a space of standard functions is embedded in *X* through the natural injection. If there is no confusion, standard functions are identified as nonstandard functions by the natural injection.

For a standard functional f, if the domain of \*(\*f) is in X, we can define a Fourier transform F(\*(\*f)). Since st(st(F(\*(\*f))) is a standard functional as  $st(st(F(*(*f)))(\alpha) = st(st(F(*(*f))(\alpha)))$  for  $a : k \in L \to *(*\alpha(k)) \in L'$ , such standard functional has a Fourier transform st(st(F(\*(\*f)))).

Similarly to the case of functions, the following subspace  $\mathcal{L}^2(A)$  of *A* is defined:

#### Definition 2.3.1.

$$\mathcal{L}^{2}(A) := \{ f \in A | \text{ there exists } c \in {}^{*}\mathbf{R} \text{ so that } (\frac{1}{c} \sum_{a \in X} \varepsilon_{0} |f(a)|^{2}) < +\infty \}.$$
(35)

The standard part st( $\sum_{a \in X} \varepsilon_0 |f(a)|^2$ ) is a \*- norm in  $\mathcal{L}^2(A)$ . Theorem 2.1.3 (2) implies the following proposition.

**Proposition 2.3.2.** The Fourier transform *F* and the inverse  $\overline{F}$  preserve the space  $\mathcal{L}^2(A)$ .

Hence if *f* is a standard functional so that (\*f) is an element of  $\mathcal{L}^2(A)$ , the Fourier transformation F(\*(\*f)),  $\overline{F}(*(*f))$  are also in  $\mathcal{L}^2(A)$ . Now there is no theory of Fourier transform for functionals in "standard analysis", and it is well-known that there is no nontrivial translation-invariant measure on an infinite-dimensional separable Banach space. In fact, on the infinite-dimensional Banach space there is an infinite sequence of pairwise disjoint open balls of same sizes in a larger ball. The measure is translation-invariant,

the measure of the small balls are same, but the measure of the larger ball is finite, it is contradiction. By the reason we do not argue a relationship between our Fourier transform and standard Fourier transform, any more.

Here number fields are extended twice to realize the delta function for functionals. The extended real number field divided to very small infinitesimal lattices. These lattices are too small for normal real number field and the first extended real number field to observe them. Axiomatically, the double extended number field can be treat in a large universe, that is, relative set theory ([13],[14]). The concept of observable and relatively observable are formulated, and two kinds of delta functions are defined. The Fourier transform theory is developed, which is called divergence Fourier transform . It is applied to solve an elementary ordinary differential equation with a delta function(cf.[12]).

## 3. Poisson summation formula

The Poisson summation formula is a fundamental formula for each Fourier transform theory. In this section, it is explained about the Kinoshita's Fourier transform and our double infinitesimal Fourier transform. Some examples of the gaussian type functions are calculated for the applications of the Poisson summation formula.

#### 3.1. Poisson summation formula for infinitesimal Fourier transform

The Poisson summation formula of finite group is extended to Kinoshita's infinitesimal Fourier transform.

#### Formulation

**Theorem 3.1.1.** Let *S* be an internal subgroup of *L*. Then the following formula is obtained, for  $\varphi \in R(L)$ ,

$$|S^{\perp}|^{-\frac{1}{2}} \sum_{p \in S^{\perp}} (F\varphi)(p) = |S|^{-\frac{1}{2}} \sum_{x \in S} \varphi(x)$$
(36)

where  $S^{\perp} := \{ p \in L \mid \exp(2\pi i p x) = 1 \text{ for } \forall x \in S \}.$ 

Since *L* is an internal cyclic group, the group *S* is also an internal cyclic group. The generator of *L* is  $\varepsilon$ . The generator of *S* is written as  $\varepsilon s$  ( $s \in *\mathbf{Z}$ ). Since the order of *L* is  $H^2$ , so *s* is a factor of  $H^2$ .

The following lemma is prepared for the proof of Theorem 3.1.1.

Lemma 3.1.2.  $S^{\perp} = < \varepsilon \frac{H^2}{s} >.$ 

**Proof of Lemma 3.1.2.** For  $p \in S^{\perp}$ , we write  $p = \varepsilon t$ . Then the following is obtained:

$$\exp(2\pi i p \varepsilon s) = 1 \iff \exp(2\pi i \varepsilon t \varepsilon s) = 1 \iff \exp(2\pi i t \frac{s}{H^2}) = 1 \iff t \frac{s}{H^2} \in {}^*\mathbf{Z}.$$
(37)

Hence the generator of  $S^{\perp}$  is  $\varepsilon \frac{H^2}{s}$ .

**Proof of Theorem 3.1.1.** By Lemma 2.1.2,  $|S| = \frac{H^2}{s}$  and  $|S^{\perp}| = s$ . If  $x \notin S$ , then  $\varepsilon \frac{H^2}{s} xs = \varepsilon H^2 x \in {}^*\mathbf{Z}$ , and  $\left(\exp\left(2\pi i\varepsilon \frac{H^2}{s}x\right)\right)^s = 1$ . For  $x \in L$ ,

$$\sum_{p \in S^{\perp}} \exp(2\pi i p x) = \begin{cases} \frac{\exp(2\pi i (-\frac{H}{2})x)(1 - (\exp(2\pi i \varepsilon \frac{H^2}{s} x)^s))}{1 - \exp(2\pi i \varepsilon \frac{H^2}{s} x)} & (x \notin S) \\ \sum_{p \in S^{\perp}} 1 & (x \in S) \end{cases}$$
$$= \begin{cases} 0 & (x \notin S) \\ s & (x \in S) \end{cases}.$$
(38)

#### Hence

 $\sum_{p\in S^\perp}(F\varphi)(p)=\sum_{p\in S^\perp}\varepsilon(\sum_{x\in L}\varphi(x)\exp(2\pi i px))$ 

$$=\varepsilon \sum_{x\in L} \varphi(x) (\sum_{p\in S^{\perp}} \exp(2\pi i px)) = \frac{s}{H} \sum_{x\in S} \varphi(x).$$
(39)

Thus

$$\frac{1}{\sqrt{s}}\sum_{p\in S^{\perp}}(F\varphi)(p) = \sqrt{\frac{s}{H^2}}\sum_{x\in S}\varphi(x)$$
(40)

hence

$$|S^{\perp}|^{-\frac{1}{2}} \sum_{p \in S^{\perp}} (F\varphi)(p) = \frac{1}{|S|^{\frac{1}{2}}} \sum_{x \in S} \varphi(x) \cdots (\sharp_1).$$
(41)

**Proposition 3.1.3.** Especially if *s* is equal to *H*, then  $(\sharp_1)$  implies that  $\sum_{p \in S^{\perp}} (F\varphi)(p) = \sum_{x \in S} \varphi(x)$ . The standard part of it is st $(\sum_{p \in S^{\perp}} (F\varphi)(p)) = \operatorname{st}(\sum_{x \in S} \varphi(x))$ .

If there exists a standard function  $\varphi' : \mathbf{R} \to \mathbf{C}$  so that  $\varphi = {}^*\varphi'|_L$ , then the right hand side is equal to  $\sum_{-\infty < x < \infty} \varphi'(x)$ , that is,  $\sum_{-\infty < x < \infty} \operatorname{st}(\varphi)(x)$ . Furthermore if  $\varepsilon s$  is infinitesimal and  $\varphi'$  is integrable on **R**, then

$$\begin{aligned} \operatorname{st}(\varepsilon s \sum_{x \in S} \varphi(x)) &= \int_{-\infty}^{\infty} \varphi'(x) dx. \\ \text{Since } (\sharp_1) \text{ implies that} \\ \sum_{p \in S^{\perp}} (F\varphi)(p) &= \varepsilon s \sum_{x \in S} \varphi(x), \\ \text{it is obtained } \operatorname{st}(\sum_{p \in S^{\perp}} (F\varphi)(p)) &= \int_{-\infty}^{\infty} \varphi'(x) dx, \text{ that is, } \int_{-\infty}^{\infty} \operatorname{st}(\varphi)(x) dx. \end{aligned}$$

The even number *H* is decomposed to prime factors  $H = p_1^{l_1} p_2^{l_2} \cdots p_m^{l_m}$ , where  $p_1 = 2$ ,  $p_1 < p_2 < \cdots < p_m$ , each  $p_i$  is a prime number,  $0 < l_i$ . Since *S* is a subgroup of *L*, the number *s* is a factor of  $H^2$ . When we write *s* as  $p_1^{k_1} p_2^{k_2} \cdots p_m^{k_m}$ , the order of *S* is equal to  $p_1^{2l_1-k_1} p_2^{2l_2-k_2} \cdots p_m^{2l_m-k_m}$  and the order of  $S^{\perp}$  is  $p_1^{k_1} p_2^{k_2} \cdots p_m^{k_m}$ . Hence (27) is

$$(p_1^{k_1} p_2^{k_2} \cdots p_m^{k_m})^{-\frac{1}{2}} \sum_{p \in S^{\perp}} (F\varphi)(p)) = (p_1^{2l_1 - k_1} p_2^{2l_2 - k_2} \cdots p_m^{2l_m - k_m})^{-\frac{1}{2}} \sum_{x \in S} \varphi(x).$$
(42)

#### Examples

Theorem 3.1.1 is applied to the following two kinds of functions :

$$1.\varphi_i(x) = \exp(-i\pi x^2) \tag{43}$$

$$2.\varphi_{\xi}(x) = \exp(-\xi\pi x^2) \tag{44}$$

where  $\xi \in \mathbf{C}$ ,  $\operatorname{Re}(\xi) > 0$ . Then the infinitesimal Fourier transforms are :

$$1.(F\varphi_i)(p) = \exp(-i\frac{\pi}{4})\overline{\varphi_i(p)}\cdots(\sharp_2)$$
(45)

$$2.(F\varphi_{\xi})(p) = c_{\xi}(p)\varphi_{\xi}(\frac{p}{\xi}),\tag{46}$$

where st( $c_{\xi}(p)$ ) =  $\frac{1}{\sqrt{\xi}}$ , if *p* is finite. Hence the following formulas are obtained :

$$1.|S^{\perp}|^{-\frac{1}{2}}\exp(-i\frac{\pi}{4})\sum_{p\in S^{\perp}}\overline{\varphi_i(p)} = |S|^{-\frac{1}{2}}\sum_{x\in S}\varphi_i(x),$$
(47)

$$2.|S^{\perp}|^{-\frac{1}{2}} \sum_{p \in S^{\perp}} c_{\xi}(p) \varphi_{\xi}(\frac{p}{\xi}) = |S|^{-\frac{1}{2}} \sum_{x \in S} \varphi_{\xi}(x).$$
(48)

When the generator of *S* is  $\varepsilon s$ , this is written as the following, explicitly :

$$1.H\exp(-i\frac{\pi}{4})\sum_{p\in S^{\perp}}\exp(i\pi p^2) = s\sum_{x\in S}\exp(-i\pi x^2)$$
(49)

$$2.H\sum_{p\in S^{\perp}}c_{\xi}(p)\exp(-\frac{1}{\xi}\pi p^2) = s\sum_{x\in S}\exp(-\xi\pi x^2).$$
(50)

The following proposition is obtained:

#### **Proposition 3.1.4.**

(i) If s = H, then the generator of *S* is 1 and  $S = S^{\perp} = L \cap {}^{*}\mathbf{Z}$ . Hence

1. 
$$\exp(-i\frac{\pi}{4}) \sum_{p \in L \cap {}^{*}\mathbf{Z}} \exp(i\pi p^{2}) = \sum_{x \in L \cap {}^{*}\mathbf{Z}} \exp(-i\pi x^{2})$$
 (51)

2. 
$$\sum_{p \in L \cap *\mathbf{Z}} c_{\xi}(p) \exp(-\frac{1}{\xi} \pi p^2) = \sum_{x \in L \cap *\mathbf{Z}} \exp(-\xi \pi x^2).$$
 (52)

Taking their standard parts, we obtain :

$$2.st(\sum_{p \in L \cap *\mathbf{Z}} c_{\xi}(p) \exp(-\frac{1}{\xi} \pi p^{2})) = st(\sum_{x \in L \cap *\mathbf{Z}} \exp(-\xi \pi x^{2}))$$
$$= \sum_{-\infty < n < \infty} \exp(-\xi \pi n^{2}) = \theta(i\xi)$$
(53)

where  $\theta(z)$  is a  $\theta$ -function, defined by  $\theta(z) = \sum_{-\infty < n < \infty} \exp(i\pi z n^2)$ . (ii) If  $\varepsilon s$  is infinitesimal, then the equation:

 $H\sum_{p\in S^{\perp}} c_{\xi}(p)\exp(-\frac{1}{\xi}\pi p^2) = s\sum_{x\in S} \exp(-\xi\pi x^2)$  implies the following:

$$st(\sum_{p\in S^{\perp}} c_{\xi}(p)\exp(-\frac{1}{\xi}\pi p^{2})) = st(\varepsilon s\sum_{x\in S}\exp(-\xi\pi x^{2}))$$
$$= \int_{-\infty}^{\infty}\exp(-\xi\pi x^{2})dx = \frac{1}{\sqrt{\xi}}.$$
(54)

It is known that  $\operatorname{st}(c_{\xi}(p)) = \frac{1}{\sqrt{\xi}}$ , and  $\sum_{-\infty < x < \infty} \exp(-\xi \pi x^2)$  in the formula 2 of (i) is equal to  $\frac{1}{\sqrt{\xi}} \sum_{-\infty by the standard Poisson summation formula. Hence, by 2 of (i), we obtain <math>\operatorname{st}(\sum_{p \in S^{\perp}} c_{\xi}(p) \exp(-\frac{1}{\xi} \pi p^2)) = \sum_{-\infty .$ 

The formula  $(\sharp_2)$  in 1 for  $\varphi_i(x)$  is extended to  $\varphi_{im}(x) = \exp(-im\pi x^2)$ , for an integer *m* so that  $m|2H^2$ . If  $m|\frac{p}{\varepsilon}$ , we recall

$$(F\varphi_{im})(p) = c_{im}(p)\exp(i\pi\frac{1}{m}p^2),$$

where  $c_{im}(p) = \sqrt{\frac{m}{2}} \frac{1+i^{\frac{2H^2}{m}}}{1+i}$  for a positive *m* and  $c_{im}(p) = \sqrt{\frac{-m}{2}} \frac{1+(-i)^{\frac{2H^2}{-m}}}{1-i}$  for a negative *m*. Hence  $|S^{\perp}|^{-\frac{1}{2}} \sum_{p \in S^{\perp}} c_{im}(p) \varphi_{\frac{1}{im}}(p) = |S|^{-\frac{1}{2}} \sum_{x \in S} \varphi_{im}(x)$ . When the generator  $\varepsilon s'$  of  $S^{\perp}$  satisfies m|s', that is, the generator  $\varepsilon s$  of *S* satisfies  $m|\frac{H^2}{s}$ , it reduces to the following:

$$H\sqrt{\frac{m}{2}}\frac{1+i^{\frac{2H^2}{m}}}{1+i}\sum_{p\in S^{\perp}}\exp(i\pi\frac{1}{m}p^2) = s\sum_{x\in S}\exp(-im\pi x^2)$$
(55)

for a positive *m*,

$$H\sqrt{\frac{-m}{2}}\frac{1+(-i)^{\frac{2H^2}{-m}}}{1-i}\sum_{p\in S^{\perp}}\exp(i\pi\frac{1}{m}p^2) = s\sum_{x\in S}\exp(-im\pi x^2)$$
(56)

for a negative *m*.

#### 3.2. Poisson summation formula for Definition 2.2.2

Poisson summation formula of finite group is extended to the double infinitesimal Fourier transform for Definition 2.2.2 on the space of functionals.

#### Formulation

**Theorem 3.2.1.** Let *Y* be an internal subgroup of *X*. Then the following is obtained, for  $f \in A$ ,

$$|Y^{\perp}|^{-\frac{1}{2}} \sum_{b \in Y^{\perp}} (Ff)(b) = |Y|^{-\frac{1}{2}} \sum_{a \in Y} f(a)$$
(57)

where  $Y^{\perp} := \{b \in X \mid \exp(2\pi i < a, b >) = 1 \text{ for } \forall a \in X\}$  and  $\langle a, b \rangle := \sum_{k \in L} a(k)b(k)$ . Lemma 3.2.2.  $|Y^{\perp}| = \frac{|X|}{|Y|}$ . Proof of Lemma 3.2.2. For  $k \in L$ , we denote  $Y_k := \{a(k) \in L' \mid a \in Y\}$ .  $b \in Y^{\perp} \iff \forall a \in Y$ ,  $\exp(2\pi i \sum_{k \in L} a(k)b(k)) = 1$   $\iff \forall k \in L$ ,  $b(k) \in Y_k^{\perp}$   $\iff b : L \to L'$ ,  $\forall k \in L$ ,  $b(k) \in Y_k^{\perp}$ . Hence  $|Y^{\perp}| = \prod_{k \in L} |Y_k^{\perp}|$ . Lemma 3.1.2 implies  $|Y_k^{\perp}| = \frac{H'^2}{|Y_k|}$ . Thus

$$|Y^{\perp}| = \prod_{k \in L} \left(\frac{H'^2}{|Y_k|}\right) = \frac{H'^{2^*H^2}}{\prod_{k \in L} |Y_k|} = \frac{|X|}{|Y|}$$
(58)

Proof of Theorem 3.2.1.

$$|Y^{\perp}|^{-\frac{1}{2}} \sum_{b \in Y^{\perp}} (Ff)(b) = |Y^{\perp}|^{-\frac{1}{2}} \sum_{a \in X} \varepsilon_0 (\sum_{b \in Y^{\perp}} \exp(-2\pi i < a, b >)) f(a).$$
(59)

Since  $\sum_{b \in Y^{\perp}} \exp(-2\pi i < a, b >) = \begin{cases} 0 & (a \notin Y) \\ |Y^{\perp}| & (a \in Y) \end{cases}$ , the above is equal to

$$|Y^{\perp}|^{-\frac{1}{2}}\varepsilon_{0}|Y^{\perp}|\sum_{a\in Y}f(a) = |Y^{\perp}|^{\frac{1}{2}}H'^{-*H^{2}}\sum_{a\in Y}f(a) = |Y|^{-\frac{1}{2}}\sum_{a\in Y}f(a).$$
(60)

In the special case where  $f(a) = \prod_{k \in L} f_k(a(k))$ ,

 $(Ff)(b) = \sum_{a \in X} \varepsilon_0 \exp(-2\pi i \sum_{k \in L} a(k)b(k)) \prod_{k \in L} f_k(a(k))$ 

$$=\prod_{k\in L} (\sum_{a(k)\in L'} \varepsilon' \exp(-2\pi i a(k)b(k))f_k(a(k))).$$
(61)

Namely, the Fourier transform in functional space is the product of those in function space.

#### Corollary 3.2.3.

(i) If each generator of  $Y_k$  is equal to 1, f is written as  $\prod_{k \in L} f_k$ ,  $f_k = *(\operatorname{st}(f_k))|_{L'}$ , and  $\sum_{-\infty < n < \infty} \operatorname{st}(f_k)(n)$  converges, then

$$st(\sum_{b\in Y^{\perp}} (Ff)(b)) = \prod_{k\in L} (\sum_{-\infty < n < \infty} st(f_k)(n)).$$
(62)

(ii) If each generator of  $Y_k$  is infinitesimal, f is written as  $\prod_{k \in L} f_k$ ,  $f_k = *(\operatorname{st}(f_k))|_{L'}$  and  $\operatorname{st}(f_k)$  is  $L_1$ -integrable on **R**, then

$$st(\sum_{b \in Y^{\perp}} (Ff)(b)) = \prod_{k \in L} \int_{-\infty < t < \infty} st(f_k)(t)dt.$$
(63)

#### Examples

Theorem 3.2.1 is applied to the following two kinds of functionals :

$$1.f_i(a) = \exp(-i\pi \sum_{k \in L} a(k)^2)$$
(64)

$$2.f_{\xi}(a) = \exp(-\xi\pi \sum_{k \in L} a(k)^2),$$
(65)

where  $\xi \in \mathbf{C}$ ,  $\operatorname{Re}(\xi) > 0$ .

The infinitesimal Fourier transforms of the functionals are :

$$1.(Ff_i)(b) = (-1)^{\frac{H}{2}} \overline{f_i(b)} \cdots (\sharp_3)$$
(66)

$$2.(Ff_{\xi})(b) = B_{\xi}(b)f_{\xi}(\frac{b}{\xi}), \tag{67}$$

hence the followings are obtained :

$$1.|Y^{\perp}|^{-\frac{1}{2}}(-1)^{\frac{H}{2}}\sum_{b\in Y^{\perp}}\overline{f_i(b)} = |Y|^{-\frac{1}{2}}\sum_{a\in Y}f_i(a)$$
(68)

$$2.|Y^{\perp}|^{-\frac{1}{2}} \sum_{b \in Y^{\perp}} B_{\xi}(b) f_{\xi}(\frac{b}{\xi}) = |Y|^{-\frac{1}{2}} \sum_{a \in Y} f_{\xi}(a).$$
(69)

These are written as the following, explicitly :

$$1.|Y^{\perp}|^{-\frac{1}{2}}(-1)^{\frac{H}{2}}\sum_{b\in Y^{\perp}}\exp(-i\pi\sum_{k\in L}b(k)^{2}) = |Y|^{-\frac{1}{2}}\sum_{a\in Y}\exp(-i\pi\sum_{k\in L}a(k)^{2}),$$
(70)

$$2.|Y^{\perp}|^{-\frac{1}{2}} \sum_{b \in Y^{\perp}} B_{\xi}(b) \exp(-\frac{1}{\xi}\pi \sum_{k \in L} b(k)^2) = |Y|^{-\frac{1}{2}} \sum_{a \in Y} \exp(-\xi\pi \sum_{k \in L} a(k)^2).$$
(71)

Corollary 3.2.3 implies the following proposition 3.2.4.

#### Proposition 3.2.4.

(i) If each generator of  $Y_k$  is equal to 1, then

$$1.(-1)^{\frac{H}{2}}st(\sum_{b\in Y^{\perp}}\exp(-i\pi\prod_{k\in L}b(k)^{2})) = (\sum_{-\infty< n<\infty}\exp(-i\pi n^{2}))^{H^{2}}$$
(72)

$$2.st(\sum_{b\in Y^{\perp}} B_{\xi}(b) \exp(-\frac{1}{\xi}\pi \sum_{k\in L} b(k)^2)) = (\sum_{-\infty < n < \infty} \exp(-\xi\pi n^2))^{H^2}$$
(73)

$$\left(=\left(\theta(i\xi)\right)^{H^2}\right).$$

(ii) If each generator of  $Y_k$  is equal to a natural number  $m_k$ , then

$$1.(-1)^{\frac{H}{2}} st(\sum_{b \in Y^{\perp}} \exp(-i\pi \prod_{k \in L} b(k)^2)) = \prod_{k \in L} (m_k \sum_{-\infty < n < \infty} \exp(-i\pi m_k^2 n^2))$$
(74)

$$2.st(\sum_{b\in Y^{\perp}} B_{\xi}(b) \exp(-\frac{1}{\xi}\pi \sum_{k\in L} b(k)^2)) = \prod_{k\in L} (m_k \sum_{-\infty < n < \infty} \exp(-\xi\pi m_k^2 n^2))$$
(75)

$$\left(=\prod_{k\in L}(m_k\theta(im_k^2\xi))\right).$$

(iii) If each generator of  $Y_k$  is infinitesimal, then

$$2.st(\sum_{b\in Y^{\perp}} B_{\xi}(b) \exp(-\frac{1}{\xi}\pi \sum_{k\in L} b(k)^2)) = (\int_{-\infty}^{\infty} \exp(-\xi\pi t^2) dt)^{H^2}$$
(76)

$$\left(=\left(*\left(\frac{1}{\sqrt{\xi}}\right)\right)^{H^2}\right).$$

The above formula  $(\sharp_3)$  for  $f_i(a)$  is extended to  $f_{im}(a) = \exp(-im\pi \sum_{k \in L} a^2(k))$ , for an integer m so that  $m|2H'^2$ . If  $m|\frac{b(k)}{\epsilon'}$ , we recall

$$(Ff_{im})(b) = B_{im}(b)f_{\frac{1}{im}}(b)$$
 (77)

where  $B_{im}(b) = \left(\sqrt{\frac{m}{2}} \frac{1+i^{\frac{2H'^2}{m}}}{1+i}\right)^{(*H)^2}$  for a positive *m*,  $B_{im}(b) = \left(\sqrt{\frac{-m}{2}} \frac{1+(-i)^{\frac{2H'^2}{-m}}}{1-i}\right)^{(*H)^2}$  for a negative *m*.

Hence  $|Y^{\perp}|^{-\frac{1}{2}} \sum_{b \in Y^{\perp}} B_{im}(b) f_{\frac{1}{im}}(b) = |Y|^{-\frac{1}{2}} \sum_{a \in Y} f_{im}(a)$ . When each generator  $\varepsilon' s'_k$  of  $Y_k^{\perp}$  satisfies  $m|s'_k$ , that is, each generator  $\varepsilon' s_k$  of  $Y_k$  satisfies  $m|\frac{H'^2}{s_k}$ , it reduces to the following :

$$H^{\prime(*H)^{2}}\left(\sqrt{\frac{m}{2}}\frac{1+i^{\frac{2H^{\prime2}}{m}}}{1+i}\right)^{(*H)^{2}}\sum_{b\in Y^{\perp}}\exp(i\pi\frac{1}{m}\sum_{k\in L}b(k)^{2}) = \prod_{k\in L}s_{k}\sum_{a\in Y}\exp(-im\pi\sum_{k\in L}a(k)^{2})$$
(78)

for a positive *m*, and

$$H^{\prime(*H)^{2}}\left(\sqrt{\frac{-m}{2}}\frac{1+(-i)^{\frac{2H^{\prime2}}{-m}}}{1-i}\right)^{(*H)^{2}}\sum_{b\in Y^{\perp}}\exp(i\pi\frac{1}{m}\sum_{k\in L}b(k)^{2})$$
$$=\prod_{k\in L}s_{k}\sum_{a\in Y}\exp(-im\pi\sum_{k\in L}a(k)^{2})$$
(79)

for a negative *m*.

If  $s_k = H'$  and m|H', then

$$\left(\sqrt{\frac{m}{2}}\frac{1+i^{\frac{2H'^2}{m}}}{1+i}\right)^{(*H)^2} \sum_{b \in Y^{\perp}} \exp(i\pi \frac{1}{m}\sum_{k \in L} b(k)^2) = \sum_{a \in Y} \exp(-im\pi \sum_{k \in L} a(k)^2)$$
(80)

for a positive *m*, and

$$\left(\sqrt{\frac{-m}{2}}\frac{1+(-i)^{\frac{2H'^2}{-m}}}{1-i}\right)^{(*H)^2}\sum_{b\in Y^{\perp}}\exp(i\pi\frac{1}{m}\sum_{k\in L}b(k)^2) = \sum_{a\in Y}\exp(-im\pi\sum_{k\in L}a(k)^2)$$
(81)

for a negative *m*, that is,

$$\left(\sqrt{m}\exp(-i\frac{\pi}{4})\right)^{(*H)^2} \sum_{b\in Y^{\perp}} \exp(i\pi\frac{1}{m}\sum_{k\in L}b(k)^2) = \sum_{a\in Y}\exp(-im\pi\sum_{k\in L}a(k)^2)$$
(82)

for a positive *m*, and

$$\left(\sqrt{-m}\exp(i\frac{\pi}{4})\right)^{(*H)^2} \sum_{b \in Y^{\perp}} \exp(i\pi\frac{1}{m}\sum_{k \in L} b(k)^2) = \sum_{a \in Y} \exp(-im\pi\sum_{k \in L} a(k)^2)$$
(83)

for a negative *m*.

#### 3.3. Poisson summation formula for Definition 2.2.3

Poisson summation formula of finite group is extended to the double infinitesimal Fourier transformation for Definition 2.2.3 on the space of functionals originally defined in [8].

#### Formulation

The following theorem for Definition 2.2.3 is obtained as the argument in the section 3.2.

**Theorem 3.3.1.** Let *Y* be an internal subgroup of *X*. Then the following is obtained, for  $f \in A$ ,

$$|Y^{\perp\varepsilon}|^{-\frac{1}{2}} \sum_{b \in Y^{\perp\varepsilon}} (Ff)(b) = |Y|^{-\frac{1}{2}} \sum_{a \in Y} f(a)$$
(84)

where  $\langle a, b \rangle_{\varepsilon} := {}^{*} \varepsilon \sum_{k \in L} a(k)b(k)$  and  $Y^{\perp \varepsilon} := \{b \in X \mid \exp(2\pi i \langle a, b \rangle_{\varepsilon}) = 1 \text{ for } \forall a \in Y\}.$ Lemma 3.3.2.  $|Y^{\perp \varepsilon}| = \frac{|X|}{|Y|}.$ Proof of Lemma 3.3.2. For  $k \in L$ , it is denoted  $Y_k := \{a(k) \in L' \mid a \in Y\}.$   $b \in Y^{\perp \varepsilon} \iff \forall a \in Y, \exp(2\pi i {}^{*} \varepsilon \sum_{k \in L} a(k)b(k)) = 1$   $\iff \forall k \in L, {}^{*} \varepsilon b(k) \in Y_k^{\perp}.$ For  $k \in L$ , generators defined by the following are written as m, n : $Y_k = \langle \varepsilon'm \rangle, \{b(k) \in L' \mid {}^{*} \varepsilon b(k) \in Y_k^{\perp}\} = \langle \varepsilon'n \rangle.$ 

Now

$$\exp(2\pi i^{*}\varepsilon\varepsilon' m\varepsilon' n) = 1 \iff {}^{*}\varepsilon\varepsilon' m\varepsilon' n = 1.$$
(85)

It is written  $Y_k^{\perp \varepsilon} := \{b(k) \in L' \mid \star \varepsilon b(k) \in Y_k^{\perp}\}$ . Then  $|Y_k^{\perp \varepsilon}| = m$ . This is equal to  $\frac{\star HH'^2}{\star HH'^2/m} = \frac{|L'|}{|Y_k|}$ . Hence

$$|Y^{\perp\varepsilon}| = \prod_{k\in L} |Y_k^{\perp\varepsilon}| = \frac{|X|}{|Y|}.$$
(86)

Proof of Theorem 3.3.1.

$$|Y^{\perp\varepsilon}|^{-\frac{1}{2}} \sum_{b \in Y^{\perp\varepsilon}} (Ff)(b) = |Y^{\perp\varepsilon}|^{-\frac{1}{2}} \sum_{a \in X} \varepsilon_0 (\sum_{b \in Y^{\perp\varepsilon}} \exp(-2\pi i < a, b >_{\varepsilon})) f(a).$$
(87)

Since  $\sum_{b \in Y^{\perp \varepsilon}} \exp(-2\pi i < a, b >_{\varepsilon}) = \begin{cases} 0 & (a \notin Y) \\ |Y^{\perp \varepsilon}| & (a \in Y) \end{cases}$ , the above is equal to

$$|Y^{\perp\varepsilon}|^{-\frac{1}{2}}\varepsilon_0|Y^{\perp\varepsilon}|\sum_{a\in Y}f(a) = |Y|^{-\frac{1}{2}}\sum_{a\in Y}f(a).$$
(88)

The following is obtained:

#### Corollary 3.3.3.

(i) If each generator of  $Y_k$  is equal to 1, f is written as  $\prod_{k \in L} f_k$ ,  $f_k = *(\operatorname{st}(f_k))|_{L'}$ , and  $\sum_{-\infty < n < \infty} \operatorname{st}(f_k)(n)$  converges, then

$$H^{\frac{H^2}{2}}st(\sum_{b\in Y^{\perp}} (Ff)(b)) = \prod_{k\in L} (\sum_{-\infty < n < \infty} st(f_k)(n)).$$
(89)

(ii) If each generator of  $Y_k$  is infinitesimal, f is written as  $\prod_{k \in L} f_k$ ,  $f_k = *(\operatorname{st}(f_k))|_{L'}$ , and  $\operatorname{st}(f_k)$  is  $L_1$ -integrable on **R**, then

$$H^{\frac{H^2}{2}}st(\sum_{b\in Y^{\perp}} (Ff)(b)) = \prod_{k\in L} \int_{-\infty}^{\infty} st(f_k)(t)dt.$$
(90)

Examples Theorem 3.3.1 is applied to the following two functionals :

$$1.g_i(a) = \exp(-i\pi^* \varepsilon \sum_{k \in L} a(k)^2)$$
(91)

$$2.g_{\xi}(a) = \exp(-\xi \pi^* \varepsilon \sum_{k \in L} a(k)^2)$$
(92)

where  $\xi \in \mathbf{C}$ ,  $\operatorname{Re}(\xi) > 0$ . The infinitesimal Fourier transforms are :

$$1.(Fg_i)(b) = (-1)^{\frac{H}{2}} \overline{g_i(b)} \cdots (\sharp_4)$$
(93)

$$2.(Fg_{\xi})(b) = C_{\xi}(b)g_{\xi}(\frac{b}{\xi})$$
(94)

hence the following formulas are obtained :

$$1.|Y^{\perp\varepsilon}|^{-\frac{1}{2}}(-1)^{\frac{H}{2}}\sum_{b\in Y^{\perp\varepsilon}}\overline{g_i(b)} = |Y|^{-\frac{1}{2}}\sum_{a\in Y}g_i(a)$$
(95)

$$2.|Y^{\perp\varepsilon}|^{-\frac{1}{2}}\sum_{b\in Y^{\perp\varepsilon}}C_{\xi}(b)g_{\xi}(\frac{b}{\xi}) = |Y|^{-\frac{1}{2}}\sum_{a\in Y}g_{\xi}(a).$$
(96)

These are written as the following, explicitly :

$$1.|Y^{\perp\varepsilon}|^{-\frac{1}{2}}(-1)^{\frac{H}{2}}\sum_{k\in Y^{\perp\varepsilon}}\exp(-i\pi^{\star\varepsilon}\sum_{k\in L}b(k)^{2}) = |Y|^{-\frac{1}{2}}\sum_{a\in Y}\exp(-i\pi^{\star\varepsilon}\sum_{k\in L}a(k)^{2})$$
(97)

$$2.|Y^{\perp\varepsilon}|^{-\frac{1}{2}}\sum_{b\in Y^{\perp\varepsilon}}C_{\xi}(b)\exp(-\frac{1}{\xi}\pi^{\star}\varepsilon\sum_{k\in L}a(k)^{2}) = |Y|^{-\frac{1}{2}}\sum_{a\in Y}\exp(-\xi\pi^{\star}\varepsilon\sum_{k\in L}a(k)^{2}).$$
 (98)

Corollaly 3.3.3 implies the following proposition 3.3.4.

#### Proposition 3.3.4.

(i) If each generator of  $Y_k$  is equal to 1, then the standard parts are :

$$1.H^{\frac{H^2}{2}}(-1)^{\frac{H}{2}}st(\sum_{b\in Y_{\varepsilon}^{\perp}}\exp(-i\pi\varepsilon\sum_{k\in L}b(k)^2)) = (\sum_{-\infty< n<\infty}\exp(-i\pi\varepsilon n^2))^{H^2}$$
(99)

$$2.H^{\frac{H^2}{2}}st(\sum_{b\in Y_{\varepsilon}^{\perp}}C_{\xi}(b)\exp(-\frac{1}{\xi}\pi\varepsilon\sum_{k\in L}b(k)^2)) = (\sum_{-\infty< n<\infty}\exp(-\xi\pi\varepsilon n^2))^{H^2}$$
(100)

$$\left(=(\theta(i\xi))^{H^2}\right)$$

(ii) If each generator of  $Y_k$  is equal to a natural number  $m_k$ , then

$$1.H^{\frac{H^2}{2}}(-1)^{\frac{H}{2}}st(\sum_{k\in Y_{\varepsilon}^{\perp}}\exp(-i\pi\varepsilon\sum_{k\in L}b(k)^2)) = \prod_{k\in L}(m_k\sum_{-\infty < n < \infty}\exp(-i\pi\varepsilon m_k^2n^2))$$
(101)

$$2.H^{\frac{H^2}{2}}st(\sum_{b\in Y_{\varepsilon}^{\perp}}C_{\xi}(b)\exp(-\frac{1}{\xi}\pi\varepsilon\sum_{k\in L}b(k)^2)) = \prod_{k\in L}(m_k\sum_{-\infty< n<\infty}\exp(-\xi\pi\varepsilon m_k^2n^2))$$
(102)

$$\left(=\prod_{k\in L}(m_k\theta(im_k^2\xi))\right)$$

(iii) If each generator of  $Y_k$  is infinitesimal, then

$$2.st\left(\sum_{b\in Y_{\varepsilon}^{\perp}} C_{\xi}(b) \exp\left(-\frac{1}{\xi}\pi\varepsilon\sum_{k\in L} b(k)^{2}\right)\right) = \left(\int_{-\infty}^{\infty} \exp\left(-\xi\pi t^{2}\right) dt\right)^{H^{2}}$$
(103)

$$\left(=\left(*\left(\frac{1}{\sqrt{\zeta}}\right)\right)^{H^2}\right).$$

The above formulation  $(\sharp_4)$  of  $g_i(a)$  is extended to  $g_{im}(a) = \exp(-im\pi^* \varepsilon \sum_{k \in L} a^2(k))$ , for an integer *m* so that  $m|2^*HH'^2$ . If  $m|\frac{b(k)}{\varepsilon'}$  for an arbitrary  $k \in L$ , it is recalled

$$(Fg_{im})(b) = C_{im}(b)g_{\frac{1}{im}}(b), \text{ where } C_{im}(b) = \left(\sqrt{\frac{m}{2}}\frac{1+i\frac{2^{*}HH'^2}{m}}{1+i}\right)^{*H^2} \text{ for a positive } m \text{ and}$$
$$C_{im}(b) = \left(\sqrt{\frac{-m}{2}}\frac{1+(-i)\frac{2^{*}HH'^2}{m}}{1-i}}\right)^{*H^2} \text{ for a negative } m.$$

Hence  $|Y^{\perp_{\varepsilon}}|^{-\frac{1}{2}} \sum_{b \in Y^{\perp}} C_{im}(b) g_{\frac{1}{im}}(b) = |Y|^{-\frac{1}{2}} \sum_{a \in Y} g_{im}(a)$ . When each generator  $\varepsilon' s'_k$  of  $Y_k^{\perp_{\varepsilon}}$  satisfies  $m|s'_k$ , that is, each generator  $\varepsilon' s_k$  of  $Y_k$  satisfies  $m|\frac{*HH'^2}{s_k}$ , it reduces to the following:

$$H^{\frac{H^2}{2}}H'^{(*H)^2}\left(\sqrt{\frac{m}{2}}\frac{1+i\frac{2^{*HH'^2}}{m}}{1+i}\right)^{(*H)^2}\sum_{b\in Y^{\perp_{\varepsilon}}}\exp(i\pi\frac{1}{m}*\varepsilon\sum_{k\in L}b(k)^2)$$
$$=\prod_{k\in L}s_k\sum_{a\in Y}\exp(-im\pi*\varepsilon\sum_{k\in L}a(k)^2)$$
(104)

for a positive *m*, and

$$H^{\frac{H^{2}}{2}}H'^{(*H)^{2}}\left(\sqrt{\frac{-m}{2}}\frac{1+(-i)^{\frac{2^{*}HH'^{2}}{-m}}}{1-i}\right)^{(*H)^{2}}\sum_{b\in Y^{\perp_{\varepsilon}}}\exp(i\pi\frac{1}{m}\,^{*}\varepsilon\sum_{k\in L}b(k)^{2})$$
$$=\prod_{k\in L}s_{k}\sum_{a\in Y}\exp(-im\pi\,^{*}\varepsilon\sum_{k\in L}a(k)^{2})$$
(105)

for a negative *m*. If  $s_k = H'$  and m|H', then

$$H^{\frac{H^{2}}{2}}\left(\sqrt{\frac{m}{2}}\frac{1+i^{\frac{2^{\star}HH^{\prime2}}{m}}}{1+i}\right)^{(^{\star}H)^{2}}\sum_{b\in Y^{\perp\varepsilon}}\exp(i\pi\frac{1}{m}\sum_{k\in L}b(k)^{2}) = \sum_{a\in Y}\exp(-im\pi^{\star}\varepsilon\sum_{k\in L}a(k)^{2})$$
(106)

for a positive *m*, and

$$H^{\frac{H^{2}}{2}}\left(\sqrt{\frac{-m}{2}}\frac{1+(-i)^{\frac{2^{*}HH'^{2}}{-m}}}{1-i}\right)^{\binom{*}{H}^{2}}\sum_{b\in Y^{\perp_{\varepsilon}}}\exp(i\pi\frac{1}{m}\sum_{k\in L}b(k)^{2})$$
$$=\sum_{a\in Y}\exp(-im\pi^{*}\varepsilon\sum_{k\in L}a(k)^{2})$$
(107)

for a negative *m*, that is,

$$H^{\frac{H^2}{2}}\left(\sqrt{m}\exp(-i\frac{\pi}{4})\right)^{(*H)^2}\sum_{b\in Y^{\perp_{\varepsilon}}}\exp(i\pi\frac{1}{m}\sum_{k\in L}b(k)^2) = \sum_{a\in Y}\exp(-im\pi^{*\varepsilon}\sum_{k\in L}a(k)^2) \quad (108)$$

for a positive *m*, and

$$H^{\frac{H^2}{2}}\left(\sqrt{-m}\exp(i\frac{\pi}{4})\right)^{(*H)^2}\sum_{b\in Y^{\perp_{\varepsilon}}}\exp(i\pi\frac{1}{m}\sum_{k\in L}b(k)^2) = \sum_{a\in Y}\exp(-im\pi^*\varepsilon\sum_{k\in L}a(k)^2) \quad (109)$$

for a negative *m*.

#### 4. Quantum field theory and Zeta function

In this section the quantum field theory is developed by using the double infinitesimal Fourier transform. The propagator for a system of the harmonic oscillators is considered in the quantum field theory.

#### 4.1. Path integral in the quantum field theory

**Definition4.1.1.** A path integral of  $f \in A$  is defined as follows:

$$\sum_{a \in X} \varepsilon_0 f(a) \tag{110}$$

with  $\varepsilon_0 := (H')^{-(*H)^2} \in *(*\mathbf{R}).$ 

It is briefly explained that the complexification of the propagator for the harmonic oscillator is represented as the following path integral. In Feynman's formulation of quantum mechanics([2]), the propagator of the one-dimensional harmonic oscillator is the following path integral:  $K(q, q_0, t)$ 

$$= \lim_{n \to \infty} \int_{\mathbf{R}^n} \left(\frac{m}{2\pi i \hbar \epsilon}\right)^{(n+1)/2} \exp\left(\frac{i\epsilon}{\hbar} \sum_{j=1}^{n+1} \left(\frac{m}{2} \left(\frac{x_j - x_{j-1}}{\epsilon}\right)^2 - \frac{m}{2} \lambda^2 x_j^2\right)\right) dx_1 dx_2 \cdots dx_n \quad (111)$$

where  $x_0 = q_0$ ,  $x_{n+1} = q$ ,  $\epsilon = \frac{t}{n}$ . In nonstandard analysis, it is known that, for a sequence an,

$$\lim_{n \to \infty} a_n = a \quad iff \quad {}^*a_w \approx a \tag{112}$$

for any infinite natural number  $\omega \in \mathbf{N} - \mathbf{N}$ , where  $a_n$  is the \* extension of  $\{a_n\}_{n \in \mathbb{N}}$ , and  $\approx$  means that  $a_w - a$  is infinitesimal, that is, the standard part of  $a_w$  is a, usually denoted by  $st(a_w) = a$ . The standard part of the nonstandard path integral is written as

$$st \int_{*\mathbf{R}^w} \left(\frac{m}{2\pi i\hbar\epsilon}\right)^{(\omega+1)/2} \exp\left(\frac{i\epsilon}{\hbar} \sum_{j=1}^{w+1} \left(\frac{m}{2} \left(\frac{x_j - x_{j-1}}{\epsilon}\right)^2 - \frac{m}{2}\lambda^2 x_j^2\right)\right) dx_1 dx_2 \cdots dx_w.$$
(113)

By extending *t* to a complex number, the path integral is complexified to the following :

$$st \int_{*\mathbf{R}^w} \left(\frac{m}{2\pi i\hbar\epsilon}\right)^{(\omega+1)/2} \exp\left(\frac{i\epsilon}{\hbar} \sum_{j=1}^{w+1} \left(\frac{m}{2} \left(\frac{x_j - x_{j-1}}{\epsilon}\right)^2 - \frac{m}{2}\lambda^2 x_j^2\right)\right) dx_1 dx_2 \cdots dx_w.$$
(114)

**Theorem 4.1.2.** Let  $t \in \mathbf{R}$ ,  $t \neq st(\pm \frac{\sqrt{2}n}{\lambda}\sqrt{1 - \cos(\frac{k\pi}{\omega+1})})$ ,  $k = 1, 2, \cdots, \omega$ , or for  $t \in \mathbf{C}$ , whose imaginary part is negative. The complexified one-dimensional harmonic oscillator standard functional integral is given by  $(\frac{m}{2\pi i\hbar})^{\frac{1}{2}}\sqrt{\frac{\lambda}{\sin(\lambda t)}}\exp(\frac{im}{\hbar}\frac{\lambda}{\sin\lambda t}((q_0^2 + q^2)\cos\lambda t - 2qq_0))$ .

**Proof.** If  $t \neq st(\pm \frac{\sqrt{2}n}{\lambda}\sqrt{1-\cos(\frac{k\pi}{\omega+1})}), k = 1, 2, \cdots, \omega$ , then

$$t \neq \pm \frac{\sqrt{2}n}{\lambda} \sqrt{1 - \cos(\frac{k\pi}{\omega + 1})}, k = 1, 2, \cdots, \omega$$
(115)

for arbitrary infinite number  $\omega$ . The theorem is followed from the discrete calculation using the matrix representation of the operator(cf. [7]).

It corresponds to the well-known real propagator for one dimensional harmonic oscillator. For the d-dimensional harmonic oscillator, *d*-dimensional vectors are written as  $\mathbf{q}_0, \mathbf{q}$ , the square norms are  $|\mathbf{q}_0|^2$ ,  $|\mathbf{q}|^2$ , and the inner product of  $\mathbf{q}_0$ ,  $\mathbf{q}$  is  $\mathbf{q}_0\mathbf{q}$ . We have :

**Corollary 4.1.3.** For the complexified d-dimensional harmonic oscillator standard functional integral, the complexified propagator is given by

$$\left(\frac{m}{2\pi i\hbar}\right)^{\frac{d}{2}} \left(\frac{\lambda}{\sin(\lambda t)}\right)^{\frac{d}{2}} \exp\left(\frac{im}{\hbar} \frac{\lambda}{\sin \lambda t} \left(\left(|\mathbf{q}_0|^2 + |\mathbf{q}|^2\right) \cos \lambda t - 2\mathbf{q}\mathbf{q}_0\right)\right).$$
(116)

**Proof.** By factorizing Theorem 4.1.2 into a product on d dimensional, the corollary is obtained.

The trace of the complexified propagator is calculated for one dimensional harmonic oscillator.

Since

$$\int_{-\infty}^{\infty} \left(\frac{m}{2\pi i\hbar}\right)^{\frac{1}{2}} \sqrt{\frac{\lambda}{\sin(\lambda t)}} \exp\left(\frac{im}{\hbar} \frac{\lambda}{\sin\lambda t} 2\left((\cos\lambda t - 1)q^2\right)\right) dq = \frac{1}{2i\sin(\lambda t/2)}$$
(117)

the following is obtained (cf.[6],[7]):

**Theorem 4.1.4.** Let  $t \in \mathbf{R}$ ,  $t \neq \pm st(\frac{\sqrt{2\omega}}{\lambda}\sqrt{1-\cos(\frac{k\pi}{\omega+1})})$ ,  $k = 1, 2, \dots, \omega$ , or  $t \in \mathbf{C}$ , whose imaginary part is negative. The trace of the complexified one-dimensional harmonic oscillator standard functional integral is given by  $\frac{1}{2i\sin(\lambda t/2)}$ .
**Proof.** By putting  $q_0 = q$  in  $\left(\frac{m}{2\pi i \hbar}\right)^{\frac{1}{2}} \sqrt{\frac{\lambda}{\sin(\lambda t)}} \exp\left(\frac{im}{\hbar} \frac{\lambda}{\sin\lambda t} \left(\left(q_0^2 + q^2\right) \cos\lambda t - 2qq_0\right)\right)$ , the trace is the following integral :

$$\int_{-\infty}^{\infty} \left(\frac{m}{2\pi i\hbar}\right)^{\frac{1}{2}} \sqrt{\frac{\lambda}{\sin(\lambda t)}} \exp\left(\frac{im}{\hbar} \frac{\lambda}{\sin\lambda t} 2\left((\cos\lambda t - 1)q^2\right)\right) dq = \frac{1}{2i\sin(\lambda t/2)}.$$
 (118)

**Corollary 4.1.5.** If the potential is modified to  $V(q) = \frac{m}{2}(\frac{\lambda^2}{2}|q|^2 - \frac{\lambda}{2})$ , then the trace is  $\frac{1}{2i\sin(\lambda t/2)}\exp(\frac{\lambda t}{2})$ .

For the d-dimensional harmonic oscillator, the following is obtained :

**Corollary 4.1.6.** For the trace of the modified complexified propagator for d-dimensional harmonic oscillator, the trace is  $(\frac{1}{2i\sin(\lambda t/2)}\exp(\frac{\lambda t}{2})))^d$ .

In the next section, Corollaries 4.1.5 and 4.1.6 are used to treat an infinite dimensional harmonic oscillator.

#### 4.2. Representation of the zeta function.

Corollary 4.1.5 is extended to an infinite dimensional harmonic oscillator using nonstandard analysis. For it the three types of extension \***R** ,\*\***R**, #\*\***R** of **R** are prepared corresponding to Definition 2.2.2 , then the three stages of infinite numbers exist. In these three extension fields, we fix infinite natural numbers  $H_F \in *\mathbf{N}$ ,  $H_T \in **\mathbf{N}$ ,  $H'' \in 2^{\#**}\mathbf{N}$ . Let *T* be a positive standard real number and let  $\epsilon_T$  ,  $\epsilon''$  be infinitesimals in \*\***R** , #\*\***R** defined by  $\frac{T}{H_T}$ ,  $\frac{1}{H''}$ . A lattice *L*" and two function space *X*, *A* are defined as the following:

$$L'' := \left\{ \varepsilon'' z'' \ \left| z'' \in ^{\# * *} \mathbf{Z}, -\frac{\mathbf{H}''}{2} \leq '''' \mathbf{z}'' < \frac{\mathbf{H}''}{2} \right\} \right\}.$$
  
$$X := \left\{ \alpha :^{\# *} \{ 0, 1, \cdots .H_F - 1 \} \to L'', internal \right\},$$
  
$$A := \left\{ a :^{\#} \{ 0, 1, \cdots .H_T \} \to X, internal \right\}.$$

Then an element *a* of *A* is written as the component  $(a_j^k, 0 \le j \le H_T, 0 \le k \le H_F - 1)$ . All prime numbers are ordered as p(1) = 2, p(2) = 3, ..., p(n) < p(n+1), ..., that is, *p* is a mapping from **N** to the set of prime numbers,  $p : \mathbf{N} \to \{\text{prime number}\}$ . Let  $\lambda_k$  be  $\ln^* p(k)$  for each *k*,  $0 \le k \le H_F - 1$ . A potential  $V_k : \#^* \mathbf{R} \to \#^* \mathbf{R}$  is defined for each *k*,  $0 \le k \le H_F - 1$ , as  $V_k(q) = \frac{\lambda_k^2}{2} |q|^2 - \frac{\lambda_k}{2}$ . An element  $\alpha$  of *X* is written as the component  $\alpha = (\alpha^k, 0 \le k \le H_F - 1)$ .

Let *V* be a global potential as the following:

$$V(\alpha) = \sum_{k=0}^{H_F - 1} V_k(\alpha^k) \left( = \sum_{k=0}^{H_F - 1} \left( \frac{\lambda_k^2}{2} \left| \alpha^k \right|^2 - \frac{\lambda_k}{2} \right) \right).$$
(119)

In order to transport *t* to later, the element  $-\frac{\lambda_k}{2}$  is put in the usual potential for harmonic oscillators. It is considered the following summation K(a, b, t) depending of  $a, b \in X$ :

$$K(a,b,t) = \sum_{a \in A, a_0 = a.a_{H_T} = b} ((\epsilon')^{H_F})^{H_T} ((\frac{1}{2\pi\epsilon_T})^{H_F})^{H_T} \exp(\epsilon_T (\frac{1}{2}\sum_{j=1}^{H_T} |\frac{a_j - a_{j-1}}{\epsilon_T}|^2 - V(a_j))).$$
(120)

Then K(a, b, t) is calculated,

$$K(a,b,t) = \left(\frac{1}{2\pi\epsilon_T}\right)^{H_T} \prod_{k=1}^{H_F-1} \sum_{a_j^k \in L', 0 \le j \le H_T-1} (\epsilon')^{H_T} \left(\frac{1}{2\pi\epsilon_T}\right)^{H_T} \exp\left(\epsilon_T \left(\frac{1}{2}\sum_{j=1}^{H_T} |\frac{a_j^k - a_{j-1}^k}{\epsilon_T}|^2 - V(a_j^k)\right)\right), \quad (121)$$

where  $a_0 = a, a_{H_T} = b$ .

The summation  $\sum_{a \in X} (\epsilon')^{H_T} K(a, a.t)$  is denoted by tr(K(a, a, t)). Three correspondences putting standard parts are written as  $st_{\#} : {}^{\# \star *} \mathbf{R} \to {}^{\star *} \mathbf{R}$ ,  $st_{\star} : {}^{\star *} \mathbf{R} \to {}^{*} \mathbf{R}$ ,  $st_{\star} : {}^{*} \mathbf{R} \to \mathbf{R}$ ,  $st_{\star} : {}^{*} \mathbf{R} \to \mathbf{R}$ . When there are no confusion, they are simply written as st. The composition  $st_{\star} \circ st_{\star} \circ st_{\#} : {}^{\# \star *} \mathbf{R} \to \mathbf{R}$  is denoted also by st for simplicity.

**Theorem 4.2.1.** If the real part of *t* is greater than 1, the standard part st(tr(K(a, a, t))) of tr(K(a, a, t)) corresponds to Riemann's zeta function  $\zeta(t)$ .

Proot. The standard parts of tr(K(a, a, t)) as follows.

$$st_{\#}(tr(K(a, a, t))) = \prod_{k=1}^{H_{F}-1} \int \int \cdots \int (\frac{1}{2\pi\epsilon_{T}})^{H_{T}} \exp(\epsilon_{T}(\frac{1}{2}\sum_{j=1}^{H_{T}}(\frac{q_{j}^{k}-q_{j-1}^{k}}{\epsilon_{T}})^{2} - V(q_{j}^{k}))) dq_{0}^{k} dq_{1}^{k} \cdots dq_{H_{T}-1}^{k}$$
(122)

$$=\prod_{k=1}^{H_{F}-1}\int\{\int\cdots\int(\frac{1}{2\pi\epsilon_{T}})^{H_{T}}\exp(\epsilon_{T}(\frac{1}{2}\sum_{j=1}^{H_{T}}(\frac{q_{j}^{k}-q_{j-1}^{k}}{\epsilon_{T}})^{2}-V(q_{j}^{k})))dq_{1}^{k}\cdots dq_{H_{T}-1}^{k}\}dq_{0}^{k}$$
(123)

by Fubini's theorem. Furthermore,

$$st_{\star}st_{\#}(tr(K(a,a,t))) =$$

$$= \prod_{k=1}^{H_{F}-1} st_{\star} \{ \int \{ \int \cdots \int (\frac{1}{2\pi\epsilon_{T}})^{H_{T}} \exp(\epsilon_{T}(\frac{1}{2}\sum_{j=1}^{H_{T}}(\frac{q_{j}^{k}-q_{j-1}^{k}}{\epsilon_{T}})^{2} - V(q_{j}^{k}))) dq_{1}^{k} \cdots dq_{H_{T}-1}^{k} \} dq_{0}^{k} \}$$
(124)

by the same calculation of Theorem 4.1.2 (cf.[6],[7]),

$$=\prod_{k=0}^{H_F-1} \left(\frac{1}{2i\sin(\frac{\lambda_k t}{2i})}\exp(\frac{\lambda_k t}{2})\right) = \prod_{k=0}^{H_F-1} \frac{1}{1-p_k^{-t}}.$$
(125)

By Lebesque's convergence theorem,  $(st_*(st_*(st_*(tr(K(a, a, t))))) = \prod_{k=0}^{\infty} \frac{1}{1-p_k^{-t}} = \zeta(t)$ , if the real part of *t* is positive.

#### 4.2. Another representation of the zeta function

In this section, both  $st_*, st_*$  and  $st_\#$  are denoted as st for the simplification. A functional is defined on X, and a relationship between the functional and Riemann's zeta function is shown later. The nonstandard extension  $*p : *N \to *\{\text{prime number}\}\)$  is written as  $*p([l_\mu]) = [p(l_\mu)]$ , and a mapping  $\tilde{p} : *N \to *(*\{\text{prime number}\})\)$  is defined as  $\tilde{p}([l_\mu]) = *[p(l_\mu)]$ . For  $s \in \mathbf{C}$ ,  $Z_s(\in A)$  is defined as the following :

$$Z_s(a) := \prod_{k \in L} \tilde{p}(H(k + \frac{H}{2}) + 1)^{(-s(a(k) + \frac{H'}{2}))}.$$
(126)

Now  $H(k + \frac{H}{2}) + 1$  is an element of \*N and a(k) + H'/2 is an element of \*(\*N). Then  $Z_s(a)$  is calculated as  $\exp(-s\sum_{k\in L}\log(\tilde{p}(H(k + \frac{H}{2}) + 1))a(k))\prod_{k\in L}\tilde{p}(H(k + \frac{H}{2}) + 1)^{-s\frac{H'}{2}}$ . The following theorem is obtained for the Fourier transform of  $Z_s$  for Definition 2.2 1: **Theorem 4.3.1.** 

$$(F((Z_s))(b) = \left(\prod_{k \in L} \tilde{p}(H(k + \frac{H}{2}) + 1)\right)^{-s\frac{H'}{2}}$$

$$\cdot \prod_{k \in L} \varepsilon' \frac{\sinh((2\pi i b(k) + s \log \tilde{p}(H(k + \frac{H}{2}) + 1))\frac{H'}{2})}{\exp(-\frac{\varepsilon'}{2}(2\pi i b(k) + s \log \tilde{p}(H(k + \frac{H}{2}) + 1))\sinh(\frac{\varepsilon'}{2}(2\pi i b(k) + s \log \tilde{p}(H(k + \frac{H}{2}) + 1))}.$$
(127)

Proof.

$$(F((Z_s))(b) = \left(\prod_{k \in L} \tilde{p}(H(k + \frac{H}{2}) + 1)\right)^{-s\frac{H'}{2}}$$
$$\cdot \sum_{a \in X} \varepsilon_0 \exp(-s\sum_{k \in L} \log \tilde{p}(H(k + \frac{H}{2}) + 1)a(k)) \exp(-2\pi i\sum_{k \in L} a(k)b(k))$$
$$= \left(\prod_{k \in L} \tilde{p}(H(k + \frac{H}{2}) + 1)\right)^{-s\frac{H'}{2}} \cdot \sum_{a \in X} \varepsilon_0 \exp(-(2\pi i b(k) + s\log \tilde{p}(H(k + \frac{H}{2}) + 1))a(k))$$
$$= \left(\prod_{k \in L} \tilde{p}(H(k + \frac{H}{2}) + 1)\right)^{-s\frac{H'}{2}}$$

$$\cdot \prod_{k \in L} \varepsilon' \frac{\sinh((2\pi i \, b(k) + s \log \tilde{p}(H(k + \frac{H}{2}) + 1))\frac{H'}{2})}{\exp(-\frac{\varepsilon'}{2}(2\pi i \, b(k) + s \log \tilde{p}(H(k + \frac{H}{2}) + 1))\sinh(\frac{\varepsilon'}{2}(2\pi i \, b(k) + s \log \tilde{p}(H(k + \frac{H}{2}) + 1))})}$$

Riemann's zeta function  $\zeta(s)$  is defined by  $\zeta(s) = \prod_{l=1}^{\infty} \frac{1}{1-p(l)^{-s}}$  for  $\operatorname{Re}(s) > 1$ . Let  $Y_{\mathbb{Z}}$  be a subgroup of *X* so that each generator of  $(Y_{\mathbb{Z}})_k$  is equal to 1. Then the following theorem is obtained :

**Theorem 4.3.2.** If Re(s) > 1, then  $\text{st}(\text{st}(\sum_{a \in Y_{\mathbb{Z}}} (Z_s))(a))) = \zeta(s)$ .

**Proof.** st(st( $\sum_{a \in Y_{\mathbf{Z}}} (Z_s)(a)$ )) = st $\left( st\left( \left( \prod_{k \in L} \tilde{p}(H(k + \frac{H}{2}) + 1) \right)^{\left(-s(a(k) + \frac{H'}{2})\right)} \right) \right)$ 

$$= st\left(st\left(\prod_{k\in L}\frac{1-\tilde{p}(H(k+\frac{H}{2})+1)^{-sH'}}{1-\tilde{p}(H(k+\frac{H}{2})+1)^{-s}}\right)\right) = st\left(\prod_{k\in L}\frac{1}{1-\tilde{p}(H(k+\frac{H}{2})+1)^{-s}}\right) = \zeta(s).$$
(128)

Furthermore, Poisson summation formula and Theorem 4.3.2 imply the following : Corollary 4.3.3.

$$st\left(\sum_{b\in Y_{\underline{z}}} (F(Z_s)(b)) = st\left(\prod_{k\in L} \frac{1-\tilde{p}(H(k+\frac{H}{2})+1)^{-sH'}}{1-\tilde{p}(H(k+\frac{H}{2})+1)^{-s}}\right).$$
(129)

Hence we obtain :

$$st(st(\sum_{b\in Y_{\mathbf{Z}}^{\perp}} (F(Z_s)(b)))) = \zeta(s)$$
(130)

...

· · · /

for  $\operatorname{Re}(s) > 1$ .

In general, the physical theory has variables for position, time, and fields. Especially there are many kinds of variables in quantum field theory. The function depends on such variables mixed as  $f(\mathbf{q}, t, \mathbf{a}, \mathbf{b}, \mathbf{c})$  where  $\mathbf{q}$  is position, t is time,  $\mathbf{a}, \mathbf{b}, \mathbf{c}$  are fields. When the function is treated for such mixed variables, the Kinoshita's infinitesimal Fourier transform and our double infinitesimal Fourier transform are applied in the double extended number field. The two kinds of Fourier transforms can be used for one function. In the theory, the delta functions for variable and for fields have different infinitesimals and infinite values. The delta function for fields has an infinitesimal much smaller and much bigger infinite number. However they can be treat in the double extended number field. Two kinds of delta functions are defined with another degrees. One delta function has an infinitesimal of the first degree and the other delta function has an infinitesimal of the second degree. The infinitesimal of the second one can not be observable with respect to the first one.

# 5. Conclusion

The real and complex number fields are extended to the larger number fields where there are many infinitesimal and infinite numbers. A lattice of infinitesimal width is included in the extended real number field. An infinitesimal Fourier transform theory is constructed on the infinitesimal lattice. These extended number fields are furthermore extended to much higher generalized fields where there exist much higher infinitesimal and infinite numbers. A double infinitesimal Fourier transform theory is developed on these double extended number fields. The usual formulae for Fourier theory are satisfied in the theory, especially the Poisson summation formula. The Fourier theory is based on the integral theory for functionals corresponding to the path integral in the physics. The theory is associated to the physical theory in the quantum field theory which is mathematically rigorous . For an application for the double infinitesimal calculation, Riemann's zeta function is represented as such an integral for the propagator of an infinite dimensional harmonic oscillator.

## Acknowledgement

Supported by JSPS Grant-in-Aid for Scientific Research (B) No. 25287010.

## Author details

Takashi Gyoshin Nitta

Department of Mathematics, Faculty of Education, Faculty of Education, Mie University, Japan

## References

- [1] Dirac PAM. The principles of quantum mechanics. Oxford Univ.Press; 1930.
- [2] Feynman RP, Hibbs AR. Quantum mechanics and path integrals. McGrow-Hill Inc. All rights; 1965.
- [3] Gordon EI. Nonstandard methods in commutative harmonic analysis, Translations of mathematical monographs 164 American mathematical society;1997.
- [4] Kinoshita M. Nonstandard representation of distribution I. Osaka J. Math.1988; 25 805-824.
- [5] Kinoshita M. Nonstandard representation of distribution II. Osaka J. Math. 1990; 27 843-861.
- [6] Nitta T. Complexification of the propagator for the harmonic oscillator. Topics in contemporary differential geometry, complex analysis and mathematical physics; 2007. p261-268.
- [7] Nitta T. A complexified path integral for a system of harmonic oscillators. Nonlinear Anal. 2009; 71 2469-2473.

- [8] Nitta T, Okada T. Double infinitesimal Fourier transformation for the space of functionals and reformulation of Feynman path integral, Lecture Note Series in Mathematics, Osaka University 2002 7 255-298 in Japanese.
- [9] Nitta T, Okada T. Infinitesimal Fourier transformation for the space of functionals. Nihonkai Math. J. 2005; 16 1-21.
- [10] Nitta T, Okada T. Poisson summation formula for the space of f functionals, Topics in contemporary differential geometry, complex analysis and mathematical physics. ;2007. p261-268.
- [11] Nitta T, Okada T, Tzouvaras A. Classification of non-well-founded sets and an application. Math. Log. Quart. ;2003 49 187-200.
- [12] Nitta T,Péraire Y. Divergent Fourier analysis using degrees of observability. Nonlinear Anal. 2009; 71 2462-2468.
- [13] Péraire Y. Théorie relative des ensembles internes. Osaka J.Math. 1992; 29 267-297.
- [14] Péraire Y. Some extensions of the principles of idealization transfer and choice in the relative internal set theory, Arch. Math. Logic . 1995; 34 269-277.
- [15] Remmert R. Theory of complex functions. Graduate Texts in Mathematics 122 Springer Berlin-Heidelberg-New York; 1992.
- [16] Saito M. Ultraproduct and non-standard analysis. Tokyo tosho; 1976 in Japanese.
- [17] Satake I. The temptation to algebra. Yuseisha; 1996 in Japanese.
- [18] Takeuti G. Dirac space. Proc. Japan Acad. 1962; 38 414-418.

Section 2

**Physical Sciences** 

**Chapter 6** 

# Experimental Data Deconvolution Based on Fourier Transform Applied in Nanomaterial Structure

Adrian Bot, Nicolae Aldea and Florica Matei

Additional information is available at the end of the chapter

http://dx.doi.org/10.5772/59667

# 1. Introduction

In many kinds of experimental measurements, such as astrophysics, atomic physics, biophysics, geophysics, high energy physics, nuclear physics, plasma physics, solid state physics, bending or torsion elastic, heat propagation or statistical mechanics, the signal measured in the laboratory can be expressed mathematically as a convolution of two functions. The first represents the resolution function called the instrumental signal, which is specific for each setup, and the second is the true sample that contains all physical information. These phenomena can be modelled by an integral equation, which means the unknown function is under the integral operator. The most important type of integral equation applied in physical and technical signal treatments is the Fredholm integral equation of the first kind. The opposite process when used for true sample function determination is known in the literature as experimental data deconvolution. Solution determination of the deconvolution equation does not readily unveil its true mathematical implications concerning the stability of the solutions or other aspects. Thus, from this point of view, the problem is described as improper or illposed. The most rigorous methods for solving the deconvolution equation are: regularization, spline function approximation and Fourier transform technique. The essential feature of regularization method is the replacement of a given improper problem with another, auxiliary, correctly posed problem. The second method consists in approximating both the experimental and instrumental signals by piecewise cubic spline. Most often when using this technique, the true sample function belongs to the same piecewise cubic spline class. The topic of this chapter is the application of Fourier transform in experimental data deconvolution for use in nanomaterial structures.



© 2015 The Author(s). Licensee InTech. This chapter is distributed under the terms of the Creative Commons Attribution License (http://creativecommons.org/licenses/by/3.0), which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

# 2. Mathematical background of signal deconvolution

As mentioned in the introduction, ill-posed problems from a mathematical point of view have many applications in physics and technologies [1]. In addition to the abovementioned examples, the examples below should be noted.

Solving the Cauchy problem for the Laplace equation,  $\Delta U = 0$  has a direct application in biophysics as in [2]. The problem consists in determining the biopotential distribution within the body denoted by *U*, when the body surface potential values are known. The phenomenon

is modelled by the Laplace equation, and the Cauchy conditions are  $U|_{S} = f(S)$  and  $\frac{\partial U}{\partial n}|_{S} = 0$ ,

where *S* represents the surface of the body.

The determination of radioactive substances in the body, as in [2], and protein crystallography structures also deal with ill-posed problems: see [3].

The same formalism is used in quantum mechanics to determine the particle scattering crosssection on different targets, as well as in plasma physics in the case of the electron distribution after speed is received from the dispersion curve analysis [2].

An intuitive way of grasping an ill-posed problem can be modelled by the movement of the vibrating string when many forces are acting perpendicularly on the string, as represented in Figure 1.



Figure 1. Physical model of the vibrating string

In terms of the mathematical equation, the phenomenon described above has a correspondent in physics spectroscopy used in the study of nanomaterials. In the first instance, it is considered that in the point of abscissa  $x_{k}$  force  $\vec{f}_{k}$  acts perpendicularly to the direction of the string. The

string movement in the vertical plane at an arbitrary point *s* is given by the proportionality relationship,

$$h(s) = g(s, x_k) f(x_k) \tag{1}$$

where  $g(s, x_k)$  characterizes the impact of force  $\vec{f}(x_k)$  on the movement h(s). Using the same considerations, for N forces  $\vec{f}_1, \vec{f}_2, \dots, \vec{f}_N$  that act independently in N points of abscissa  $x_1, x_2, \dots, x_N$  in the direction perpendicular to the string, the string movements will be obtained as  $h_1, h_2, \dots, h_N$ . Therefore the movement associated with an arbitrary point of the string of abscissa s is described by the relation below

$$h(s) = g(s, x_1)f(x_1) + g(s, x_2)f(x_2) + \dots + g(s, x_k)f(x_k) = \sum_{i=1}^{N} g(s, x_k)f(x_k)$$
(2)

When a force is distributed continuously along the entire string, the movement of the point *s* of the string will be given by

$$h(s) = \int_{0}^{l} g(s, x) f(x) dx$$
(3)

where *l* represents the length of the string.

The function *f* is the density of force, which means the force per unit length, and f(x)dx represents the force that acts on the arc element dx. The function *g* is called the influence function because it shows the degree of influence of the distribution force *f* on displacement *h*.

The equation (3) is named the Fredholm integral equation of the first kind, and it is a particular case of the integral equation,

$$l(s)f(s) + \int_{a}^{b} g(s,x)f(x)dx = h(s), \quad c \le x \le d$$
(4)

where l, g and h are continuous known functions. If function l is null, then equation (4) represents an integral equation of the first kind. If function l has no zero on [c, d] then the equation (4) is of the second kind, while if l has some zeros on [c,d] then the equation (4) is of the third kind.

Although the aim of this chapter is signal deconvolution using the Fourier transform, it is important to mention the other two methods used to solve equation (4) when l=0, that is, the regularization method and the spline approach.

Hadamard stated that a problem is well posed if it has a unique solution, and the solution depends continuously on the data [4]. Any problem that is not a well-posed problem is an ill-posed one. The Fredholm equation of the first kind is ill posed because small changes in the data generate huge modification of the unknown function.

#### 2.1. Regularization method

This method consists in the replacement of the ill-posed problem (4) with  $l \equiv 0$  by a well-posed problem, and there are many scientific papers that develop different types of regularization method depending on kernel type and other specific needs. Below we describe the Tikhonov regularization method applied to the equation (4) with  $l \equiv 0$ . Let *X* and *Y* be Hilbert spaces and  $\| \cdot \|$  be the norm on Hilbert space. If the kernel *g* is smooth, the operator  $G: X \to Y$ 

$$(Gf)(s) = \int_{a}^{b} g(s,x)f(x)dx$$
(5)

is linear. Then equation (4) with  $l \equiv 0$  becomes

$$Gf = h$$
 (6)

The regularization method consists in the determination of the approximate solution of the equation (4) of the first kind as a minimization of the following functional

$$\Phi_a(f) = \left\| G - h \right\|^2 + \alpha \left\| Lf \right\|^2, \forall f \in X$$
(7)

The value  $\alpha > 0$  represents the regularization parameter and L is a linear operator defined below

$$Lf = a_0(f - \hat{f}) + a_1 f' + a_2 f''$$
(8)

where  $a_i$  has the value 0 or 1; and f' and f'' are the first and the second derivative of f. Function  $\hat{f}$  represents a trial solution for equation (4) with  $l \equiv 0$ . The regularization order for the operator L is the same as the derivability order of f. The regularization parameter should be chosen carefully, because a good minimum for the functional (7) does not always lead to an adequate solution for equation (4) with  $l \equiv 0$  as in [4]. The discrimination procedure of the equation (4) with  $l \equiv 0$  and functional (7) depends on the specifics of each type of problem such as domain, type of kernel, etc., but this is not the subject of this chapter: see [4-6].

Some disadvantages of the regularization method, which is an iterative method, are the fact that it is very sensitive to the noise present in the experimental function and is time consuming.

If the kernel g of the equation (4) with  $l \equiv 0$  has a delayed argument then the equation is called a convolution equation, and is widely applied in physical spectroscopy. The general form of a convolution equation is given by

$$h(s) = \int_{-\infty}^{\infty} g(s-x)f(x)dx$$
(9)

After the change of variable x=t-s it is found that (9) is equivalent by the equation

$$h(s) = \int_{-\infty}^{\infty} g(t) f(t-s) dt$$
(10)

#### 2.2. Spline technique

Spline functions for signal deconvolution technique help eliminate the drawbacks mentioned above [7]. The advantage of the method proposed in [7] lies in the fact that Beniaminy's method is a one-step method. In this case, the true sample function f is represented as a piecewise cubic spline function, and after the substitution of it into equation (10), the experimental function h becomes a piecewise cubic spline function with the same knots but different coefficients. The connection between the coefficients of functions h and f are given by the moments of instrumental function g. Thus, if function f has the form

$$f(t) = \sum_{k=1}^{n-1} s_k(t)$$
(11)

where

$$s_{k}(t) = \begin{cases} 0 & \text{if } t < \xi_{k} \\ a_{k}t^{3} + b_{k}t^{2} + c_{k}t + d_{k} & \text{if } \xi_{k} \le t \le \xi_{k+1} \\ 0 & \text{if } \xi_{k+1} < t \end{cases}$$
(12)

with  $\xi_k$ ,  $k = \overline{1, n-1}$  are the knots and  $a_k, b_k, c_k$  and  $d_k$  are the coefficients of the spline function *f*. They are chosen such that the function together with its first two derivatives is continuous. Replacing (12) in (11), the experimental function has the form

$$h(s) = \sum_{k=1}^{n-1} \left( A_k t^3 + B_k t^2 + C_k t + D_k \right)$$
(13)

where

$$A_{k} = a_{k}M_{0}$$

$$B_{k} = b_{k}M_{0} - 3a_{k}M_{1}$$

$$C_{k} = 3a_{k}M_{2} - 2b_{k}M_{1} + c_{k}M_{0}$$

$$D_{k} = -a_{k}M_{3} + b_{k}M_{2} - c_{k}M_{1} + d_{k}M_{0}$$
(14)

and  $M_k = \int_{-\infty}^{\infty} t^k g(t) dt$  represents the moment of order *k*. Beniaminy considered that experimental function *h* given by (14) is a cubic spline function. In [8] it is shown that that function *h* is not a spline function due to the lack of the continuity in the first two derivatives of *h*. However, the algorithm from [7] gives good results, but the quality of the true sample function depends on how wide the instrumental function is. In order to obtain the true sample function *f* given by (12) and (13), we calculate spline coefficients of the experimental function and using these

#### 2.3. Solving the convolution equation using Fourier transform

values and (14) obtain the coefficients  $a_k$ ,  $b_k$ ,  $c_k$  and  $d_k$ .

Take the functions *h*, *f*, and *g* whose Fourier transform is given by the functions *H*, *F* and *G*. By applying the Fourier transform operator on both members of equation (10) we obtain

$$\int_{-\infty}^{+\infty} h(s) \exp(-2\pi i v s) ds = \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} g(\tau) f(s-\tau) d\tau \exp(-2\pi i v s) ds$$
(15)

By changing the order of integration, the Fourier transform of the signal *h* is expressed by the relation,

$$H(v) = \int_{-\infty}^{+\infty} g(\tau) \left[ \int_{-\infty}^{+\infty} f(s-\tau) \exp(-2\pi i v s) ds \right] d\tau$$
(16)

Using the substitution  $\sigma = s - v$ , the quantity between square brackets from the previous relation becomes

$$\int_{-\infty}^{+\infty} f(\sigma) \exp\left[-2\pi i \nu \left(\sigma + \tau\right)\right] d\sigma = \exp\left(-2\pi i \nu \tau\right) \int_{-\infty}^{+\infty} f(\sigma) \exp(-2\pi i \nu \sigma) d\sigma = \exp(-2\pi i \nu \tau) F(\upsilon)$$
(17)

In this context the relation (16) becomes

$$H(\mathbf{v}) = \int_{-\infty}^{+\infty} g(\tau) \exp(-2\pi i v \tau) F(\mathbf{v}) d\tau = F(\mathbf{v}) G(\mathbf{v})$$
(18)

The relation (18) is known as the convolution theorem. If direct and inverse Fourier transform operators and convolution product are respectively denoted by TF, TF<sup>-1</sup> and \*, then the relation (18) is written symbolically as

$$TF(h) = TF(f)TF(g) = FG = TF(f * g)$$

and

$$TF^{-1}(FG) = h = f * g$$

In this way, the process of the inverse Fourier transform applied to function F determines f signal. In X-ray diffraction theory this is known as the Stokes method.

Experimental signals h, coded by (1), (3), (5) and (6) for a set of supported gold catalyst (Au/SiO<sub>2</sub>), and instrumental contribution g measured on a gold foil, are presented in Figure 2.



Figure 2. The experimental relative intensities *h* of the supported gold catalysts and instrumental function *g* 

## 3. Why is the technique of deconvolution used in nanomaterials science?

In the scientific literature we can see many authors display serious confusion about the concept of deconvolution. Often, when they decompose the experimental signal h according to certain specific criteria, some say that it has achieved the deconvolution of the initial signal. This fact may be accepted only if the instrumental function g from equation (11) is described by the Dirac distribution. Only in this case is the true sample function f identical to the experimental signal h. Unfortunately, no instrumental function of any measuring device can be described by the Dirac distribution.

It is well known that the macroscopic physical properties of various materials depend directly on their density of states (DS). The DS is directly linked to crystallographic properties. For physical systems that belong to the long order class, moving the crystallographic lattice in the whole real space will reproduce the whole structure. The nanostructured materials, which belong to the short-range class, are obtained by moving the lattice in the three crystallographic directions at the limited distances, generating crystallites whose size is no greater than a few hundred angstroms. In this case, the DS is drastically modified in comparison with the previous class of materials. From a physical point of view the DS is closely related to the nanomaterials' dimensionality, so crystallite size gives direct information about new topological properties. It can emphasize that amorphous, disordered or weak crystalline materials can have new bonding and anti-bonding options. The systems consisting of nanoparticles whose dimensions do not exceed 50 Å have the majority of atoms practically situated on the surface for the most part. Additionally, the behaviour of crystallites whose size is between 50 Å and 300 Å is described on the basis of quantum mechanics to explain the advanced properties of the tunnelling effect. All these reasons lead to the search for an adequate method to determine reliable information such as effective particle size, microstrains of lattice, and particle distribution function. This information is obtained by Fourier deconvolution of the instrumental and experimental X-ray line profiles (XRLP) approximated by Gauss, Cauchy and Voigt distributions and generalized by Fermi function (GFF) as in [9]. The powder reflection broadening of the nanomaterials is normally caused by small size, crystallites and distortions within crystallites due to dislocation configurations. It is the most valuable and cheapest technique for the structural determination of crystalline nanomaterials.

Generally speaking, in X-ray diffraction on powder, the most accurate and reliable analysis of the signals is given by the convolution equation (10) where h, g and f are experimental data, instrumental contribution of setup experimental spectrum, and true sample function as a solution of equation (10), respectively.



Figure 3. Numerical solution of the deconvolution equation (19) determined by an algebraic discretization

Let us consider the experimental signals of (111) X-ray line profile of supported nickel catalyst, and the instrumental function given by nickel foil obtained by a synchrotron radiation setup at 201 points with a constant step of  $0.04^{\circ}$  in 20 variables, as shown in Figure 3.

The convolution equation (9) can be approximated in different ways, but the simplest approximation is given by following the algebraic system

$$h(x_i) = \sum_{j=-201}^{201} g(x_i - s_j) f(s_j) \Delta s_j \dots i = 1,201$$
(19)

where  $\Delta s_j$  is a constant step in 20 variables. It turns out that the roots  $f(s_j)$  of system (19) do not lead to a smooth signal, but yield a curve which makes for enhanced oscillations. Its behaviour is given by f signal in Figure 3. This result is given by a computer code written in Maple 11 language, a sequence of which is presented in Appendix 1. From a physical point of view, this type of solution is impracticable because the crystallite size in nanostructured systems is contained in the tails of XRLP. Therefore, the lobes of the XRLP must be sufficiently smooth. As shown in the inset of Figure 3, this condition is not met.. It would be possible to improve the quality of signal f trying to extend the definition interval for signal g. Thus we will approximate the unbounded integral on a bounded interval, but one that is sufficiently large.

This depends on the performances of the computer system and on the algorithm developed for solving inhomogeneous systems of linear equations with sizes of at least several thousand.

# 4. Distributions frequently used in physics and chemical signal deconvolution applied in nanomaterials science

It is known that, from a mathematical point of view, the XRLP are described by the symmetric or asymmetric distributions. As in [10,11] a large variety of functions for analysis of XRLP, such as Voigt (V), pseudo-Voigt (pV) and Pearson VII (P7), are proposed.

#### 4.1. Gauss distribution

Many results such as the propagation of uncertainties and the least square method can be derived analytically in explicit form when the relevant variables are normally distributed. Gauss distribution is defined by mathematical relation

$$I_G = \frac{I_{0G}}{\sqrt{\pi}\gamma_G} \exp\left[-\left(\frac{x-a}{\gamma_G}\right)^2\right]$$
(20)

where  $I_{0G}$ , *a* and  $\gamma_{G}$  are the profile area, gravitational centre measured in  $2\theta$  variable, and broadening of the XRLP, respectively. The *n*<sup>th</sup> moment, *n*=0,1 is given by relations

$$\mu_{0G} = \int_{-\infty}^{+\infty} I_G(x) dx = I_{0G}, \qquad \mu_{1G} = a$$

The integral width  $\delta_G$  and full width at half maximum FWHM<sub>G</sub> are given by relations

$$\delta_G = \sqrt{\pi} \gamma_G$$
 and  $FWHM_G = 2\sqrt{\ln 2} \gamma_G$ 

If both signals h and g are described by Gaussian distributions and take into account the relationship (18), the full width and FWHM of the true sample function are expressed by the relations

$$\gamma_{G,f} = \sqrt{\gamma_{G,h}^2 - \gamma_{G,g}^2} \quad FWHM_{G,f} = 2\sqrt{\ln 2}\gamma_{G,f} \tag{21}$$

#### 4.2. Cauchy distribution

The Cauchy distribution, also called the Lorentzian distribution, is a continuous distribution that describes population distribution of electron levels with multiple applications in physical spectroscopy. Its analytical expression is given by relation

$$I_{C} = \frac{I_{0C}}{\pi} \frac{\gamma_{C}}{\gamma_{C}^{2} + (x - a)^{2}}$$
(22)

where  $I_{0C}$ , *a* and  $\gamma_C$  are profile surface, gravitational centre and broadening of the XRLP, respectively. The *n*<sup>th</sup> moment *n*=0,1 is given by relations

$$\mu_{0C} = \int_{-\infty}^{+\infty} I_C(x) dx = I_{0C}$$
 and  $\mu_{1C} = a$ 

The integral widths  $\delta_G$  and full width at half maximum *FWHM*<sub>C</sub> are given by relations

$$\delta_C = \pi \gamma_C$$
 and  $FWHM_C = 2\gamma_C$ 

The deconvolution of two signals h and g determined by Cauchy distributions is also a Cauchy distribution whose full width  $\delta_{C,f}$  and  $FWHM_{C,f}$  are given by relations

$$\delta_{C,f} = \delta_{C,h} - \delta_{C,g} \quad \text{and} \quad FWHM_{C,f} = 2\delta_{C,f} \tag{23}$$

#### 4.3. Generalized Fermi function

Although extensive research over the past few decades has made progress in XRLP global approximations, their complete analytical properties have not been reported in the literature. Unfortunately, most of them have complicated forms, and they are not easy to handle mathematically. Recently, as in [9,11], a simple function with a minimal number of parameters named the generalized Fermi function (GFF), suitable for minimization and with remarkable analytical properties, was presented from a purely phenomenological point of view. It is given by the relationship,

$$h(s) = \frac{A}{e^{-a(s-c)} + e^{b(s-c)}}$$
(24)

where *A*, *a*, *b*, *c* are unknown parameters. The values *A*, *c* describe the amplitude and the position of the peak, and *a*, *b* control its shape. If *b*=0, the *h* function reproduces the Fermi-Dirac electronic energy distribution. The GFF has remarkable mathematical properties, with direct use in determining the moments, the integral width, and the Fourier transform of the XRLP, as well as the true sample function. Here we give its properties without proofs.

i. By setting

$$s' = s - c$$
  $\rho = (a + b) / 2$   $q = (a - b) / 2$ 

we obtain

$$h(s') = \frac{A}{2} \left( \frac{\cosh q s' + \sinh q s'}{\cosh \rho s'} \right)$$
(25)

**ii.** the limit of *h* function for infinite arguments is finite, so  $\lim h(s')=0$  when  $s' \to \pm \infty$ ;

**iii.** the zero, first and second order moments  $(\mu_0, \mu_1, \mu_2)$  of the *h* function are given by the relations

$$\mu_0 = \frac{\pi A}{2\rho \cos \frac{\pi q}{2\rho}}, \quad \mu_1 = \frac{\pi}{2\rho} \tan \frac{\pi q}{2\rho}, \quad \mu_2 = \left(\frac{\pi}{2\rho}\right)^2 \left(\frac{1}{\cos^2 \frac{\pi q}{2\rho}} + \tan^2 \frac{\pi q}{2\rho}\right)$$

iv. the integral width  $\delta_h(a, b)$  of the *h* function has the following form

$$\delta_h(a,b) = \frac{\pi}{\left(a^a b^b\right)^{1/(a+b)} \cos\left(\frac{\pi}{2} \frac{a-b}{a+b}\right)}$$
(26)

#### **v.** the Fourier transform of the *h* function is given by the relationship

$$H(L) = \frac{A}{2} \int_{-\infty}^{+\infty} \frac{\cosh q s' + \sinh q s'}{\cosh \rho s'} e^{-2\pi s' L} ds' = \frac{\pi A}{2\rho \left| \cos \left(\frac{\pi q}{2\rho} + i \frac{\pi^2 L}{\rho} \right) \right|^2} \cos \left(\frac{\pi q}{2\rho} - i \frac{\pi^2 L}{\rho} \right)$$
(27)

vi. if we consider the functions f and g defined by equation (25), by their deconvolution we can compute the |F(L)| function, which is used in Warren and Averbach's analysis in [12]. Therefore, the magnitude of F(L) function has the following form:

$$\left|F(L)\right| = \frac{A_h \rho_g}{A_g \rho_h} \sqrt{\frac{\cos^2 \alpha + \sinh^2 \beta L}{\cos^2 \gamma + \sinh^2 \delta L}},$$
(28)

where the arguments of trigonometric and hyperbolic functions are expressed by

$$\alpha = \frac{\pi q_g}{2\rho_g}, \quad \beta = \frac{\pi^2}{\rho_g}, \quad \gamma = \frac{\pi q_h}{2\rho_h}, \quad \delta = \frac{\pi^2}{\rho_h}$$

The subscripts g and h refer to the instrumental and experimental XRLP. Taking into account the convolution theorem, the true sample function f is given by the relationship

$$f(s) = \frac{A_h \rho_g}{A_g \rho_h} \int_{-\infty}^{+\infty} \frac{\cos\left(\frac{\pi q_g}{2\rho_g} + i\frac{\pi^2 L}{\rho_g}\right)}{\cos\left(\frac{\pi q_h}{2\rho_h} + i\frac{\pi^2 L}{\rho_h}\right)} \exp(2\pi i Ls) ds$$

The last integral cannot be accurately resolved. In order to do so we have to consider some arguments. The Fourier transform of *f* is the *F* function, given by the relations

$$F(L) = |F(L)| \exp(i\theta(L)), \quad \theta(L) = \arctan\frac{\Im(F(L))}{\Re(F(L))}$$

where  $\theta$  means the angle function, and  $\Re(F)$  and  $\Im(F)$  are the real and imaginary parts of the complex function *F*, respectively. The arguments  $\alpha$ ,  $\beta$ ,  $\gamma$  and  $\delta$  from equation (28) depend only on the asymmetry parameters *a* and *b* of the *g* and *f* functions. If the XRLP asymmetry is not very large (i.e., *a* and *b* parameters are close enough as values) the  $\cos^2 \alpha \approx 1$ ,  $\cos^2 \gamma \approx 1$  approximations are reliable. Therefore, we obtain  $\Im(F) << \Re(F)$ ,  $\theta(L) \approx 0$  and the magnitude of the Fourier transform for the true XRLP sample can be expressed as

Experimental Data Deconvolution Based on Fourier Transform Applied in Nanomaterial Structure 153 http://dx.doi.org/10.5772/59667

$$\left|F(L)\right| = \frac{A_h \rho_g}{A_g \rho_h} \frac{\cosh \frac{\pi^2 L}{\rho_g}}{\cosh \frac{\pi^2 L}{\rho_h}}$$
(29)

(vii) if we consider the previous approximation, the true XRLP sample is given by an inverse Fourier transform of the *F* function, and consequently we have

$$f(s') = \frac{2A_h\rho_g}{\pi A_g} \frac{\cos\frac{\pi\rho_h}{2\rho_g}\cosh\rho_h s'}{\cosh 2\rho_h s' + \cos\frac{\pi\rho_h}{\rho_g}}$$
(30)

(viii) the integral width of the true XRLP sample can be expressed by the  $\delta_f$  function

$$\delta_f(\rho_h, \rho_g) = \frac{\pi}{2\rho_h \cos\frac{\pi\rho_h}{2\rho_g}} \left( \cos\frac{\pi\rho_h}{\rho_g} + 1 \right)$$
(31)

#### 4.4. Voigt distribution applied in X-ray line profile analysis

Before briefly describing the mathematical properties of the Voigt distribution, let us examine the physical concept underlying the approximation of the XRLP by Voigt distribution and the convolution process.

During decades of research, Warren and Averbach [12] introduced the X-ray diffraction concept for the mosaic structure model, in which the atoms are arranged in blocks, each block itself being an ideal crystal, but with adjacent blocks that do not accurately fit together. They considered that the XRLP h represents the convolution between the true sample f and the instrumental function g, produced by a well-annealed sample. The effective crystallite size  $D_{eff}$  and lattice disorder parameter  $\langle \varepsilon_{hkl} \rangle$  were analysed as a set of independent events in a likelihood concept. Based on Fourier convolution produced between f and g signals and the mosaic structural model, the analytical form of the Fourier transform for the true sample function was obtained. The normalized *F* was described as the product of two factors,  $F^{(s)}(L)$  and  $F^{(\varepsilon)}(L)$ , where variable *L* represents the distance perpendicular to the (hkl) reflection planes. The factor  $F^{(s)}(L)$  describes the contribution of crystallite size and stocking fault probability, while the factor  $F^{(\varepsilon)}(L)$  gives information about the microstrain of the lattice. The general form of the Fourier transform of the lattice. The general form of the Fourier transform for the lattice.

$$F^{(s)}(L) = e^{-\frac{|L|}{D_{eff}(hkl)}}, \qquad F^{(\varepsilon)}(L) = e^{-\frac{2\pi^2 \langle \varepsilon_L^2 \rangle_{hkl} h_0^2 L^2}{a^2}},$$
(32)

where  $h_0^2 = h^2 + k^2 + l^2$ . The general form of the true sample function *f* is given by inverse Fourier transform of *F*(*L*)

$$f(s) = \int_{-\infty}^{\infty} e^{-\beta L^2 - \gamma |L|} e^{2\pi i s L} dL =$$

$$= \sqrt{\frac{\pi}{\beta}} \exp\left[\frac{\gamma^2 - (2\pi s)^2}{4\beta}\right] \left\{ \Re\left(erfc\left(\frac{\gamma - 2\pi i s}{2\sqrt{\beta}}\right)\right) \cos\frac{\pi \gamma s}{\beta} - \Im\left(erfc\left(\frac{\gamma + 2\pi i s}{2\sqrt{\beta}}\right)\right) \sin\frac{\pi \gamma s}{\beta} \right\}$$
(33)

where  $s=2\left(\frac{\sin\theta}{\lambda}-\frac{\sin\theta_0}{\lambda}\right)$ ,  $erf(x)=\frac{2}{\sqrt{\pi}}\int_{0}^{x}e^{-t^2}dt$ , erfc(x)=1-erf(x) is the complementary error

function [13] and  $\beta = \frac{2\pi^2 \langle \varepsilon_L^2 \rangle_{hkl} h_0^2}{a^2}$ ,  $\gamma = \frac{1}{D_{eff}(hkl)}$ . The last relation from the mathematical point of view represents a Voigt distribution. If we take into account the properties of the Gauss and Cauchy distributions, the Voigt distribution can be generalized by relation

$$V(x,\gamma_{G},\gamma_{C}) = \int_{-\infty}^{+\infty} I_{G}(x',\gamma_{G},x_{0G}) I_{C}(x-x',\gamma_{C},x_{0C}) dx'$$
(34)

Based on relation (18), its Fourier transform is given by  $FT[V] = FT[I_G] \cdot FT[I_C]$  where

$$F_G(L) = e^{-2\pi i x_{0G} L_e - \pi^2 \gamma_G^2 L^2}$$
 and  $F_C(L) = e^{-2\pi i x_{0C} L - 2\pi \gamma_C |L|}$ 

The analytical expression of the Voigt distribution is

$$V(x,\gamma_G,\gamma_C) = FT^{-1} \left[ e^{-2\pi i (x_{0C} + x_{0G})L} e^{-\pi^2 \gamma_G^2 L^2 - 2\pi \gamma_C |L|} \right]$$
(35)

Explicit forms of experimental signal and true sample function normalized at  $I_{0V}$  are given by relations [13]

$$V(x,\gamma_{G},\gamma_{C}) = \frac{I_{0V}}{\sqrt{\pi}\gamma_{G}} \exp\left[\frac{\gamma_{C}^{2} - (x - x_{0C} - x_{0G})^{2}}{\gamma_{G}^{2}}\right].$$

$$\cdot \left\{ \Re\left[ erfc\left(\frac{\gamma_{C} - i(x - x_{0C} - x_{0G})}{\gamma_{G}}\right)\right] \cos\frac{2\gamma_{C}(x - x_{0C} - x_{0G})}{\gamma_{G}^{2}} - \Im\left[ erfc\left(\frac{\gamma_{C} + i(x - x_{0C} - x_{0G})}{\gamma_{G}}\right)\right] \sin\frac{2\gamma_{C}(x - x_{0C} - x_{0G})}{\gamma_{G}^{2}} \right\}$$
(36)

Experimental Data Deconvolution Based on Fourier Transform Applied in Nanomaterial Structure 155 http://dx.doi.org/10.5772/59667

and

$$V_{f}(x,\gamma_{G,f},\gamma_{C,f}) = \frac{1}{\sqrt{\pi}\gamma_{C,f}} \exp\left[\frac{\gamma_{C,f}^{2} - (x - x_{0C} - x_{0G})^{2}}{\gamma_{G,f}^{2}}\right] \cdot \left\{ \Re\left[ erfc\left(\frac{\gamma_{C,f} - i(x - x_{0C} - x_{0G})}{\gamma_{G,f}}\right)\right] \cos\frac{2\gamma_{C,f}(x - x_{0C} - x_{0G})}{\gamma_{G,f}^{2}} - \Im\left[ erfc\left(\frac{\gamma_{C,f} + i(x - x_{0C} - x_{0G})}{\gamma_{G,f}}\right)\right] \sin\frac{2\gamma_{C}(x - x_{0C} - x_{0G})}{\gamma_{G,f}^{2}} \right\}$$
(37)

Maximum value of true sample function is

$$V_{\max} = \frac{1}{\sqrt{\pi}\gamma_G} \exp\left(\frac{\gamma_C^2}{\gamma_G^2}\right) erfc\left(\frac{\gamma_C}{\gamma_G}\right)$$

Voigt function is a probability density function and it displays the distribution of target values,

$$\int_{-\infty}^{\infty} V(x, \gamma_G, \gamma_C) dx = \frac{1}{\pi \sqrt{\pi}} \frac{\gamma_C}{\gamma_G} \int_{-\infty}^{\infty} \left[ \int_{-\infty}^{\infty} \frac{e^{-\left(\frac{x}{\gamma_G}\right)^2}}{\gamma_C^2 + \left(x - x'\right)^2} dx' \right] dx = 1,$$

$$\delta_V = \frac{\sqrt{\pi} \gamma_G}{\exp\left(\frac{\gamma_C}{\gamma_G}\right)^2 \operatorname{erfc}\left(\frac{\gamma_C}{\gamma_G}\right)}$$
(38)

and the convolution of two Voigt functions is also a Voigt function.

The integral width of a true sample function has the two components given by the Gauss and Cauchy contributions

$$\delta_{G,f}^{2} = \frac{1}{\pi} \Big( \delta_{G,h}^{2} - \delta_{G,g}^{2} \Big), \quad \delta_{C,f} = \frac{1}{\pi} \Big( \delta_{C,h} - \delta_{C,g} \Big)$$
(39)

Balzar and Popa are among the leading scientists in the field of Fourier analysis of X-ray diffraction profiles, and they suggested that each Gauss and Cauchy component contains information about the average crystallite size ( $\delta_S$ ) and distortion of the lattice ( $\delta_D$ ) as in [14]. From the algebraic point of view, they proposed the following relationship

$$\delta_{G,f}^{2} = \delta_{SG,f}^{2} + \delta_{DG,f}^{2}, \quad \delta_{C,f} = \delta_{SC,f} + \delta_{DC,f}$$
(40)

Based on the new concept introduced by them, the two components of the Fourier transform are given by the relations

$$F^{S}(L) = e^{-\pi L^{2} \delta_{SG,f}^{2} - 2|L|\delta_{SC,f}}, \quad F^{D}(L) = e^{-\pi L^{2} \delta_{DG,f}^{2} - 2|L|\delta_{DC,f}}$$
(41)

The particle size distribution function, P(L) is determined from the second derivative of straincorrected Fourier transform of the true sample function. The volume-weighted column-length  $P_V$  and surface-weighted column-length  $P_S$  distributions are given by the following [14]:

$$P_{V}(L) = L \frac{d^{2} F^{S}(L)}{dL^{2}} = 2L \bigg[ 2 \big( \pi L \delta_{SG}^{2} + \delta_{SC} \big)^{2} - \pi \delta_{SG}^{2} \bigg] F^{S}(L)$$
(42)

$$P_{S}(L) = P_{V}(L) = \frac{d^{2}F^{S}(L)}{dL^{2}} = 2\left[2\left(\pi L\delta_{SG}^{2} + \delta_{SC}\right)^{2} - \pi\delta_{SG}^{2}\right]F^{S}(L)$$
(43)

#### 5. Experimental section, data analysis and results

A series of four supported gold catalysts were studied by X-ray diffraction (XRD) in order to determine the average particle size of the gold, the microstrain of the lattice as well as the size and microstrain distribution functions by XRLP deconvolution using Fourier transform technique. The gold catalyst samples with up to 5 wt% gold content were prepared by impregnation of the SiO<sub>2</sub> support with aqueous solution of HAuCl<sub>4</sub>×3H<sub>2</sub>O and homogeneous deposition-precipitation using urea as the precipitating agent method, respectively. The X-ray diffraction data of the supported gold catalysts displayed in Figure 3 were collected using a Rigaku horizontal powder diffractometer with rotated anode in Bragg-Brentano geometry with Ni-filtered Cu K $\alpha$  radiation,  $\lambda$  = 1.54178 Å, at room temperature. The typical experimental conditions were: 60 sec for each step, initial angle  $2\theta = 32^{\circ}$ , and a step of  $0.02^{\circ}$ , and each profile was measured at 2700 points. The XRD method is based on the deconvolution of the experimental XRLP (111) and (222) using Fourier transform procedure by fitting the XRLP with the Gauss, Cauchy, GFF and Voigt distributions. The Fourier analysis of XRLP validity depends strongly on the magnitude and nature of the errors propagated in the data analysis. The scientific literature treated three systematic errors: uncorrected constant background, truncation, and effect of sampling for the observed profile at a finite number of points that appear in discrete Fourier analysis. In order to minimize propagation of these systematic errors, a global approximation of the XRLP is adopted instead of the discrete calculus. The reason for this choice was the simplicity and mathematical elegance of the analytical Fourier transform magnitude and the integral width of the true XRLP given by equations (20)-(24), (31), (34) and (38), as in [15]. The robustness of these approximations for the XRLP arises from the possibility of using the analytical forms of the Fourier transform instead of a numerical fast Fourier transform (FFT). It is well known that the validity of the numerical FFT depends drastically on the filtering technique what was adopted in [16]. In this way, the validity of the nanostructural parameters is closely related to the accuracy of the Fourier transform magnitude of the true XRLP.

Experimental relative intensities (111) with respect to  $2\theta$  values for (1) system are shown in Figure 4. The next steps consist in background correction of XRLP by polynomial procedures, finding the best parameters for the distributions adopted using the method of least squares or nonlinear fit, and then deconvoluting them using instrumental function. The main steps in the data analysis of the investigated systems are shown in Figure 4.



Figure 4. Various stages of processing for X-ray line profile (111) of the sample (1)

Experimental relative intensities (222) with respect to  $2\theta$  values for (6) system are shown in Figure 5.

The Fourier transforms normalized for the true sample function of the investigated samples (1) and (6) were calculated by three distinct methods, based on relations (28), (32) and (41), and are displayed in Figure 6.

The microstrain and particle size distribution functions determined by Fourier deconvolution of a single XRLP were calculated using equation (32), and are plotted in Figure 7.

The credibility of the parameters describing the investigated nanostructure systems depends primarily on the process of approximation of XRLP. This criterion is expressed by the root mean squares of residuals (*rmsr*) of data analysis and is given by relation



rmsr = 100

 $(y_i^{calc} - y_i)$  $\sigma_i^2$ 

points

N naram

Figure 5. Various stages of processing for X-ray line profile (222) of the sample (6)



Figure 6. Fourier transform of true sample function of XRLP (111) and (222) for systems (1) and (6): blue - general relation, red - GFF, green - Voigt distribution

The *rmsr* values for all distributions used in XRLP approximation process are given in Table 1. The *rmsr* values are closely related to the spectral noise of experimental data. Here it is shown that a model based on GFF and Voigt distribution may be more realistic and accurate.

The integral widths and FWHM of the true sample functions calculated for all distributions were determined using the relations (21), (23), (31) and (38). Their values are presented in Table 2. Experimental Data Deconvolution Based on Fourier Transform Applied in Nanomaterial Structure 159 http://dx.doi.org/10.5772/59667



Figure 7. Size and microstrain distribution functions of (111) XRLP for system (1)

Comple	<b>b</b> [c]	Distribution						
Sample	<u> 11K1</u> –	GFF	Gauss	Cauchy	Voigt			
(1)	111	26.2658	47.6477	40.6091	26.9398			
(1)	222	14.8795	15.2648	16.0429	15.1880			
(2)	111	21.5743	31.4428	28.0142	22.1633			
(3)	222	12.5725	12.4615	12.6212	12.4534			
(E)	111	18.1273	26.6941	21.8148	17.4276			
(3)	222	13.2033	13.3122	13.2599	13.2771			
(6)	111	28.1267	31.8679	36.0040	35.5948			
(0)	222	18.8487	20.5945	33.2718	19.9656			

Table 1. Values for rmsr for investigated samples

Because the experimental XRLP was measured for both (111) and (222), the surface-weighted column-length  $P_s$  and volume-weighted column-length  $P_V$  distribution functions were determined using relations (42,43) implemented in BREADTH software [17]. Additionally, it has found that the Gumbel distribution is the most adequate function for the global approximation of both probabilities' curves, and the results are shown in Figure 8.

The global structural parameters obtained for the investigated samples are summarized in Table 3 and Table 4.

	hkl	200 [Deg]	Distributions							
Sample			GFF		Gauss		Cauchy		Voigt	
			ð [Deg]	a* [Deg]	ð [Deg]	a* [Deg]	ð [Deg]	a* [Deg]	ð [Deg]	a* [Deg]
(1)	111	38.291	0.644	0.540	0.638	0.599	0.738	0.469	0.713	0.537
	222	81.780	0.862	0.715	0.854	0.803	1.025	0.653	0.927	0.765
(3)	111	38.220	0.802	0.672	0.798	0.750	0.919	0.585	0.891	0.668
	222	81.763	1.028	0.860	1.011	0.950	1.181	0.752	1.095	0.912
(5)	111	38.211	0.631	0.529	0.621	0.583	0.723	0.460	0.701	0.519
	222	81.801	1.052	0.873	1.067	1.003	1.225	0.780	1.185	0.890
(6)	111	38.292	0.363	0.304	0.363	0.341	0.426	0.271	0.374	0.335
	222	81.872	0.506	0.423	0.498	0.468	0.613	0.390	0.528	0.461
a* represents FWHM										

Table 2. Values for integral width and full width at half maximum for investigated samples



**Figure 8.** Surface-weighted column-length distribution function,  $P_{s_s}$  and volume-weighted column-length distribution function,  $P_{V_s}$  for (5) and (6) systems

Sample		GFF approximation				Single Voigt approximation			
	$D_{111}^{Sch}$	D <sub>111</sub>	$D_{222}^{Sch}$	D <sub>222</sub>	$D_{111}^{Sch}$	D <sub>111</sub>	$D_{222}^{Sch}$	D <sub>222</sub>	
(1)	180	168	180	139	145	154	118	145	
(3)	143	135	139	130	116	118	98	139	
(5)	183	171	145	112	153	151	108	95	
(6)	398	309	313	263	249	384	199	303	

Table 3. Values for crystallite size determined by Scherrer method, and effective crystallite size using single XRLP approximations

Sample	hkl	$\langle D \rangle_S \pm \Delta D_S$ [Å]	$\langle D \rangle_V \pm \Delta D_V$ <sup>[Å]</sup>	$\langle \varepsilon^2(D_V/2) \rangle^{1/2} \pm \varDelta \langle \varepsilon^2(D_V/2) \rangle^{1/2}$
(1)	[111/222]	90±12	133±15.	$0.211E-02 \pm 0.152E-03$
(3)	[111/222]	69±13	104± 17	$0.262E-02 \pm 0.288E-03$
(5)	[111/222]	106±30	153±41	$0.280E-02 \pm 0.216E-03$
(6)	[111/222]	214±72	233±79	$0.105E-02 \pm 0.522E-03$

Table 4. Values for the average crystallite size and microstrain using double Voigt approaches

Hydrogen chemisorption, transmission electron microscopy (TEM), magnetization, electronic paramagnetic resonance (EPR) and other methods could also be used to determine the average diameter of particles by taking into account a prior spherical form for the grains. By XRD method we can obtain the crystallite sizes that have different values for different crystallographic planes. There is a large difference between the particle size and the crystallite size due to the different physical meaning of the two concepts. It is possible that the particles of the supported gold catalysts are made up of many gold crystallites.

The size of the crystallites determined by equations (32) and (41), corresponding to (111) and (222) planes, have different values. The crystallite sizes  $D_{111}^{Sch}$  and  $D_{222}^{Sch}$  are determined by the Scherrer method [18] without taking into account the microstrain of the lattice. The values  $D_{111}$  and  $D_{222}$  were determined by Fourier deconvolution method for single XRLP, while the averages of  $D_V$  and  $D_S$  were calculated by a double Voigt approach. The difference between the crystallites' size can be explained by the fact that the analytical models are different due to the different approaches. This means that the geometry of the crystallites is not spherical [18]. The microstrain parameter of the lattice can also be correlated with the effective crystallite size in the following way: the value of the effective crystallite size increases when the microstrain value decreases.

The main procedures of the SIZE.mws software dedicated to Fourier analysis of the XRLP by GFF and Voigt distributions written in Maple 11 language are presented in Appendix 2.

## 6. Conclusions

In the present chapter, it is shown that XRD analysis provides more information for understanding the physical properties of nanomaterial structure. Powder X-ray diffraction is the cheapest and most reliable method compared with hydrogen chemisorptions, TEM techniques, magnetic measurements, EPR, etc. The main conclusions that can be drawn from these studies are:

- 1. For XRLP analysis, a global approximation should be applied rather than a numerical Fourier analysis. The former analysis is better than a numerical calculation because it can minimize the systematic errors that could appear in the traditional Fourier analysis.
- **2.** Our numerical results show that by using the GFF and the Voigt distribution we successfully obtained reliable global nanostructural parameters;

- **3.** Cauchy and Gauss distributions used for XRLP approximation give roughly structural information;
- 4. Powder X-ray diffraction gives the most detailed nanostructural results, such as: average crystallite size, microstrain, and distribution functions of crystallite size and microstrain;
- **5.** Surface-weighted domain size depends only on Cauchy integral breadth, while volume-weighted domain size depends on Cauchy and Gauss integral breadths;
- **6.** To obtain valid structural results, it is important to have: a good S/N ratio of the experimental spectra, a good deconvolution technique for the experimental and instrumental spectra, and an adequate computer package and programs for data analysis.

# Appendix 1

Input data h.txt and g.txt files

```
`k`:=1;
line h:= readline(`h.txt`):
line_g:= readline(`g.txt`):
while line <> 0 do
temp_h:= sscanf(line_h,`%8f%8f`):temp_g:=sscanf(line_g,`%8f %8f`):
printf(`%10.5f %10.5f`,temp_h[1],temp_h[2]): lprint():
printf(`%10.5f %10.5f`,temp_g[1],temp_g[2]): lprint():
twotheta_h[`k`]:=temp_h[1];
intensity_h[`k`]:=temp_h[2];
twotheta_g[`k`]:=temp_g[1];
intensity_g[`k`]:=temp_g[2];
line h:= readline(`h.txt`):
line_g:= readline(`g.txt`):
`k`:=`k`+1;
end do;
`k`:=`k`-1;
p_h:=plot([twotheta_h[`ih`],intensity_h[`ih`],`ih`=1..k],col-
or=red,style=LINE,thickness=2,axes=boxed,gridlines,
labels=["2theta",""]):
p_g:=plot([twotheta_g[`ig`], intensity_g[`ig`], `ig`=1..k], col-
or=blue,style=LINE,thickness=2,axes=boxed,gridlines,
labels=["2theta",""]):
display({p_h,p_g});
deltatwotheta:=twotheta h[2]-twotheta h[1]:
```

h vector determination

```
twok:=2*k;
for `i` from 1 to k
do
h[`i`]:=intensity_h[`i`]:
end do:
```

```
h[`k`+1]:=0:
`j`:=1:
for `i` from `k`+2 to twok+1
do
h[`i`]:=intensity_h[`j`]:
`j`:=`j`+1:
end do:
print(h);
```

g array determination

```
`j`:=1:
for `i` from -twok to -k
do
g[`i`]:=intensity_g[`j`]:
`j`:=`j`+1;
end do:
`j`:=1:
for `i` from -k to -1
do
g[`i`]:=intensity_g[`j`]:
`j`:=`j`+1:
end do:
g[0]:=0.:
for `i` from 1 to \boldsymbol{k}
do
g[`i`]:=intensity_g[`i`]:
end do:
`j`:=1:
for `i` from k+1 to twok
do
g[`i`]:=intensity_g[`j`]:
`j`:=`j`+1:
end do:
print(g):
```

a matrix determination

```
for `i` from 1 to twok+1
do
for `j` from 1 to twok+1
do
a[`i`,`j`]:=0.:
end do:
end do:
`i1`:=0:
for `i` from -k to k
do
`j1`:=0:
`i1`:=`i1`+1:
for `j` from -k to k
do
```

```
`j1`:=`j1`+1:
a[`i1`,`j1`]:=g[`i`-`j`]*deltatwotheta;
end do:
end do:
print(a);
```

solving integral deconvolution equation by direct discretization

```
f:=linsolve(a,h):
for `i` from 1 to twok+1
do
twotheta_f[`i`]:=twotheta_h[1]+(`i`-1)*deltatwotheta:
intensity_f[`i`]:=eval(f[`i`]);
end do:
p_h:=plot([twotheta_h[`ihh`],intensity_h[`ihh`],`ihh`=1..k],col-
or=red,style=LINE,thickness=2,axes=boxed,gridlines,labels=["2theta",""]):
p_g:=plot([twotheta_g[`igg`],intensity_g[`igg`],`igg`=1..k],
color=blue,style=LINE,thickness=2,axes=boxed,gridlines,
labels=["2theta",""]):
p_f:=plot([twotheta_f[`iff`], intensity_f[`iff`], `iff`=1..twok+1],
color=green,style=LINE,thickness=2,axes=boxed,gridlines,
labels=["2theta",""]):
display({p_h,p_g,p_f});
fd:= fopen("f",WRITE,TEXT):
for `i` from 1 to k
do
fprintf(fd,"%g %g\n",twotheta f[`i`],intensity f[`i`]):
end do:
fclose(fd):
```

# Appendix 2

Fourier transform of true sample function procedure

```
f_GFF_freq:=proc(freq)
local arg_in,arg_sa;
arg_in:=(Pi*q_in)/(2*rho_in) + I *(Pi*Pi*freq)/rho_in;
arg_sa:=(Pi*q_sa)/(2*rho_sa) + I * (Pi*Pi*freq)/rho_sa;
(ampl_sa/ampl_in)*(rho_in/rho_sa)*cos(arg_in)/cos(arg_sa);
end:
```

Module of Fourier transform of true sample function procedure

```
FT_GFF_modul:=proc(freq)
local aux,bux,auxr_0,auxi_0;
aux:=evalc(Re(f_GFF_freq(freq))):
bux:=evalc(Im(f_GFF_freq(freq))):
aux:=aux*aux+bux*bux:
auxr_0:=evalc(Re(f_GFF_freq(0))):
auxi_0:=evalc(Im(f_GFF_freq(0))):
```

```
bux:=auxr_0*auxr_0+auxi_0*auxi_0:
sqrt(aux/bux):
end:
```

True sample function procedure

```
f_GFF_s:=proc(s)
local arg1,arg2;
arg1:=(Pi/2)*(rho_sa/rho_in);
arg2:=(rho_sa*s);
(2/Pi)*(ampl_sa/ampl_in)*
rho_in*cos(arg1)*cosh(arg2)/(cosh(2*arg2)+cos(2*arg1));
end:
```

Integral width of true sample function procedure

```
int_width_GFF:=proc(rho_in,rho_sa)
local arg;
arg:=Pi*rho_sa/rho_in;
Pi/(2*rho_sa*cos(arg/2))*(cos(arg)+1);
end:
```

Moment of zero order for experimental X-ray line profile procedure

```
mu_0_GFF:=proc(ampl,rho,q)
local arg;
arg:=(Pi*q)/(2*rho);
(ampl/2)*(Pi/rho)*(1/cos(arg));
end:
```

Moment of first order for experimental X-ray line profile procedure

```
mu_1_GFF:=proc(rho,q)
local arg;
arg:=(Pi*q)/(2*rho);
(Pi/(2*rho))*tan(arg);
end:
```

Moment of second order for experimental X-ray line profile procedure

```
mu_2_GFF:=proc(rho,q)
local arg;
arg:=(Pi*q)/(2*rho);
((Pi/(2*rho))^2)*(1./(cos(arg)^2)+tan(arg)^2);
end:
```

Experimental X-ray line profile procedure approximated by GFF distribution

```
exp_profile_GFF:=proc(s)
local arg_q,arg_rho;
arg_q:=q*s; arg_rho:=rho*s;
(ampl/2)*(cosh(arg_q)+sinh(arg_q))/cosh(arg_rho);
end:
```

Instrumental X-ray line profile procedure determined by GFF distribution

```
inst_profile_GFF:=proc(s)
local arg_q,arg_rho;
arg_q:=q_in*s; arg_rho:=rho_in*s;
(ampl_in/2)*(cosh(arg_q)+sinh(arg_q))/cosh(arg_rho);
end:
```

Fourier transform procedure for general relation of true sample function developed by Warren-Averbach theory

```
gen_function:=proc(freq)
exp(-beta_gen(fmin,fmax)*freq*freq-
gama_gen(fmin,fmax)*abs(freq));
end:
```

Procedure for experimental XRLP given by Voigt approximation

```
h_Voigt_function:=proc(s)
local arg1,arg2,arg3,arg4;
arg1:=(gama_h_c**2-s**2)/(gama_h_g**2);
arg2:=(gama_h_c-I*s)/gama_h_g;
arg3:=(gama_h_c+I*s)/gama_h_g;
arg4:=2.*gama_h_c*s/(gama_h_g**2);
amp_h/(sqrt(Pi)*gama_h_g)*exp(arg1)*
(Re(erfc(arg2))*cos(arg4)-Im(erfc(arg3))*sin(arg4));
end:
```

Procedure for instrumental XRLP given by Voigt approximation

```
g_Voigt_function:=proc(s)
local arg1,arg2,arg3,arg4;
arg1:=(gama_g_c**2-s**2)/(gama_g_g**2);
arg2:=(gama_g_c-I*s)/gama_g_g;
arg3:=(gama_g_c+I*s)/gama_g_g;
arg4:=2.*gama_g_c*s/(gama_g_g**2);
amp_g/(sqrt(Pi)*gama_g_g)*exp(arg1)*
(Re(erfc(arg2))*cos(arg4)-Im(erfc(arg3))*sin(arg4));
end:
```

Procedure for the true sample function calculated by Voigt approximation

```
f_Voigt_function:=proc(s)
local arg1,arg2,arg3,arg4;
arg1:=(gama_f_c**2-s**2)/(gama_f_g**2);
arg2:=(gama_f_c-I*s)/gama_f_g;
arg3:=(gama_f_c+I*s)/gama_f_g;
arg4:=2.*gama_f_c*s/(gama_f_g**2);
amp_h/amp_g/(sqrt(Pi)*gama_f_g)*exp(arg1)*(Re(erfc(arg2))*cos(arg4)-
Im(erfc(arg3))*sin(arg4));
end:
```

# Acknowledgements

Financial support received from the European Union through the European Regional Development Fund, Project ID 1822/SMIS CSNR 48797 CETATEA, is gratefully acknowledged. In particular, one of the topics covered by the book *Fourier Transform of the Signals* will be a useful starting point in accomplishing one of its major objectives, energy recovery from ambient pollution. Additionally, the authors are grateful to the staff of Beijing Synchrotron Radiation Facilities for beam time and for their technical assistance in XRD measurements.

# Author details

Adrian Bot<sup>1</sup>, Nicolae Aldea<sup>1\*</sup> and Florica Matei<sup>2</sup>

\*Address all correspondence to: naldea@itim-cj.ro

1 National Institute for Research and Development of Isotopic and Molecular Technologies, Cluj-Napoca, Romania

2 University of Agricultural Sciences and Veterinary Medicine, Cluj-Napoca, Romania

# References

- [1] Kabanikin S. Inverse and Ill-Posed Problems: Theory and Applications. Berlin/ Boston: Walter de Gruyter GmbH; 2011.
- [2] Nedelcov I. P. Improper Problems in Computational Physics. Computer Physics Communications 1972; 4(2)157-163.
- [3] Read R. J. Intensity Statistics in the Presence of Translational Noncrystallographic Symmetry. Acta Crystallographica Section D 2013; 69(2) 176-183.
- [4] Kleefeld A., Cottbus B. T. U. Numerical Results for Linear Fredholm Integral Equations of the First Kind over Surfaces in 3D. International Journal of Computer Mathematics 2010; 1(1) 1-16.
- [5] Naumova V., Pereverzyev S. V. Multi-penalty Regularization with a Componentwise Penalization. Inverse Problems 2013; 29(7) 1-16.
- [6] Kabanikin S., editor. Regularization Theory for Ill-posed Problems: Selected Topics. Inverse and Ill Posed Problems Series 58. Berlin/Boston: Walter de Gruyter GmbH; 2013.

- [7] Beniaminy I., Deutsch M. A Spline Based Method for Experimental Data Deconvolution. Computer Physics Communications 1980; 21(2): 271-277.
- [8] Fredrikze H., Verkerk P. Comment on "A spline based method for experimental data deconvolution". Computer Physics Communications 1981; 24(1), 5-7.
- [9] Aldea N., Tiusan C., Zapotinschi R. A New Approach Used to Evaluation the Crystallite Size of Supported Metal Catalysts by Single X-Ray Profile Fourier Transform Implemented on Maple V. In: Borcherds P., Bubak M., Maksymowicz A., editors. 8<sup>th</sup> Joint EPS-APS International Conference on Physics Computing, PC '96 17-21 September 1996, Krakow: Academic Computer Centre CYFRONET-KRAKOW; 1996.
- [10] Balzar D., Ledbetter H. J. Voigt-Function Modeling in Fourier-Analysis of Size and Xray Diffraction Peaks-Peaks. Journal of Applied Crystallography 1993; 26(1) 97-103.
- [11] Aldea N., Gluhoi A., Marginean P., Cosma C., Yaning X. Extended X-Ray Absorption Fine Structure and X-Ray Diffraction Studies on Supported Nickel Catalysts. Spectrochimica Acta Part 2000; 55(7) 997-1008.
- [12] Aldea N., Barz B., Pintea S., Matei F. Theoretical Approach Regarding Nanometrology of the Metal Nanoclusters Used in Heterogeneous Catalysis by Powder X-Ray Diffraction Method. Journal of Optoelectronics and Advanced Materials 2007; 9(10) 3293-3296.
- [13] Gradstein I. S., Rijik L. M. Tables of Integrals, Sums, Series, and Products. Moscow: Fizmatgiz; 1962.
- [14] Balzar D., Popa N. C. Crystallite Size and Residual Strain/Stress Modeling in Rietveld Refine. In: Meittemeijer E. J., Scardi P., editors. Diffraction Analysis of the Microstructure of Materials. Berlin Heidelberg New York: Springer-Verlag; 2003, pp. 125-144.
- [15] Lazar M., Valer A., Pintea S., Barz B., Ducu C., Malinovschi V., Xie Yaning Aldea N. Preparation and Structural Characterization by XRD and XAS of the Supported Gold Catalysts. Journal of Optoelectronics and Advanced Materials 2008; 10(9) 2244-2251.
- [16] Walker J. S. Fast Fourier Transform. 2nd ed. New York, London, Tokyo: Boca Raton CRC; 1997.
- [17] Balzar D. BREADTH- a Program for Analyzing Diffraction Line Broadening. Journal of Applied Crystallography 1995; 28(2) 244-245.
- [18] Rednic V., Aldea N., Marginean P., Rada M., Bot A., Zhonghua W., Zhang J., Matei F. Heat Treatment Influence on the Structural Properties of Supported Ni Nanoclusters. Metals and Materials International 2014; 20(4) 641-646.
# **Gabor-Fourier Analysis**

Nafya Hameed Mohammad and Massoud Amini

Additional information is available at the end of the chapter

http://dx.doi.org/10.5772/60034

# 1. Introduction

The notion of Gabor transform, named after Dennis Gabor [1], is a special case of the short-time Fourier transform. The Gabor analysis, as it stands now, is a rather new field, but the idea goes back quite some while. Dennis Gabor investigated in [1] the representation of a one dimensional signal in two dimensions, time and frequency. He suggested to represent a function by a linear combination of translated and modulated Gaussians. Interestingly, there is a tight connection between this approach and quantum mechanics (c.f. [2]). On the mathematical side, the representation of functions by other functions was further investigated, leading to the theory of atomic decompositions, developed by Feichtinger and Gröchenig [3].

Gabor transform and Gabor expansion have long been recognized as very useful tools for the signal processing, and it is because of this reason over the recent years, an increasing attention has been given to the study of them in engineering and applied Mathematics, see for instance [4, 5]. Borichev et al. [6] studied the stability problem for the Gabor expansions generated by a Gaussian function. In [7], Ascensi and Bruna proved that the unique Gabor atom with analytical Gabor space, the image of  $L^2(\mathbb{R})$  under the Gabor transform, is the Gaussian function. The structure of Gabor and super Gabor spaces inside  $L^2(\mathbb{R}^{2d})$  is studied by Abreu [8]. Christensen [9] has done a comprehensive study of the Gabor system and has asked for the necessary and sufficient conditions to get a frame for  $L^2(\mathbb{R})$ .

Today Gabor analysis and the closely related wavelet analysis are considered topics in harmonic analysis. The basic idea behind wavelet analysis is that the notion of an orthonormal basis is not always useful. Sometimes it is more important for a decomposing set to have special properties, like good time frequency localization, than to have unique coefficients. This led to the concept of frames, which was introduced by Duffin and Schaefer in [10] and was made popular by Daubechies, and today is one of the most important foundations of Gabor theory and a fundamental subject in harmonic analysis.



© 2015 The Author(s). Licensee InTech. This chapter is distributed under the terms of the Creative Commons Attribution License (http://creativecommons.org/licenses/by/3.0), which permits unrestricted use, distribution, and eproduction in any medium, provided the original work is properly cited. Most examples of Gabor frames correspond to regular nets of points. That is, sets of the type  $\{e^{2\pi i bnt}h(t-am)\}_{n,m\in\mathbb{Z}^d}$ . One can usually find sufficient and necessary conditions for the existence of such kind of frames, with a variety of applications. For technical reasons, however, one needs to work with frames coming from irregular grids. One of the main purposes of this chapter is to study perturbations of irregular Gabor frames and the problem of stability.

On the other hand, the theory of nonharmonic Fourier series is concerned with the completeness and expansion properties of sets of complex exponentials  $\{e^{i\lambda_n t}\}$  in  $L^p[-\pi, \pi]$ . In 1952, Duffin and Schaeffer [10] used frames to study this theory, and later Young put together many results in his book [11]. Reid [12] proved that if  $\{\lambda_n\}$  is a sequence of real numbers whose differences are nondecreasing, then the set of complex exponentials  $\{e^{i\lambda_n t}\}$  is a Riesz-Fischer sequence in  $L^2[-A, A]$  for every A > 0. Jaffard [13] investigated how the regularity of nonharmonic Fourier series is related to the spacing of their frequencies, and this is obtained by using a transformation which simultaneously captures the advantages of the Gabor and wavelet transforms.

In this chapter, we restate and prove some classical results of (nonharmonic) Fourier expansions for Gabor systems instead of sets of complex exponentials. Some of the results may be known or obtainable via Hilbert space methods, but the main advantage of this work is that it uses analytic methods and can be fully understood with elementary knowledge of functional and complex analysis in several variables [14, 15].

## 2. Preliminaries

Let us introduce the notions and basic results, needed later in the chapter.

**Definition 2.1** We say that  $\Lambda = \{z_j\}_{j \in \mathbb{N}} \subset \mathbb{C}^d$  is a *separated set* if there exists  $\varepsilon > 0$  such that  $|z_i - z_j| \ge \varepsilon$ ,  $i \ne j$ . The largest of such  $\varepsilon$  is called the *separation constant* of  $\Lambda$ . A finite union of separated sets is called a *relatively separated set*.

**Definition 2.2** A sequence of vectors  $\{x_n\}$  in a normed space  $\mathcal{X}$  is said to be *complete* if its linear span is dense in  $\mathcal{X}$ , that is, if for each vector x and each  $\varepsilon > 0$  there is a finite linear combination  $c_1x_1 + \cdots + c_nx_n$  such that

$$\|x - (c_1 x_1 + \dots + c_n x_n)\| < \varepsilon.$$

**Definition 2.3** A sequence  $\{f_n\}$  in a Hilbert space *H* is said to be a *Bessel sequence* if

$$\sum_{n=1}^{\infty} |\langle f, f_n \rangle|^2 < \infty$$

for every element  $f \in H$ . It is called a *Riesz-Fischer sequence* if the moment problem

$$\langle f, f_n \rangle = c_n, \quad n \ge 1$$

admits at least one solution  $f \in H$  whenever  $\{c_n\} \in l^2$ .

**Proposition 2.4** Let  $\{f_n\}$  be a sequence in a Hilbert space *H*. Then

(i)  $\{f_n\}$  is a Bessel sequence with bound *M* if and only if the inequality

$$\left\|\sum c_n f_n\right\|^2 \leq M \sum |c_n|^2$$

holds for every finite sequence of scalars  $\{c_n\}$ ;

(ii)  $\{f_n\}$  is a Riesz-Fischer sequence with bound *m* if and only if the inequality

$$m\sum |c_n|^2 \leq \left\|\sum c_n f_n\right\|^2$$

holds for every finite sequence of scalars  $\{c_n\}$ .

**Remark 2.5** For a sequence  $\{f_n\}$  in a Hilbert space *H*, the moment problem

$$\langle f, f_n \rangle = c_n, \quad n \ge 1$$

has at most one solution for every choice of the scalars  $\{c_n\}$  if and only if  $\{f_n\}$  is complete.

**Definition 2.6** A countable family  $\{f_k\}_{k \in I}$  in a separable Hilbert space *H* is a *frame* for *H* if there exist constants *A* and *B* such that  $0 < A \leq B < \infty$  and

$$A\|f\|^2 \leq \sum_{k \in I} |\langle f, f_k \rangle|^2 \leq B\|f\|^2, \quad f \in H.$$

*A*, *B* are called the *lower* and *upper frame bounds* respectively. They are not unique: the biggest lower bound and the smallest upper bound are called the *optimal frame bounds*. Every element in *H* has at least one representation as an infinite linear combination of the frame elements.

**Definition 2.7** Let  $c \in \mathbb{R}^d$ , the unitary operators  $T_c$  and  $M_c$  on  $L^2(\mathbb{R}^d)$  defined by  $T_c f(t) = f(t-c)$  and  $M_c f(t) = e^{2\pi i c t} f(t)$  are called the *Translation* and *Modulation* operator, respectively. For a discrete set  $\Lambda = \{z_j\}_{j \in \mathbb{Z}}$  in  $\mathbb{C}^d$  and a fixed nonzero window function  $h \in L^2(\mathbb{R}^d)$ , we define the *Gabor system*  $G(h, \Lambda)$  as:

$$G(h,\Lambda) = \{M_y T_x h(t) = e^{2\pi i y t} h(t-x); x + i y \in \Lambda\}.$$

For simplicity we denote  $e^{2\pi i y t} h(t - x)$  by  $h_z(t)$ , where z = x + i y. Gabor systems were first introduced by Gabor [1] in 1946 for signal processing, and is still widely used. A Gabor

system is said to be *exact* in  $L^2(\mathbb{R}^d)$  if it is complete, but fails to be complete on the removal of any one term.

If  $G(h, \Lambda)$  is a frame for  $L^2(\mathbb{R}^d)$ , it is called a *Gabor frame* or *Weyl-Heisenberg frame*.

**Definition 2.8** Let *f* be an entire function. For r > 0, the *maximum modulus function* is  $M(r) = \max\{|f(z)| : |z| = r\}$ . Unless *f* is a constant of modulus less than or equal to 1, its *order*, which is denoted by  $\rho$ , is defined by

 $\rho = \limsup_{r \to \infty} \frac{\log \log M(r)}{\log r}.$ 

Simple examples of functions of finite order include  $e^z$ ,  $\sin z$ , and  $\cos z$ , all of which are of order 1, and  $\cos \sqrt{z}$ , which is of order  $\frac{1}{2}$ . Every polynomial is of order 0; the order of a constant function is of course 0 and the function  $e^{e^z}$  is of infinite order.

**Remark 2.9** An entire function has an order of growth  $\leq \rho$  if  $|f(z)| \leq A e^{B|z|^{\rho}}$ .

The following is the fundamental factorization theorem for entire functions of finite order. It is due to Hadamard who used the result in his celebrated proof of the Prime Number Theorem. It is one of the classical theorems in function theory.

**Theorem 2.10 (Hadamard Factorization Theorem)** Let f be an entire function of finite order  $\rho$ ,  $\{z_n\}$  be the zeros of f different from 0, k be the order of zero of f at the origin, and

$$f(z) = z^k e^{g(z)} \prod_{n=1}^{\infty} (1 - \frac{z}{z_n})$$

be its canonical Factorization, then g(z) is a polynomial of degree no longer than  $\rho$ .

**Definition 2.11** The (*Bargmann-*)*Fock space*,  $\mathcal{F}(\mathbb{C}^d)$ , is the Hilbert space of all entire functions f on  $\mathbb{C}^d$  for which

$$\|f\|_{\mathcal{F}}^2 = \int_{\mathbb{C}^d} |f(z)|^2 e^{-\pi |z|^2} dz,$$

is finite. The natural inner product on  $\mathcal{F}(\mathbb{C}^d)$  is defined by

$$\langle f,g \rangle_{\mathcal{F}} = \int_{\mathbb{C}^d} f(z) \overline{g(z)} e^{-\pi |z|^2} dz; \quad f,g \in \mathcal{F}(\mathbb{C}^d).$$

The *Bargmann transform* of a function  $f \in L^2(\mathbb{R}^d)$  is the function Bf on  $\mathbb{C}^d$  defined by

$$Bf(z) = 2^{\frac{d}{4}} e^{-\frac{\pi}{2}z^2} \int_{\mathbb{R}^d} f(t) e^{-\pi t^2} e^{2\pi t z} dt.$$

**Definition 2.12** Fix a function  $h \in L^2(\mathbb{R}^d)$  (called the window function). The *Gabor transform* with respect to the window *h* is the isomorphic inclusion

$$V_h: L^2(\mathbb{R}^d) \longrightarrow L^2(\mathbb{C}^d),$$

defined by

$$V_h f(z) = \langle f(t), h_z(t) \rangle = 2^{d/4} \int_{\mathbb{R}^d} f(t) \overline{h(t-x)} e^{-2\pi i t y} dt$$

for every  $f \in L^2(\mathbb{R}^d)$  and  $z = x + iy \in \mathbb{C}^d$ . The following subspace of  $L^2(\mathbb{C}^d)$  which is the image of  $L^2(\mathbb{R}^d)$  under the Gabor transform with the window h,

$$\mathcal{G}_h = \{ V_h f : f \in L^2(\mathbb{R}^d) \},\$$

is called *Gabor space* or *model space*. A simple calculation shows that the Bargmann transform is related to the Gabor transform with the Gaussian window  $g(t) = 2^{d/4}e^{-\pi t^2}$  in  $L^2(\mathbb{R}^d)$  by the formula

$$V_g f(x - iy) = e^{i\pi xy} e^{-\pi \frac{|x + iy|^2}{2}} (Bf)(x + iy).$$
(1)

For more details we refer the reader to [2, 7, 8, 17].

#### 3. Gabor Expansion

Here we discuss the fundamental completeness properties of the Gabor systems. The most extensive results in the case of the sets of complex exponentials  $\{e^{i\lambda_n t}\}$  over a finite interval of the real axis were obtained by Paley and Wiener [16]. At the same time, we will be laying the groundwork for a more penetrating investigation of nonharmonic Gabor expansions in  $L^2(\mathbb{R}^2)$ .

Let  $\{(\lambda_n, \mu_n)\}_{n \in \mathbb{Z}}$  be an arbitrary countable subset of  $\mathbb{R}^2$  and

$$\{\varphi_n(\xi)\}_{n\in\mathbb{Z}} = \left\{M_{\mu_n}T_{\lambda_n}g(\xi)\right\}_{n\in\mathbb{Z}} = \left\{\sqrt{2}\,e^{2\pi i\mu_n\xi - \pi(\xi - \lambda_n)^2}\right\}_{n\in\mathbb{Z}};\tag{2}$$

where  $\xi \in \mathbb{R}^2$  or  $\mathbb{C}$ , be the corresponding Gabor system with respect to the Gaussian window g in  $L^2(\mathbb{R}^2)$ . If  $\{\varphi_n\}_{n \in \mathbb{Z}}$  is incomplete in  $L^2(\mathbb{R}^2)$  then the closed linear span  $\mathcal{M}$  of  $\{\varphi_n\}_{n \in \mathbb{Z}}$  is a proper subspace of  $L^2(\mathbb{R}^2)$ . By Hahn-Banach Theorem there exists a function F in  $L^2(\mathbb{R}^2)$ 

such that  $F|_{\mathcal{M}} = 0$  and  $F \neq 0$ . Riesz Representation Theorem implies that  $F = F_{\varphi}$  for some  $\varphi$  in  $L^2(\mathbb{R}^2)$  and

$$F(h) = F_{\varphi}(h) = \int_{\mathbb{R}^2} h \, \varphi \, d\xi; h \in L^2(\mathbb{R}^2).$$

For  $(z, w) \in \mathbb{C}^2$  take

$$f(z,w) = \sqrt{2} \int_{\mathbb{R}^2} e^{2\pi i w \xi - \pi (\xi - z)^2} \,\varphi(\xi) \,d\xi,$$
(3)

then  $f(\lambda_n, \mu_n) = F(\varphi_n) = 0$  (since  $F|_{\mathcal{M}} = 0$ ).

**Remark 3.1** The system (2) is incomplete in  $L^2(\mathbb{R}^2)$  if and only if there exists a nontrivial entire function of the form (3) in the Gabor space  $\mathcal{G}_g$ , which is zero for every  $(\lambda_n, \mu_n)$ . Furthermore, since

$$f(z,w) = V_g \varphi(z,-w) = e^{i\pi z w} e^{-\pi \frac{|z|^2 + |w|^2}{2}} (B\varphi)(z,w),$$

we have

$$|f(z,w)| \leq ||\varphi||_2 e^{\frac{\pi}{2}|(z,w)|^2}$$

**Theorem 3.2** Let  $\{\lambda_n\}_{n\in\mathbb{Z}}$  be a symmetric sequence of real numbers  $(\lambda_{-n} = -\lambda_n)$ . If the Gabor system

$$\left\{\sqrt[4]{2}e^{2\pi i\lambda_n t - \pi (t - \lambda_n)^2}\right\}_{n \in \mathbb{Z}}$$
(4)

is exact in  $L^2(\mathbb{R})$ , then the product

$$\prod_{n=1}^{\infty} \left(1 - \frac{z^2}{\lambda_n^2}\right) e^{\frac{z^2}{\lambda_n^2}}$$

converges to an entire function which belongs to the Gabor space with Gaussian window in  $L^2(\mathbb{R})$ .

**Proof.** By Remark 3.1, if the system (4) is exact, then there exists an entire function f(z) in the Gabor space  $\mathcal{G}_g$  such that  $f(\lambda_n) = 0$  for  $n \neq 0$ , and

$$f(z) = \sqrt[4]{2} \int_{\mathbb{R}} e^{2\pi i z t - \pi (t-z)^2} \varphi(t) \, dt; \quad \varphi \in L^2(\mathbb{R}).$$

Since  $f(\lambda_n) = 0$  for  $n \neq 0$  and the sequence  $\{\lambda_n\}$  is symmetric,  $\varphi(-t)$  has the same orthogonality properties as  $\varphi(t)$ . But by Remark 2.5,  $\varphi(t)$  is unique, so  $\varphi(t)$  must be even.

Hence f(z) is even. Now f(z) vanishes only at the  $\lambda_n$  with  $n \neq 0$ . Indeed, if f(z) vanishes at  $z = \gamma$ , then the function

$$\tilde{f}(z) = \frac{zf(z)}{z - \gamma}$$

would also belong to  $\mathcal{G}_g$  and would vanish at every  $\lambda_n$ . The system (4) would then be incomplete in  $L^2(\mathbb{R})$ , contrary to hypothesis.

Let us observe that the function  $\tilde{f}$  belongs to  $\mathcal{G}_g$ . Since the Bargmann transform is related to the Gabor transform by the formula (1), it is sufficient to show that the function  $e^{i\pi xy}e^{\frac{\pi}{2}(|x|^2+|y|^2)}\tilde{f}(z)$ ; z = x + iy, belongs to the Fock space  $\mathcal{F}(\mathbb{C})$ . In other words, we must show that the integral

$$\int_{\mathbb{C}} \frac{|z|^2}{|z-\gamma|^2} |f(z)e^{i\pi xy} e^{\frac{\pi}{2}(|x|^2+|y|^2)} |^2 e^{-\pi(|x|^2+|y|^2)} dx \, dy; \quad z=x+iy,$$

is finite. Since  $\lim_{z\to\infty} |\frac{z}{z-\gamma}| = 1$ , we have  $|\frac{z}{z-\gamma}| \leq 3/2$  outside a square *T* with complement *T<sup>c</sup>*. Thus the above integral is no larger than

$$\begin{split} &\int_{T} \frac{|z|^{2}}{|z-\gamma|^{2}} |f(z)e^{i\pi xy} e^{\frac{\pi}{2}(|x|^{2}+|y|^{2})} |^{2} e^{-\pi(|x|^{2}+|y|^{2})} dx \, dy \\ &+ 9/4 \int_{T^{c}} |f(z)e^{i\pi xy} e^{\frac{\pi}{2}(|x|^{2}+|y|^{2})} |^{2} e^{-\pi(|x|^{2}+|y|^{2})} dx \, dy \\ &\leq \int_{T} \frac{|z|^{2}}{|z-\gamma|^{2}} |f(z)e^{i\pi xy} e^{\frac{\pi}{2}(|x|^{2}+|y|^{2})} |^{2} e^{-\pi(|x|^{2}+|y|^{2})} dx \, dy \\ &+ 9/4 \int_{\mathbb{C}} |f(z)e^{i\pi xy} e^{\frac{\pi}{2}(|x|^{2}+|y|^{2})} |^{2} e^{-\pi(|x|^{2}+|y|^{2})} dx \, dy. \end{split}$$

In the last expression, since *T* is compact the first integral is finite, and since the function  $f(z)e^{i\pi xy}e^{\frac{\pi}{2}(|x|^2+|y|^2)}$  is in the Fock space  $\mathcal{F}(\mathbb{C})$ , so is the second integral. Next since

$$|f(z)| \leq ||\varphi||_2 e^{\frac{\pi}{2}|z|^2},$$

the order of growth of f is at most 2, and by Hadamard's factorization theorem,

$$f(z) = e^{Az} \prod_{n=1}^{\infty} \left( 1 - \frac{z^2}{\lambda_n^2} \right) e^{\frac{z^2}{\lambda_n^2}}; \quad A \in \mathbb{R}.$$

Since f(z) and the canonical product are both even, A = 0 and

$$f(z) = \prod_{n=1}^{\infty} \left( 1 - \frac{z^2}{\lambda_n^2} \right) e^{\frac{z^2}{\lambda_n^2}}.$$

We have the following version of Plancherel-Pólya theorem. We give the proof which is similar to [11, Th. 2.16] for the sake of completeness.

**Theorem 3.3 (Plancherel-Pólya).** If f(z) is an entire function of order of growth  $\leq \tau$  and if for some positive number p,

$$\int_{-\infty}^{\infty} |f(x)|^p \, dx < \infty,$$

then

$$\int_{-\infty}^{\infty} |f(x+iy)|^p \, dx \leq e^{p\tau|y|} \int_{-\infty}^{\infty} |f(x)|^p \, dx.$$

The proof will require two preliminary lemmas. Suppose that q(z) is a non constant continuous function in the closed upper half-plane,  $\text{Im} z \ge 0$ , and analytic in its interior. Let *a* and *p* be positive real numbers and put

$$\mathcal{Q}(z) = \int_{-a}^{a} |q(z+t)|^p \, dt$$

It is clear that Q(z) is continuous for  $\text{Im} z \ge 0$ . Since  $|q(z)|^p$  is subharmonic for Im z > 0 (see [12, p.83]), so is Q(z).

**Lemma 3.4** Let q(z) be a function of order of growth  $\leq \tau$  in the half-plane Im $z \geq 0$  and suppose that the following quantities are both finite:

$$M = \sup_{-\infty < x < \infty} \mathcal{Q}(x) and N = \sup_{y > 0} \mathcal{Q}(iy).$$

Then on this half-plane,

$$\mathcal{Q}(z) \leq max(M, N).$$

**Proof.** Since q(z) is of order of growth  $\leq \tau$ , then there exist positive numbers *A* and *B* such that

$$|q(z)| \leq Ae^{B|z|^{\tau}} (Imz \geq 0).$$
<sup>(5)</sup>

For each positive number  $\varepsilon$ , define the auxiliary function

$$q_{\varepsilon}(z) = q(z)e^{-\varepsilon(\lambda(z+a))^{3/2}},$$
(6)

where  $\lambda = e^{-i\pi/4}$ . The exponent of *e* in (6) has two possible determinations in the half-plane Imz > 0; we choose the one whose real part is negative in the quarter-plane x > -a,  $y \ge 0$ . Put

$$\mathcal{Q}_{\varepsilon}(z) = \int_{-a}^{a} |q_{\varepsilon}(z+t)|^{p} dt,$$

which is then defined and continuous in the upper half-plane  $\text{Im} z \ge 0$ , and subharmonic in its interior. A simple calculation involving (5) and (6) shows that in the quarter plane x > -a,  $y \ge 0$ ,

$$|q_{\varepsilon}(z)| \leq A e^{B|z|^{\tau} - \varepsilon \gamma |z+a|^{3/2}},\tag{7}$$

where  $\gamma = \cos 3\pi/8$ , and  $|q_{\varepsilon}(z)| \leq |q(z)|$ . Hence

$$\mathcal{Q}_{\varepsilon}(z) \leq \mathcal{Q}(z) (x \geq 0, y \geq 0),$$

and in particular

$$\mathcal{Q}_{\varepsilon}(x) \leq M$$
 for  $x \geq 0$  and  $\mathcal{Q}_{\varepsilon}(iy) \leq N$  for  $y \geq 0$ .

Let  $z_0$  be a fixed but arbitrary point in the first quadrant. We shall apply the maximum principle to  $Q_{\varepsilon}(z)$  in the region  $\Omega = \{z : Rez \ge 0, Imz \ge 0, |z| \le R\}$ , choosing *R* large enough so that (i)  $z_0 \in \Omega$ , and (ii) the maximum value of  $Q_{\varepsilon}(z)$  on  $\Omega$  is not attained on the circular arc|z| = R (this is possible by virtue of (7)). Since  $Q_{\varepsilon}(z)$  does not reduce to a constant, the maximum value of  $Q_{\varepsilon}(z)$  on  $\Omega$  must be attained on one of the coordinate axes, and in particular,

$$\mathcal{Q}_{\varepsilon}(z_0) \leq max(M, N).$$

Now let  $\varepsilon \to 0$ . This establishes the result for the first quadrant; the proof for the second quadrant is similar.

Lemma 3.5 In addition to the hypotheses of Lemma 3.4, suppose that

$$\lim_{y \to \infty} q(x+iy) = 0 \tag{8}$$

uniformly in *x*, for  $-a \leq x \leq a$ . Then

$$Q(z) \leq M$$
,  $Imz \geq 0$ .

**Proof.** It is sufficient to show that  $N \leq M$ . By virtue of (8), we see that the function Q(iy) tends to zero as  $y \to \infty$ , and so must attain its least upper bound *N* for some finite value of *y*, say  $y = y_0$ . If  $y_0 = 0$ , then

$$N = \mathcal{Q}(iy_0) = \mathcal{Q}(0) \leq M.$$

If  $y_0 > 0$ , then the maximum principle shows that the least upper bound of Q(z) in the half-plane Im $z \ge 0$  cannot be attained at the interior point  $z = iy_0$ . Therefore, by Lemma 3.4,

$$N = \mathcal{Q}(iy_0) < max(M, N),$$

and again N < M.

Theorem 3.3 now follows.

**Proof of Theorem 3.3.** It is sufficient to prove the theorem when y > 0 and f(z) is not identically zero. Let  $\varepsilon$  be a fixed positive number and consider the function

$$q(z) = f(z)e^{i(\tau+\varepsilon)z}.$$

It is easy to see that, for each positive number *a*, the functions q(z) and Q(z) satisfy the conditions Lemmas 3.4 and 3.5. Consequently, for y > 0,

$$\mathcal{Q}(iy) \leq M < \int_{-\infty}^{\infty} |q(x)|^p dx.$$

This together with the definitions of q(z) and Q(z) implies

$$e^{-p(\tau+\varepsilon)y}\int_{-a}^{a}|f(x+iy)|^{p}dx<\int_{-\infty}^{\infty}|f(x)|^{p}dx.$$

To get the result, first let  $a \to \infty$ , then let  $\varepsilon \to 0$ .

**Proposition 3.6** Let f(z, w) be an entire function of order of growth  $\leq \tau$  and suppose that  $\{\lambda_n\}, \{\mu_n\}$  are increasing sequences of real numbers such that

$$\lambda_{n+1} - \lambda_n \ge \varepsilon_1 > 0$$
 and  $\mu_{n+1} - \mu_n \ge \varepsilon_2 > 0$ .

If for some positive number *p*,

$$\sup_{n} \int_{-\infty}^{\infty} |f(x_{z}, \mu_{n})|^{p} dx_{z} < \infty \quad \text{and} \quad \sup_{n} \int_{-\infty}^{\infty} |f(\lambda_{n}, x_{w})|^{p} dx_{w} < \infty,$$
(9)

then

$$\sum_n |f(\lambda_n,\mu_n)|^p < \infty.$$

Proof. First, using the Plancherel-Pólya Theorem, observe that conditions (9) imply that

$$\sup_n \int_{-\infty}^{\infty} |f(z,\mu_n)|^p \, dx_z \leq e^{p\tau |y_z|} \int_{-\infty}^{\infty} \sup_n |f(x_z,\mu_n)|^p \, dx_z,$$

and

$$\sup_{n}\int_{-\infty}^{\infty}|f(\lambda_{n},w)|^{p}\,dx_{w}\leq e^{p\tau|y_{w}|}\int_{-\infty}^{\infty}\sup_{n}|f(\lambda_{n},x_{w})|^{p}\,dx_{w}.$$

Now since  $|f|^p$  is plurisubharmonic, the inequality

$$|f(z_0, w_0)|^p \leq \frac{1}{2\pi} \int_0^{2\pi} |f((z_0, w_0) + (\zeta, \eta)e^{i\theta})|^p \, d\theta \tag{10}$$

holds for all values of ( $\zeta$ ,  $\eta$ ). Fix  $\eta = 0$ , multiply both sides of (10) by  $\zeta$  and integrate between 0 and  $\delta_1$ ,

$$\int_0^{\delta_1} |f(z_0, w_0)|^p \zeta \, d\zeta \leq \frac{1}{2\pi} \int_0^{\delta_1} \int_0^{2\pi} |f(z_0 + \zeta e^{i\theta}, w_0)|^p \, d\theta \, \zeta \, d\zeta.$$

Then

$$|f(z_0, w_0)|^p \leq \frac{1}{\pi \delta_1^2} \iint_{\Omega_1} |f(z, w_0)|^p dx_z dy_z,$$

where  $\Omega_1 = \{(z, w_0) : |z - z_0| \leq \delta_1\}$ . Similarly fix  $\zeta = 0$ , multiply both sides of (10) by  $\eta$  and integrate between 0 and  $\delta_2$ ,

$$|f(z_0,w_0)|^p \leq \frac{1}{\pi \delta_2^2} \iint_{\Omega_2} |f(z_0,w)|^p dx_w dy_w,$$

where  $\Omega_2 = \{(z_0, w) : |w - w_0| \le \delta_2\}$ . Then

$$2|f(z_0, w_0)|^p \leq \frac{1}{\pi \delta_1^2} \iint_{\Omega_1} |f(z, w_0)|^p \, dx_z \, dy_z + \frac{1}{\pi \delta_2^2} \iint_{\Omega_2} |f(z_0, w)|^p \, dx_w \, dy_w.$$

Now let  $\Omega_1^n = \{(\lambda_n + z, \mu_n) : |z| \leq \delta_1\}$  and  $\Omega_2^n = \{(\lambda_n, \mu_n + w) : |w| \leq \delta_2\}$ , then

$$\begin{split} 2\sum_{n} |f(\lambda_{n},\mu_{n})|^{p} &\leq \sum_{n} \Big( \frac{1}{\pi\delta_{1}^{2}} \iint_{\Omega_{1}^{n}} |f(\lambda_{n}+z,\mu_{n})|^{p} \, dx_{z} \, dy_{z} \\ &+ \frac{1}{\pi\delta_{2}^{2}} \iint_{\Omega_{2}^{n}} |f(\lambda_{n},\mu_{n}+w)|^{p} \, dx_{w} \, dy_{w} \Big) \\ &\leq \sum_{n} \Big( \frac{1}{\pi\delta_{1}^{2}} \int_{-\delta_{1}}^{\delta_{1}} \int_{-\delta_{1}}^{\delta_{1}} |f(\lambda_{n}+z,\mu_{n})|^{p} \, dx_{z} \, dy_{z} \\ &+ \frac{1}{\pi\delta_{2}^{2}} \int_{-\delta_{2}}^{\delta_{2}} \int_{-\delta_{2}}^{\delta_{2}} |f(\lambda_{n},\mu_{n}+w)|^{p} \, dx_{w} \, dy_{w} \Big) \\ &= \sum_{n} \Big( \frac{1}{\pi\delta_{1}^{2}} \int_{-\delta_{1}}^{\delta_{1}} \int_{\lambda_{n}-\delta_{1}}^{\lambda_{n}+\delta_{1}} |f(z,\mu_{n})|^{p} \, dx_{z} \, dy_{z} \\ &+ \frac{1}{\pi\delta_{2}^{2}} \int_{-\delta_{2}}^{\delta_{2}} \int_{\mu_{n}-\delta_{2}}^{\mu_{n}+\delta_{2}} |f(\lambda_{n},w)|^{p} \, dx_{w} \, dy_{w} \Big). \end{split}$$

It is clear that the last expression above is no larger than

$$\sum_{n} \left( \frac{1}{\pi \delta_1^2} \int_{-\delta_1}^{\delta_1} \int_{\lambda_n - \delta_1}^{\lambda_n + \delta_1} \sup_{n} |f(z, \mu_n)|^p dx_z dy_z + \frac{1}{\pi \delta_2^2} \int_{-\delta_2}^{\delta_2} \int_{\mu_n - \delta_2}^{\mu_n + \delta_2} \sup_{n} |f(\lambda_n, w)|^p dx_w dy_w \right).$$

Now for  $\delta_1 = \frac{\varepsilon_1}{2}$  and  $\delta_2 = \frac{\varepsilon_2}{2}$ , the intervals  $(\lambda_n - \delta_1, \lambda_n + \delta_1)$  are pairwise disjoint, and similarly for the intervals  $(\mu_n - \delta_2, \mu_n + \delta_2)$ , thus

$$2\sum_{n} |f(\lambda_{n},\mu_{n})|^{p} \leq \frac{1}{\pi\delta_{1}^{2}} \int_{-\delta_{1}}^{\delta_{1}} \int_{-\infty}^{\infty} \sup_{n} |f(z,\mu_{n})|^{p} dx_{z} dy_{z}$$
$$+ \frac{1}{\pi\delta_{2}^{2}} \int_{-\delta_{2}}^{\delta_{2}} \int_{-\infty}^{\infty} \sup_{n} |f(\lambda_{n},w)|^{p} dx_{w} dy_{w}$$

We conclude that

$$\begin{split} 2\sum_{n} |f(\lambda_{n},\mu_{n})|^{p} &\leq \frac{1}{\pi\delta_{1}^{2}} \int_{-\delta_{1}}^{\delta_{1}} \left( e^{p\tau|y_{z}|} \int_{-\infty}^{\infty} \sup_{n} |f(x_{z},\mu_{n})|^{p} dx_{z} \right) dy_{z} \\ &+ \frac{1}{\pi\delta_{2}^{2}} \int_{-\delta_{2}}^{\delta_{2}} \left( e^{p\tau|y_{w}|} \int_{-\infty}^{\infty} \sup_{n} |f(\lambda_{n},x_{w})|^{p} dx_{w} \right) dy_{w} \\ &= B_{1} \sup_{n} \int_{-\infty}^{\infty} |f(x_{z},\mu_{n})|^{p} dx_{z} \\ &+ B_{2} \sup_{n} \int_{-\infty}^{\infty} |f(\lambda_{n},x_{w})|^{p} dx_{w} < \infty, \end{split}$$

where  $B_1 = B_1(p, \tau, \varepsilon_1)$  and  $B_2 = B_2(p, \tau, \varepsilon_2)$ .

Remark 3.7 In the above proposition, if we replace the conditions (9) by

$$\int_{-\infty}^{\infty}\int_{-\infty}^{\infty}|f(x_z,x_w)|^pdx_z\,dx_w<\infty$$

the interior integral is finite everywhere except on a null set. If we use Fubini to change the order of integration, we get a null set for the integral against the second variable. If we know that none of  $\lambda_n$ 's and  $\mu_n$ 's lie in these null sets, the conclusion still holds.

**Theorem 3.8** If  $\{\lambda_n\}_{n \in \mathbb{Z}}$  and  $\{\mu_n\}_{n \in \mathbb{Z}}$  are separated sequences of real numbers such that  $0 \leq \lambda_n \leq 1$  and  $0 \leq \mu_n \leq 1$  for each *n*, then the Gabor system (2) forms a Bessel sequence in  $L^2(\mathbb{R}^2)$ . If  $\sum_n |c_n|^2 < \infty$ , then the Gabor expansion

$$\sum_{n} c_n e^{2\pi i \mu_n \xi - \pi (\xi - \lambda_n)^2}$$

converges in mean to an element of  $L^2(\mathbb{R}^2)$ .

**Proof.** If  $\phi \in L^2(\mathbb{R}^2)$  then the inner product

$$a_n = \langle \sqrt{2} e^{2\pi i \mu_n \xi - \pi (\xi - \lambda_n)^2}, \phi(\xi) \rangle;$$

is just the value  $f(\lambda_n, \mu_n)$  of the entire function

$$f(z,w) = \sqrt{2} \int_{\mathbb{R}^2} \varphi(\xi) e^{2\pi i w \xi - \pi (\xi - z)^2} d\xi; \varphi(\xi) = \overline{\phi(\xi)},$$

in the Gabor space  $G_g$  and f is of order of growth 2. we have

$$\begin{split} \sup_{n} \int_{-\infty}^{\infty} |f(x_{z}, \mu_{n})|^{p} dx_{z} \\ &\leq 2^{p/2} M^{p} e^{\pi} \int_{-\infty}^{\infty} \left[ \int_{\mathbb{R}} e^{-2\pi (x_{\xi} - x_{z})^{2}} dx_{\xi} \int_{\mathbb{R}} e^{-2\pi (|y_{\xi}| - 1)^{2}} dy_{\xi} \right]^{p/2} dx_{z} < \infty, \end{split}$$

and similarly

$$\sup_n \int_{-\infty}^{\infty} |f(\lambda_n, x_w)|^p \, dx_w < \infty.$$

Therefore f satisfies conditions (9) and by Proposition 3.6 we have

$$\sum_{n} |\langle \sqrt{2} e^{2\pi i \mu_n \xi - \pi (\xi - \lambda_n)^2}, \phi(\xi) \rangle|^2 = \sum_{n} |a_n|^2 = \sum_{n} |f(\lambda_n, \mu_n)|^2 < \infty.$$

Thus the Gabor system (2) forms a Bessel sequence in  $L^2(\mathbb{R}^2)$ . The second part follows from the first by Proposition 2.4.

Paley and Wiener, showed in Theorem XLII of [16] that whenever

$$\lim_{n\to\pm\infty}(\lambda_{n+1}-\lambda_n)=\infty,$$

for a sequence of real numbers  $\{\lambda_n\}$ , then the exponentials are weakly independent over an arbitrarily short interval:  $\sum a_n e^{i\lambda_n t} = 0$  only when all the  $a_n$  are zero. The next lemma states a similar statement for the set of complex exponentials replaced by the system (4). Here l.i.m. is used to show the limit in mean-square in  $L^2$ . The proof is almost identical to that of Paley and Wiener.

**Lemma 3.9** Let no  $a_n$  vanish,  $\sum_{-\infty}^{\infty} |a_n|^2$  converge, and let

$$\cdots < \lambda_{-n} < \cdots < \lambda_{-1} < \lambda_0 < \lambda_1 < \cdots < \lambda_n < \cdots$$

such that

$$\lim_{n\to\pm\infty}(\lambda_{n+1}-\lambda_n)=\infty.$$

Let

$$f(t) = 1.i.m._{N \to \infty} \sum_{-N}^{N} a_n e^{2\pi i \lambda_n t - \pi (t - \lambda_n)^2};$$

over every finite range. If f(t) is equivalent to zero over any interval (a, b) then f(t) is equivalent to zero over every interval, and all the  $a_n$ 's vanish.

Now we want to show that if the separation of the  $\lambda_n$ 's is great enough then system (4) is a Riesz-Fischer sequence.

**Theorem 3.10** Let  $\{\lambda_n\}$  be a sequence of real numbers whose differences are nondecreasing and satisfy

$$\sum \frac{1}{(\lambda_{k+1} - \lambda_k)^2} < \infty.$$

Then the Gabor system (4) is a Riesz-Fischer sequence in  $L^2(\mathbb{R})$ .

**Proof.** We adapt the proof of [16, Th. 1]. By the second part of the Proposition 2.4 we have to show that for all finite sequences of scalars  $\{c_n\}$  and some constant m > 0,

$$m\sum |c_n|^2 \leq \left\|\sum c_n \sqrt[4]{2} e^{2\pi i \lambda_n t - \pi (t - \lambda_n)^2}\right\|^2.$$
(11)

Using *c* to denote an  $l^2$  sequence  $\{c_1, c_2, \dots\}$ , inequality (11) is the same as

$$\frac{\langle Gc,c\rangle_{l^2}}{\langle c,c\rangle_{l^2}} \ge m,$$

where the  $l^2$  operator *G* is the Gram matrix of the members of the Gabor system (4). It is to be shown that the eigenvalues of finite subsections of *G* are bounded away from zero, which in turn follows from these two conditions:

- (1) Gv = 0 implies v = 0, for every  $l^2$  sequence v.
- (2) G = I + M, where *M* is a compact operator.

The first condition is satisfied by Lemma 3.9. To verify condition (2), observe that the entries of G = I + M are

$$g_{nm} = \sqrt{2} \int_{-\infty}^{\infty} e^{2\pi i (\lambda_n - \lambda_m)t - \pi (t - \lambda_n)^2 - \pi (t - \lambda_m)^2} dt.$$

Now M can be shown to be compact by showing that its Schmidt norm is finite. Since G is symmetric, it suffices to show that

$$\sum_{n=1}^{\infty}\sum_{m=n+1}^{\infty}g_{nm}^2 < \infty$$

The sum is bounded above,

$$\begin{split} \sum_{n=1}^{\infty} \sum_{m=n+1}^{\infty} g_{nm}^2 &= 2 \sum_{n=1}^{\infty} \sum_{m=n+1}^{\infty} \left( \int_{-\infty}^{\infty} e^{2\pi i (\lambda_n - \lambda_m)t - \pi (t - \lambda_n)^2 - \pi (t - \lambda_m)^2} dt \right)^2 \\ &\leq 2 \sum_{n=1}^{\infty} \sum_{m=n+1}^{\infty} \left( \int_{-\infty}^{\infty} e^{2\pi i (\lambda_n - \lambda_m)t} dt \right)^2 \\ &= 2 \sum_{n=1}^{\infty} \sum_{m=n+1}^{\infty} \lim_{A \to \infty} \left( \int_{-A}^{A} e^{2\pi i (\lambda_n - \lambda_m)t} dt \right)^2 \\ &\leq \frac{2}{\pi^2} \sum_{n=1}^{\infty} \sum_{m=n+1}^{\infty} \frac{1}{(\lambda_n - \lambda_m)^2} \\ &< \frac{2}{\pi^2} \sum_{n=1}^{\infty} \sum_{m=n+1}^{\infty} \frac{1}{(\lambda_{n+1} - \lambda_n)^2 (m-n)^2}, \end{split}$$

where  $(\lambda_m - \lambda_n) \leq (\lambda_{n+1} - \lambda_n)(m+n)$  follows from the assumption that differences are nondecreasing. Letting k = m + n, one concludes that

$$\sum_{n=1}^{\infty}\sum_{m=n+1}^{\infty}g_{nm}^2 < C\sum_{n=1}^{\infty}\frac{1}{(\lambda_{n+1}-\lambda_n)^2} < \infty,$$

establishing the theorem.

Theorem 3.11 Let

$$f(z) = \int_{-\infty}^{\infty} \alpha(t) e^{2\pi i z t - \pi (t-z)^2} dt,$$

where  $\alpha \in L^2(\mathbb{R})$ . If  $f(\mu) = 0$  and  $g(z) = \frac{z - \lambda}{z - \mu} f(z)$ , then there exists a function  $\beta$  in  $L^2(\mathbb{R})$  such that

$$g(z) = \int_{-\infty}^{\infty} \beta(t) e^{2\pi i z t - \pi (t - z)^2} dt.$$
 (12)

Moreover,

$$\beta(t) = \alpha(t) + 2\pi(i+1)(\lambda-\mu)e^{-2\pi i\mu t + \pi(t-\mu)^2} \int_{-\infty}^t \alpha(s)e^{2\pi i\mu s - \pi(s-\mu)^2} ds$$
(13)

almost everywhere on  $\mathbb{R}$ .

**Proof.** To motivate the proof, let us suppose that g(z) is in fact representable in the form (12), and try to deduce (13). If (12) holds, then

$$\frac{1}{z-\mu}\int_{-\infty}^{\infty}\alpha(t)e^{2\pi i z t-\pi(t-z)^2}\,dt=\frac{1}{z-\lambda}\int_{-\infty}^{\infty}\beta(t)e^{2\pi i z t-\pi(t-z)^2}\,dt.$$

The trick in solving for  $\beta(t)$  is to transform each of these integrals by first rewriting  $e^{2\pi i z t - \pi (t-z)^2}$  as

$$e^{2\pi i z t - \pi (t-z)^2} = e^{2\pi i (z-\mu)t + 2\pi i \mu t - \pi (t-\mu)^2 + \pi (z-\mu)(2t-z-\mu)}$$

and then integrating by parts. When this is done, the result is

$$\frac{1}{z-\mu} \int_{-\infty}^{\infty} \alpha(t) e^{2\pi i z t - \pi (t-z)^2} dt = \int_{-\infty}^{\infty} \alpha_1(t) e^{2\pi i z t - \pi (t-z)^2} dt,$$

with

$$\alpha_1(t) = -2(i+1)\pi e^{-2\pi i\mu t + \pi(t-\mu)^2} \int_{-\infty}^t \alpha(s) e^{2\pi i\mu s - \pi(s-\mu)^2} \, ds,$$

and

$$\frac{1}{z-\lambda} \int_{-\infty}^{\infty} \beta(t) e^{2\pi i z t - \pi (t-z)^2} dt = \int_{-\infty}^{\infty} \beta_1(t) e^{2\pi i z t - \pi (t-z)^2} dt$$

with

$$\beta_1(t) = -2(i+1)\pi e^{-2\pi i\lambda t + \pi(t-\lambda)^2} \int_{-\infty}^t \beta(s) e^{2\pi i\lambda s - \pi(s-\lambda)^2} ds.$$

It follows that  $\alpha_1(t) = \beta_1(t)$  almost everywhere on  $\mathbb{R}$ , and so

$$e^{2\pi i(\lambda-\mu)t+\pi(\lambda-\mu)(2t-(\lambda+\mu))} \int_{-\infty}^{t} \alpha(s) e^{2\pi i\mu s-\pi(s-\mu)^2} ds$$
$$= \int_{-\infty}^{t} \beta(s) e^{2\pi i\lambda s-\pi(s-\lambda)^2} ds$$

To obtain (13), differentiate both sides of this equation with respect to *t*. Now simply observe that all of the above steps are reversible, that is  $\beta \in L^2(\mathbb{R})$ .

**Remark 3.12** A similar result holds when f is of the form

$$f(z) = \int_{-\infty}^{\infty} e^{2\pi i z t - \pi (t-z)^2} d\alpha(t),$$

and  $\alpha$  is of bounded variation on  $\mathbb{R}$ , only now

$$g(z) = \int_{-\infty}^{\infty} e^{2\pi i z t - \pi (t-z)^2} d\beta(t),$$

with

$$d\beta(t) = d\alpha(t) + 2\pi i (\lambda - \mu) e^{-2\pi i \mu t + \pi (t - \mu)^2} \int_{-\infty}^{t} e^{2\pi i \mu s - \pi (s - \mu)^2} d\alpha(s).$$

**Corollary 3.13** The completeness of system (4) is unaffected if one  $\lambda_n$  is replaced by another number.

Nowak [18] showed that the deficit of the regular Gabor system generated by  $h \in L^2(\mathbb{R}^d)$  and a, b > 0 is either zero or infinite if the system is a Bessel sequence in  $L^2(\mathbb{R}^d)$ . The next result on the deficit of the irregular Gabor system (4) is proved as in [19, Th. 4.6]. Here we give the proof for the sake of completeness.

**Theorem 3.14** If  $\{\lambda_n\}$  is a separated sequence of real numbers such that

$$\lambda_{n+1} - \lambda_n > 1; (n = 0, \pm 1, \pm 2, \cdots)$$

then the Gabor system (4) has infinite deficiency in  $L^2(\mathbb{R})$ .

**Proof.** Let N be a fixed but arbitrary positive integer. If K is large enough, then we can replace

$$\lambda_0, \lambda_1, \cdots, \lambda_K$$

by

 $\mu_0, \mu_1, \cdots, \mu_{K+N+1},$ 

so that the resulting sequence, relabeled  $\{\mu_n\}$ , satisfies

$$\inf_n(\mu_{n+1}-\mu_n)>1.$$

By Theorem 3.10 there is a function  $\varphi \in L^2(\mathbb{R})$  such that

$$\int_{\mathbb{R}} \varphi(t) \sqrt[4]{2} e^{-2\pi i \mu_n t - \pi (t - \mu_n)^2} dt = \begin{cases} 1 \text{ if } n = 0, \\ 0 \text{ if } n \neq 0 \end{cases}$$

Thus the system

$$\left\{\sqrt[4]{2}e^{2\pi i\mu_n t - \pi (t - \mu_n)^2} : n \neq 0\right\}$$

is incomplete in  $L^2(\mathbb{R})$ , and we conclude by the above corollary that the deficiency of the system in  $L^2(\mathbb{R})$  is at least *N*.

#### 4. Stability

In this section we study stability of sampling sets in Gabor spaces. Here we let  $\mathcal{G}_h$  to be the Gabor space of a Gabor window  $h \in L^2(\mathbb{R}^d)$ , and  $\Lambda$  be a discrete set in  $\mathbb{C}^d$ .

**Proposition 4.1** [17, Cor. 3.2.3] (Inversion formula for the Gabor transform) Let  $h, \gamma \in L^2(\mathbb{R}^d)$  be such that  $\langle h, \gamma \rangle \neq 0$ , and we consider  $V_h f(z) = \langle f, h_z \rangle$ , for every  $f \in L^2(\mathbb{R}^d)$ . Then it is fulfilled that  $V_h f \in L^2(\mathbb{C}^d)$ . Moreover we have inversion formula given by:

$$f(t) = \frac{1}{\langle h, \gamma \rangle} \int_{\mathbb{C}^d} V_h f(z) M_y T_x \gamma(t) \, dy \, dx; \quad z = x + iy \in \mathbb{C}^d.$$

The image of  $L^2(\mathbb{R}^d)$  under the Gabor transform with the window *h*, forms a reproducing kernel Hilbert space

$$\mathcal{G}_h = \{ V_h f : f \in L^2(\mathbb{R}^d) \}$$

(a closed subspace of  $L^2(\mathbb{C}^d)$ ) which is called *Gabor space* or *model space*.

The following result is proved for d = 1 in [19, Prop. 1.29], the proof given here is based on [17].

**Proposition 4.2** The Gabor space  $\mathcal{G}_h$  of a Gabor window  $h \in L^2(\mathbb{R}^d)$  is a Hilbert subspace of  $L^2(\mathbb{C}^d)$  that is characterized for the following reproducing kernel:

$$k_h(z, z_0) = k(z, z_0) = k_{z_0}(z) = \langle h_{z_0}, h_z \rangle$$

That is,  $F \in \mathcal{G}_h$  if and only if

$$F \in L^2(\mathbb{C}^d)$$

and

$$F(z_0) = \int_{\mathbb{C}^d} F(z) \,\overline{k(z, z_0)} \, dx \, dy. \tag{14}$$

**Proof.** We introduced the inversion formula for the Gabor transform in Proposition 4.1. Without loss of generality, we may assume that ||h|| = 1. Now for  $z_0 = x_0 + iy_0 \in \mathbb{C}^d$  we have

$$\begin{aligned} V_h f(z_0) &= \int_{\mathbb{R}^d} f(t) \, \overline{M_{y_0} T_{x_0} h(t)} \, dt \\ &= \int_{\mathbb{R}^d} \Big( \int_{\mathbb{C}^d} V_h f(z) M_y T_x h(t) dx \, dy \Big) \overline{M_{y_0} T_{x_0} h(t)} \, dt \end{aligned}$$

where z = x + iy. Switching the integrals we have

$$\begin{split} V_h f(z_0) &= \int_{\mathbb{C}^d} V_h f(z) \Big( \int_{\mathbb{R}^d} M_y T_x h(t) \,\overline{M_{y_0} T_{x_0} h(t)} \, dt \Big) dx \, dy \\ &= \int_{\mathbb{C}^d} V_h f(z) \Big( \int_{\mathbb{R}^d} h_z(t) \overline{h_{z_0}(t)} \, dt \Big) dx \, dy, \end{split}$$

that is,

$$F(z_0) = \int_{\mathbb{C}^d} F(z) \langle h_z, h_{z_0} \rangle dx \, dy$$
$$= \int_{\mathbb{C}^d} F(z) \overline{k(z, z_0)} dx \, dy.$$

Therefore k replays all the functions of the space, and as it belongs to this space, it is its reproducing kernel.

For  $x, y \in \mathbb{R}^d$  we recall  $T_x$  describes a translation by x also called a time shift and  $M_y$  a modulation by y also called a frequency shift. So the operators of the form  $M_y T_x$  or  $T_x M_y$  are known as time-frequency shifts. They satisfy the commutation relations

$$T_x M_y f(t) = (M_y f)(t - x)$$
$$= e^{2\pi i y \cdot (t - x)} f(t - x)$$
$$= e^{-2\pi i y \cdot x} M_y T_x f(t)$$

Then we have

In terms of  $k_h(z) = k_h(z, 0) = \langle h, h_z \rangle$  one has

$$\begin{aligned} k_h(z,z_0) &= \overline{\langle h_z, h_{z_0} \rangle} = \overline{e^{2\pi i x.(y-y_0)} \langle h, h_{z_0-z} \rangle} \\ &= \overline{e^{2\pi i x.(y-y_0)} k_h(z_0-z)} \end{aligned}$$

and hence the reproduction formula (14) takes the form

$$F(z_0) = \int_{\mathbb{C}^d} F(z) e^{2\pi i x \cdot (y-y_0)} k_h(z_0 - z) dx \, dy$$

Using this notations we can deduce that

$$V_h f_{z_0}(z) = \langle f_{z_0}, h_z \rangle = e^{2\pi i x_0 \cdot (y_0 - y)} \langle f, h_{z - z_0} \rangle$$
  
=  $e^{2\pi i x_0 \cdot (y_0 - y)} V_h f(z - z_0).$ 

In this way, to be consistent with the notation and the definition of the transform, we have to define the translations in  $\mathbb{C}^d$  of a function  $F \in \mathcal{G}_h$  (or in  $L^2(\mathbb{C}^d)$  in a general way) as:

$$F_{z_0}(z) = e^{2\pi i x_0 \cdot (y_0 - y)} F(z - z_0).$$

It is necessary to observe that these translations do not coincide in general with the usual translation of  $\mathbb{C}^d$ . But if we look at the function, then we have

$$|F_{z_0}(z)| = |F(z - z_0)|.$$

Since in general the function  $F(z - z_0)$  can not belong to  $G_h$ . Taking this into account we can write the reproduction formula in a bit more compact way

$$F(z_0) = \int_{\mathbb{C}^d} F(z) k_z(z_0) dx \, dy$$

The Gabor space has certain good continuity properties. More precisely, the functions of the space will be uniformly continuous. For  $F \in \mathcal{G}_h$ , since F is defined as a definite integral, it is uniformly continuous with respect to the free variable of the integrand, i.e. for each  $\varepsilon > 0$  there exists  $\delta > 0$  such that if  $|z_1 - z_2| < \delta$  by using triangle inequality we have

$$||F(z_1)| - |F(z_2)|| \leq |F(z_1) - F(z_2)| < \varepsilon$$

Ascensi [19] formalized this idea in the case d = 1 with the following result.

**Proposition 4.3** [19, Prop. 5.1] Let  $\mathcal{G}_h$  be the Gabor space of normalized Gabor window  $h \in L^2(\mathbb{R}^d)$ . Then, given  $\varepsilon$  there exists  $\delta$  such that if  $|z_1 - z_2| < \delta$ , then for every  $F \in \mathcal{G}_h$ 

$$F(z) = \langle f, h_z \rangle$$

it is fulfilled that

$$||F(z_1)| - |F(z_2)|| < ||F||\varepsilon = ||f||\varepsilon.$$

A good description of the Gabor space is most convenient if there are some complete characterizations. The best situation occurs when for some analyzing function the Gabor space is a space of holomorphic functions. The most important example and the only possible one is the Gaussian function, for which the Gabor space can be identified with the Fock space, in which the sampling and interpolation sets are completely characterized [20]. The following assertion is proved for d = 1 in [7], we do not know if the same holds in higher dimensions.

**Problem 4.4** Consider the Gabor space with a Gabor window  $h \in L^2(\mathbb{R}^d)$ 

$$\mathcal{G}_h = \Big\{ F(z) = \int_{\mathbb{R}^d} f(t) e^{-2\pi i y \cdot t} \overline{h(t-x)} \, dt, \, f \in L^2(\mathbb{R}^d) \Big\}.$$

Then this space is a space of antiholomorphic functions (i.e., F(x, -y) is holomorphic), modulo a multiplication by a weight, if and only if *h* is a time-frequency translation of the Gaussian function.

As the space in that we will work is formed by continuous functions and it has reproducing kernel, we can sample the functions at any point. Given a set of points of  $\mathbb{C}^d$  we can consider, for each  $F \in \mathcal{G}_h$ , the succession of values that F takes in this set.

**Definition 4.5** A discrete set  $\Lambda = \{z_j\}_{j \in \mathbb{Z}}$  in  $\mathbb{C}^d$  is said to be a *sampling set* for  $\mathcal{G}_h$  if there are constants A, B > 0 such that

$$A\|F\|^2 \leq \sum_{j \in \mathbb{Z}} |F(z_j)|^2 \leq B\|F\|^2 F \in \mathcal{G}_h$$

These sets are very important since they correspond with frames. We give some properties of Gabor space and sampling set in the case d > 1. The case d = 1 was considered by Ascensi and Bruna in [7]. The proofs are essentially the same (with little changes in certain cases). Recall that  $\mathcal{G}_h = \{V_h f : f \in L^2(\mathbb{R}^d)\}$  is the Gabor space. Here we assume that ||h|| = 1.

**Proposition 4.6** If  $\Lambda = \{z_j\}_{j \in \mathbb{N}}$  is a sampling set for  $\mathcal{G}_h$  then  $\Lambda$  is a relatively separated set.

Proof. The proof is exactly similar to the proof of [7, Prop. 3.1].

**Definition 4.7** Given a continuous function *F* defined in  $\mathbb{C}^d$  we define its *local maximal function* as:

$$MF(z) = \sup_{|w-z|<1} |F(w)|$$

**Lemma 4.8** Let  $\Lambda = {\lambda_i}_{i \in \mathbb{Z}}$  be a separated set with separation constant  $\varepsilon$ . Then

$$\sum_{\lambda \in \Lambda} |k(\lambda)| < \frac{1}{c\varepsilon^{2d}} \|Mk\|_1,$$

where c = m(B(0, 1)).

**Proof.** We suppose without loss of generality that  $1 < \varepsilon < 2$ . Then using sub-mean-value inequality

$$\begin{split} \sum_{\lambda \in \Lambda} |k(\lambda)| &\leq \sum_{\lambda \in \Lambda} \frac{1}{|B(\lambda, \varepsilon)|} \int_{B(\lambda, \varepsilon)} |k(z)| \, dm(z) \\ &\leq \sum_{\lambda \in \Lambda} \frac{1}{|B(\lambda, \varepsilon)|} \int_{B(\lambda, \varepsilon)} Mk(z) \, dm(z) \\ &\leq \sum_{\lambda \in \Lambda} \frac{1}{|B(\lambda, \varepsilon)|} \int_{\mathbb{C}^d} Mk(z) \, dm(z). \end{split}$$

Since by hypothesis those balls are disjoint, then

$$\sum_{\lambda \in \Lambda} |k(\lambda)| < \frac{1}{c\varepsilon^{2d}} \|Mk\|_1.$$

**Proposition 4.9** If  $\Lambda$  is a separated set, there exists B > 0 such that

$$\sum_{\lambda \in \Lambda} |F(\lambda)|^2 \leq B ||F||^2; \quad F \in \mathcal{G}_h.$$

Proof. Calculating directly we have that

$$\begin{split} \sum_{\lambda \in \Lambda} |F(\lambda)|^2 &= \sum_{\lambda \in \Lambda} \left| \int_{\mathbb{C}^d} F(z) \overline{k_\lambda(z)} \, dm(z) \right|^2 \\ &\leq \sum_{\lambda \in \Lambda} \left( \int_{\mathbb{C}^d} |F(z)|^2 |k_\lambda(z)| \, dm(z) \right) \times \left( \int_{\mathbb{C}^d} |k_\lambda(z)| \, dm(z) \right) \\ &= \int_{\mathbb{C}^d} |F(z)|^2 \sum_{\lambda \in \Lambda} |k(z-\lambda)| \, dm(z) \times \int_{\mathbb{C}^d} |k(z)| \, dm(z). \end{split}$$

Here  $\int_{\mathbb{C}^d} |k(z)| dm(z) = m < \infty$  because the kernel is integrable and also

$$\sum_{\lambda \in \Lambda} |k(z - \lambda)| = \sum_{\gamma \in (z - \Lambda)} |k(\gamma)|$$

is bounded independently of z, and since  $z - \Lambda$  has the same separation constant as  $\Lambda$  we can apply Lemma 4.8. Then

$$\sum_{\lambda \in \Lambda} |F(\lambda)|^2 \leq \int_{\mathbb{C}^d} |F(z)|^2 \sum_{\gamma \in (z-\Lambda)} |k(\gamma)| \, dm(z) \int_{\mathbb{C}^d} |k(z)| \, dm(z)$$
$$\leq B \|F\|^2,$$

where  $B = \frac{m}{c\varepsilon^{2d}} ||Mk||_1$  and  $\varepsilon$  is the separation constant of  $\Lambda$ .

Next, we want to know when the Gabor system  $G(h, \Lambda)$  is a frame for  $L^2(\mathbb{R}^d)$ . First we observe that  $V_h f(z) = \langle f, h_z \rangle$  and  $||V_h f|| = ||f||$  (if ||h|| = 1). As we have bijective correspondence between  $\mathcal{G}_h$  and  $L^2(\mathbb{R}^d)$  by the Gabor transform, we can write

$$\sum_{\lambda \in \Lambda} |F(\lambda)|^2 = \sum_{\lambda \in \Lambda} |V_h f(\lambda)|^2 = \sum_{\lambda \in \Lambda} |\langle f, h_\lambda \rangle|^2$$

for every  $f \in L^2(\mathbb{R}^d)$  or for every  $V_h f \in \mathcal{G}_h$ . Therefore the frame condition and that of sampling set are equivalent. We conclude that: given a discrete set  $\Lambda \subset \mathbb{C}^d$  and a Gabor window  $h \in L^2(\mathbb{R}^d)$ ,  $G(h, \Lambda)$  is a frame for  $L^2(\mathbb{R}^d)$  if and only if  $\Lambda$  is a sampling set for  $\mathcal{G}_h$ .

Let  $\Sigma_{\alpha} = \{h \in C^{\infty}(\mathbb{R}) \cap L^{2}(\mathbb{R}) : h' + zh \in L^{2}(\mathbb{R}) \text{ and } \|h' + zh\|_{2} \leq \alpha \|h\|_{2} \text{ for } z(t) = t \ t \in \mathbb{R} \}.$ It is clear that  $C_{c}^{\infty}(\mathbb{R}) \subseteq \Sigma_{\alpha}$  and so  $\Sigma_{\alpha}$  is a non empty set.

**Lemma 4.10** Let  $h \in \Sigma_{\alpha}$  and let  $\{\lambda_n\}_{n \in \mathbb{N}}$  and  $\{\mu_n\}_{n \in \mathbb{N}}$  be sequences of scalars and suppose that there exist positive numbers *B* and *L* such that

$$\sum_{n} |F(\lambda_{n})|^{2} \leq B ||F||^{2}; (F \in \mathcal{G}_{h})$$

and

$$|\mu_n - \lambda_n| \leq L, (n = 1, 2, 3, \cdots).$$

Then for every  $F \in \mathcal{G}_h$ 

$$\sum_{n} |F(\lambda_{n}) - F(\mu_{n})|^{2} \leq B(e^{\alpha L} - 1)^{2} ||F||^{2}.$$

**Proof.** Let *F* be an element of  $\mathcal{G}_h$ . By expanding *F* in a Taylor series about  $\lambda_n$ , we find that

$$F(\mu_n)-F(\lambda_n)=\sum_{k=1}^{\infty}\frac{F^{(k)}(\lambda_n)}{k!}(\mu_n-\lambda_n)^k(n=1,2,3,\cdots).$$

If  $\rho$  is an arbitrary positive number, then by multiplying and dividing the summand by  $\rho^k$  we find also that

$$|F(\mu_n) - F(\lambda_n)|^2 \leq \sum_{k=1}^{\infty} \frac{|F^{(k)}(\lambda_n)|^2}{\rho^{2k}k!} \sum_{k=1}^{\infty} \frac{\rho^{2k}|\mu_n - \lambda_n|^{2k}}{k!}$$

Since  $\mathcal{G}_h$  is closed under differentiation and  $||F'||_2 \leq \alpha ||F||_2$  it follows that

$$\sum_{n} |F^{(k)}(\lambda_{n})|^{2} \leq B ||F^{(k)}||^{2}$$
$$\leq B \alpha^{2k} ||F||^{2}, \quad k = 1, 2, 3, \cdots$$

Therefore we obtain

$$\sum |F(\lambda_n) - F(\mu_n)|^2 \leq B ||F||^2 \sum_{k=1}^{\infty} \frac{\alpha^{2k}}{\rho^{2k}k!} \sum_{k=1}^{\infty} \frac{(\rho L)^{2k}}{k!}$$
$$= B ||F||^2 (e^{\frac{\alpha^2}{\rho^2}} - 1) (e^{\rho^2 L^2} - 1)$$

since  $|\mu_n - \lambda_n| \leq L$ . Now by choosing  $\rho = \sqrt{\frac{\alpha}{L}}$  we get

$$\sum_{n} |F(\lambda_{n}) - F(\mu_{n})|^{2} \leq B(e^{\alpha L} - 1)^{2} ||F||^{2}.$$

**Theorem 4.11** If  $\{\lambda_n\}_{n \in \mathbb{N}}$  is a sampling set for  $\mathcal{G}_h(h \in \Sigma_\alpha)$  then there exists positive constant L such that if  $\{\mu_n\}_{n \in \mathbb{N}}$  satisfies  $|\lambda_n - \mu_n| \leq L$  for all n, then  $\{\mu_n\}_{n \in \mathbb{N}}$  is also sampling set.

**Proof.** Since  $\{\lambda_n\}_{n \in \mathbb{N}}$  is a sampling set for  $\mathcal{G}_h$ , then there exist positive constants A and B such that

$$A||F||^2 \leq \sum_n |F(\lambda_n)|^2 \leq B||F||^2$$

for every function *F* belonging to the Gabor space  $\mathcal{G}_h$ . Let  $\{\mu_n\}_{n \in \mathbb{N}}$  be complex scalars for which  $|\lambda_n - \mu_n| \leq L(n = 1, 2, 3, \cdots)$ . It is to be shown that if *L* is sufficiently small, then similar inequalities hold for the  $\mu_n$ 's.

By virtue of the previous lemma, for every  $F \in \mathcal{G}_h$ ,

$$\sum_{n} |F(\lambda_{n}) - F(\mu_{n})|^{2} \leq B(e^{\alpha L} - 1)^{2} ||F||^{2}$$

and since  $||F||^2 \leq \frac{1}{A} \sum_n |F(\lambda_n)|^2$  to have

$$\sum_{n} |F(\lambda_{n}) - F(\mu_{n})|^{2} \leq C \sum_{n} |F(\lambda_{n})|^{2}$$

where  $C = \frac{B}{A}(e^{\alpha L} - 1)^2$ . Applying Minkowski's inequality, we find that

$$\left|\sqrt{\sum |F(\lambda_n)|^2} - \sqrt{\sum |F(\mu_n)|^2}\right| \leq \sqrt{C\sum |F(\lambda_n)|^2},$$

and hence

$$\sqrt{A}(1-\sqrt{C})\|F\| \leq \sqrt{\sum |F(\mu_n)|^2} \leq \sqrt{B}(1+\sqrt{C})\|F\|$$

for every *F*. Since *C* is less than 1 if *L* is sufficiently small,  $\{\mu_n\}_{n \in \mathbb{N}}$  is a sampling set for  $\mathcal{G}_h$ .

**Problem 4.12** Let  $h, k \in L^2(\mathbb{R})$ . It would be desirable to show that there exists  $\varepsilon > 0$  such that if  $||k - h|| < \varepsilon$  and  $\{\lambda_n\}$  is a sampling set for  $\mathcal{G}_h$  then  $\{\lambda_n\}$  is a sampling set for  $\mathcal{G}_k$ . If one can show this and  $h \in \Sigma_\alpha$ , then for each  $k \in L^2(\mathbb{R})$  with  $||k - h|| < \varepsilon$  the stability result of Theorem 4.11 holds for  $\mathcal{G}_k$  as well. Now since  $\Sigma_\alpha$  is norm dense in  $L^2(\mathbb{R})$ , one could conclude that Theorem 4.11 holds for each  $h \in L^2(\mathbb{R})$ . At present we are not able to prove that a "small" perturbation does not effect sampling set.

## Acknowledgement

This is part of the Ph.D. thesis of the first author in Tarbiat Modares University. She would like to thank Tarbiat Modares University and MSRT for moral and financial support. Part of this work appeared in a joint paper of the authors in Journal of Sciences, Islamic Republic of Iran.

## Author details

Nafya Hameed Mohammad<sup>1</sup> and Massoud Amini<sup>2</sup>

\*Address all correspondence to: nafya.mohammad@su.edu.iq; mamini@modares.ac.ir

1 Department of Mathematics, College of Education, Salahaddin University, Erbil, Iraq

2 Department of Mathematics, Faculty of Mathematical Sciences, Tarbiat Modares University, Tehran, Iran

## References

- [1] Gabor, D., Theory of Communication, J. Inst. Elec. Eng. 93 (1946) 429-457.
- [2] Folland, G. B., *Harmonic Analysis in Phase Space*, Princeton University Press, Princeton, 1989.
- [3] Feichtinger, H. G. and Gröchenig, K., Banach spaces related to integrable group representations and their atomic decompositions. I., J. Funct. Anal. 86(2) (1989) 307-340.
- [4] Liang, T. and Juan, G., Fast parallel algorithms for discrete Gabor expansion and transform based on multirate filtering, *Science China* 55(2) (2012) 293-300.
- [5] Wexler, J. and Raz, S., Discrete Gabor expansions, Signal Processing 21 (1990) 207-220.
- [6] Borichev, A., Gröchenig, K. and Lyubarskii, Yu., Frame constants of Gabor frames near the critical density, *J. Math. Pures Appl.* 94 (2010) 170-182.
- [7] Ascensi, G. and Bruna, J., Model space results for the Gabor and wavelet transforms, *IEEE Trans. Inform. Theory* 55(5) (2009) 2250-2259.

- [8] Abreu, L. D., On the structure of Gabor and super Gabor spaces, Monatsh Math. 161 (2010) 237-253.
- [9] Christensen, O., Frames and Bases, An Introductory Course, Birkhäuser, Boston, 2008.
- [10] Duffin, R. J. and Schaeffer, A. C., A class of nonharmonic Fourier series, *Trans. Amer. Math. Soc.* 72(2) (1952) 341-366.
- [11] Young, R. M., An Introduction to Nonharmonic Fourier Series, 2nd. ed., Academic Press, New York, 2001.
- [12] Reid, R. M., A class of Riesz-Fischer sequences, Proc. Amer. Math. Soc. 123(3) (1995) 827-829.
- [13] Jaffard, S., Pointwise and directional regularity of nonharmonic Fourier series, *Appl. Comput. Harmon. Anal.* 22(3) (2010) 251-266.
- [14] Krantz, S. G., Function Theory of Several Complex Variables, 2nd ed., Amer. Math. Soc., Providence, 2001.
- [15] Shabat, B. V., Introduction to Complex Analysis, Part II, Functions of Several Variables, Amer. Math. Soc., Providence, 1992.
- [16] Paley, R. C. and Wiener, N., *Fourier Transforms in the Complex Domain*, Colloquium Publications, vol. 19, Amer. Math. Soc., New York, 1934.
- [17] Gröchenig, K., Foundations of Time-Frequency Analysis, Birkhäuser, Boston, 2001.
- [18] Nowak, K., Excess of Gabor Frames, University of Wien, Wien, 2006.
- [19] Ascensi, G., Generators of  $L^p(\mathbb{R})$  by translations in time and frequency, Ph.D. Thesis, Univ. of Wien, 2007.
- [20] Seip, K., Density theorems for sampling and interpolation in the Bargmann-Fock space I, *J. Reine Angew. Math.* 429 (1992) 91-106.

# Mineralogical Characterization of Chalcopyrite Bioleaching

E.R. Mejía, J.D. Ospina, L. Osorno, M.A. Márquez and A.L. Morales

Additional information is available at the end of the chapter

http://dx.doi.org/10.5772/59489

## 1. Introduction

Chalcopyrite (CuFeS<sub>2</sub>) is the most important copper ore, comprising approximately 70% of copper reserves in the world [1,2]. In metallurgical applications, chalcopyrite is mainly subjected to pyrometallurgy treatment after concentration by a flotation process [3,4]. The interest in bio-hydrometallurgy has increased recently in order to minimize the sulfur dioxide emissions, and to reduce energy consumption [5-9]. However, the chalcopyrite copper leaching rate is slower than other copper minerals such as chalcocite (Cu<sub>2</sub>S), covellite (CuS), and bornite ( $Cu_5FeS_4$ ) [10]. Initial rapid leaching rates decline with time, and bioleaching processes release only part of the copper [11]due to so-called passivation reactions at the mineral surfaces [12, 13]. After almost a century of research into the mechanisms of chalcopyrite dissolution in ferric media, there is a consensus with respect to the formation of a passivating film on the surface [3, 11-16]. Despite this, the nature of this film remains unknown, although it has been postulated that it must have low porosity and be a bad electricity conductor (Córdoba et al., 2008a). Various models were describing the mass transfer diffusion and chemical reactions on the chalcopyrite surface. Those models have been proposed to explain the nature and composition of the passivation film that causes slow oxidation of the chalcopyrite: (I) metal-deficient sulfides, (II) elemental sulfur-S<sup>o</sup>, (III) polysulfides-XS<sub>n</sub>, and (vi) jarosite-XFe<sub>3</sub>(SO<sub>4</sub>)<sub>2</sub>(OH)<sub>6</sub> [4, 11-17].

Klauber (2008) [8] reviewed the chemical characteristics of the surface layer of chalcopyrite leached with ferric sulfate and suggested passivation candidates including metal-deficient sulfides and elemental sulfur-S<sup>o</sup>. This author suggested that the metal-deficient sulfide is formed by non-stoichiometric dissolution of sulfides based on analytical evidence. Parker *et al.* (2003) [11] used XPS analysis to detect elemental sulfur, sulfate, and disulfide phases in the



© 2015 The Author(s). Licensee InTech. This chapter is distributed under the terms of the Creative Commons Attribution License (http://creativecommons.org/licenses/by/3.0), which permits unrestricted use, distribution, and eproduction in any medium, provided the original work is properly cited. solid form in chalcopyrite bioleaching experiments. Additionally, chalcopyrite bioleaching results in the dissolution of iron, which potentially leads to precipitation of Fe<sup>3+</sup> hydroxysulfates such as jarosite [11]. Under these conditions, chalcopyrite leaching may involve iron-deficient secondary minerals and intermediates [19].

These studies agreed that the jarosite precipitation is linked to chalcopyrite passivation. These different theories require substantial further research. It is, therefore, crucial to tackle the issue from different angles in an attempt to understand the nature of the recalcitrant chalcopyrite.

Moreover, mineralogical characterization of the products in different types of beneficiation processes, called "process mineralogy," has been performed as a fundamental piece of the planning, optimizing, and monitoring of different minerals [5, 20]. In this way, an appropriate understanding of the mineralogy in the chalcopyrite and its transformation is essential to understanding the passivation mechanism [21]. This type of research can be turned quite complicated due to factors like fine size of particles, low crystallinity, a small proportion of mineral phases, and nature of ore minerals in the various steps of the process. Due to these features it is necessary to use different complementary analytical techniques like electron microscopes, electron microprobe, X-ray diffractometers and spectrometric methods [22, 23].

The primary objective of this research is to characterize the mineral phases generated in the bioleaching process of chalcopyrite and to understand the evolution or transformation of these phases to elucidate its influence on chalcopyrite passivation of the process.

# 2. Material and methods

### 2.1. Mineral

All experiments were carried out using a natural chalcopyrite sample from "La Primavera" Mine (La Cruzada Segovia, Antioquia, Colombia). The mineral was subjected to crushing and milling processes followed by gravimetric separation in a Wilfley table. Afterward, manual concentration was performed under stereographic microscopy. The mineral composition of the sample measured by countdown points was 85.23% chalcopyrite (CuFeS<sub>2</sub>), 1.27% quartz (SiO<sub>2</sub>), 1.69% covellite (CuS), 2.53% sphalerite, and 3.37% molybdenite (MoS<sub>2</sub>). The mineral was milled using an agate mortar. This guaranteed size, pass through 200 Tyler mesh (~75µm), and the mineral was then sterilized in a furnace for 90 min at 80 °C.

### 2.2. Bioleaching experiments

Acidithiobacillus ferrooxidans ATCC 23270 bacterial strains was employed in the bioleaching experiments. The microorganisms were previously grown in T&K medium ((NH<sub>4</sub>)SO<sub>4</sub>: 0.5g/L; MgSO<sub>4</sub>.7H<sub>2</sub>O: 0.5g/L; K<sub>2</sub>HPO<sub>4</sub>: 0.5g/L) [24, 25]. By successive replacement of the ferrous sulfate with chalcopyrite. The medium was acidified to pH 1.8 using H<sub>2</sub>SO<sub>4</sub>. The flasks were sterilized by autoclaving for 20 min, 120°C at 18 psi. The experiment was inoculated with *A*. *ferrooxidans* 10% (v/v) with 10<sup>7</sup> cel/ml. The experiments were carried out for 30 days in 500-mL

flasks containing 300 mL medium with 10% (w/v) chalcopyrite. Those were shaking at 180 rpm and  $30^{\circ}$ C. All conditions were duplicated, and the respective abiotic control was included.

## 2.3. Chemical analysis

Measurements of pH (HACH HQ40d multi PHC30103) and redox potential (Shot Handylab 1 Pt 6880) (reference electrode Ag<sup>0</sup>/AgCl) were performed *in situ* every day. Samples were aseptically withdrawn from the flasks after 24 h and then every five days for mineralogical and chemical analysis. The samples were separated in a DIAMOND IEC DIVISION centrifuge for 15 min at 3000 rpm. Iron and sulfate concentrations were measured with an UV-visible GENESYS<sup>TM</sup> 10 spectrophotometer. The methods employed were 3500-FeD (O-phenantroline) for total iron according to the Standard Methods for water analysis[26].

## 2.4. Mineralogical analysis

Combinations of analytical techniques were used in the mineralogical sample characterization. The Fourier transform infrared (FTIR) spectra for the solid samples were recorded in an FTIR Spectrophotometer Shimadzu Advantage 8400 using KBr pellets in transmission mode. A sample of the KBr mixture at a 1:200 ratio was used. A total of 20 scans with a spectral resolution of 4 cm<sup>-1</sup>, a range of 400–4000 cm<sup>-1</sup>, and Happ-Henzel correction were used. The biooxidation samples were mounted in epoxy resin and polished with sequentially finer SiC grit paper and a final polish with 0.05- $\mu$ m alumina powder. Polished section analysis was performed with JEOL JSM 5910 LV scanning electron microscopy (SEM) in backscattering electron mode and an energy-dispersive X-ray spectroscopy detector (EDX) (Oxford Instrument) using a beam voltage of 18 kV.

X-ray diffraction (XRD) analyses of the samples were conducted in a Bruker D8ADVANCE diffractometer with Cu  $\lambda$ =1.5406 Å radiation generated at 35 kV and 30 mA. XRD data were obtained using a computer-controlled XRD Panalytical X'Pert Pro MPD. The samples collected for mineralogical studies have a statistical representation and the analyses performed by different techniques and on different grains for the same mineral give validity to the results.

# 3. Results

## 3.1. Chalcopyrite leaching experiment

Chalcopyrite oxidation in the inoculated culture presented a low pH (2.1), while the control pH was 2.8. Redox potencial increased from 330 mV until 580 mV. The abiotic control did not change in the time (180 mV). The dissolution of total Fe (Fig. 1) presented continue increase in the time showed a maximum value at 15<sup>th</sup> day (8182.25 ppm) and then decreased and stay invariant until 7251.44 ppm, abiotic control did not show a significant changes in the time (780,12 ppm).



Figure 1. Concentration of total Fe (mg/L) in the Time (Day).

The concentration of  $SO_4^{2-}$  reached its maximum value at 15<sup>th</sup> day (50200 ppm) after this day it was decreased until 25600 ppm (Fig 2). The no inoculated flask did not present considerable variation in the time, and those had a significant difference compared with an inoculated test.



Figure 2. Concentration of sulphate (mg/L) in the Time (day).

Copper extraction was 35.45%; this dissolution was growing at 15<sup>th</sup> day next stabilized in the time. Less than 6% of Cu was solubilized in the chemical controls (Fig. 3).



Figure 3. Copper dissolution (%) in the Time (Day).

#### 3.2. Mineralogical analysis

#### 3.2.1. FTIR measurements

Results obtained by FTIR (Fig 4) showed that the predominant mineral phase present was jarosite, which was confirmed by the presence of the  $v_3$  band (anti-symmetric stretching triply degenerate vibration) at 1190 cm<sup>-1</sup>, 1085 cm<sup>-1</sup>, and 1008 cm<sup>-1</sup>,  $v_4$  band (deformation vibration) at 629 cm<sup>-1</sup>, and  $v_2$  bands (deformation vibration doubly degenerate) at 513 cm<sup>-1</sup> and 470 cm<sup>-1</sup> [19, 21, 27, 28]. There was also absorption at 740 cm<sup>-1</sup>, 870 cm<sup>-1</sup>, and 1414 cm<sup>-1</sup>, which may correspond to  $v_3$  of NH<sub>4</sub><sup>+</sup> in the ammonium jarosite [19]. In addition, typical bands of quartz at 798 cm<sup>-1</sup>, 779 cm<sup>-1</sup>, and 694 cm<sup>-1</sup> could be observed [29] as well as the hydroxyl groups at 3400 cm<sup>-1</sup> and water at 1640 cm<sup>-1</sup> of the jarosite mineral [28, 30]. Bands around 2935 cm<sup>-1</sup> related to the total carbon present on the cell surface showed a permanent increase [31-33]. The samples did not show a significant difference during the first five days, but between the 5<sup>th</sup> and the 10<sup>th</sup> day, the width and intensity of the jarosite bands significantly increased. After this point, the band increases in the samples were very slow. FTIR of uninoculated samples for all tests showed a spectrum with little variation compared with the unleashed sample.



**Figure 4.** Fourier transforms infrared spectra of solid residues after bioleaching of chalcopyrite.  $H_2O$  (water), OM (organic matter),  $CO_2$  (Carbon dioxide),  $NH_4^*$ (ammonium in jarosite),  $SO_4^{2-}$  (sulphate in jarosite) and Qz (quartz).

#### 3.2.2. SEM/EDX analysis

SEM images of uninoculated samples for all tests (Fig. 5) showed surfaces with few alterations such as isolated cracks. These alterations were interpreted as mineral genetic defects. The grains had well-defined edges. EDX analysis of the grains showed the chalcopyrite's stoichiometric composition (Fig. 6). The morphology of the grains exposed to bacteria is illustrated in Figs. 7. All the samples show typical corrosion features such as pits, grooves, and gulfs on the surfaces of the chalcopyrite grains (Figs. 7) that increased from the edge of the grain toward the core. These characteristics were observable the first day of the process and became more evident with time. EDX also characterized an aggregate containing S, O, and Fe (Fig.6). Average pit size and pitting density on the surface increased with reaction time. After 15 days, the surface pitting was extensive, resulting in discrete euhedral and elongated pits and grooves (Fig. 7). The formation of jarosite aggregates increased with time and sharply increased until the end of the process. Moreover, some grains showed a partial jarosite film covering the chalcopyrite grains since the first day of the process (Fig. 7)



Figure 5. Scanning electron microscopy micrographs of uninoculated residues after chalcopyrite bioleaching. Cpy, chalcopyrite; Qz, quartz. After 30 days.



Element	Weight%	Atomic%			
ок	31.99	57.25	Element	Weight%	Atomic%
SiK	2.20	2.25	SK	32,6	47.5
SK	15.98	14.27	FeK	31,19	26,05
КК	3.10	2.27	CuK	36,35	26.60
FeK	46.73	23.96	A. 04060214018		and a contraction

**Figure 6.** Scanning electron microscopy/energy dispersive X-ray spectroscopy micrograph and analysis of the residues after bioleaching with *A. ferrooxidans* of chalcopyrite. Cpy, chalcopyrite; J, jarosite.



**Figure 7.** Scanning electron microscopy micrographs of the residues after chalcopyrite bioleaching with *A. ferrooxidans*. Cpy, chalcopyrite; J, jarosite; and Qz, quartz. a) day 5, b) day 15 and c) day 30.

#### 3.2.3. XRD measurements

According to the XRD initial qualitative analysis, were founding that the primary mineral phase present in the samples was chalcopyrite with small quantities of quartz, molybdenite, covellite, chlorite and wollastonite (Fig. 8). From the result obtained by XRD spectra of bioleached samples (Fig. 9), the most important identified minerals were:

- i. as the principal products of the bacterial oxidation process: (a) ammonium jarosite, as preponderant phase and covellite in minor quantities and (b) Wollastonite was dissolved at the beginning of the process.
- **ii.** as mineral phases resistant to the bioxidation process: (a) Chalcopyrite, as the primary sulfide, present in every sample, (b) Minor quantities of pyrite and (c) different types of silicates like quartz, chlorite and muscovite.

Otherwise, mineralogical evolution of the mineral phases consists of a gradual reduction of molybdenite and chalcopyrite peaks and the appearance of ammonium jarosite and covellite. XRD for uninoculated controls did not show change in the time (Fig. 10).



**Figure 8.** X-ray diffraction spectra for chalcopyrite of sample before the bioleaching process (CPy, chalcopyrite; Qz, quartz; Mo, molybdenite; W, wollastonite; Cl, chlorite; CuS, covellite.


**Figure 9.** X-ray diffraction spectra of chalcopyrite during the bioleaching process in the 5, 15 and 30 days. (CPy, chalcopyrite; Qz, quartz; Mo, molybdenite; W, wollastonite; Cl, chlorite; J, jarosite; Cv, covellite).



Figure 10. X-ray diffractograms of uninoculated samples after 30 days of the process. (CPy, chalcopyrite; Qz, quartz; Mo, molybdenite; Cl, chlorite; CuS, covellite).

#### 4. Discussion

#### 4.1. Chalcopyrite leaching experiment

As previously stated, it is possible to conclude that the chalcopyrite bioleaching process was passivated. The results suggest that a low level of Fe<sup>3+</sup> is favorable for Cu lixiviation since the copper release slowed at high Fe<sup>3+</sup> concentration. Chemical analysis showed that around the 15<sup>th</sup> day, the system had a flat ferrous ion concentration, high ferric ion concentration, increased redox potential, and decreased copper dissolution. Hiroyoshi *et al.* (2001) [10] found that when the concentration of ferrous and cupric ions is low in the system, the overall reaction of chalcopyrite leaching is controlled by ferric ions and the copper extraction rate is slower. This could explain what happened after at 15 days the release of copper occurs more slowly. Furthermore, ferrous ions promoted chalcopyrite bioleaching below the "critical" potential, in this case around of 430 mV, which caused enhanced copper removal on days 1–15. In the higher potential area (days 16–30), the release of copper was smaller than that in the lower-potential region because there might not have been enough ferrous ion to promote chalcopyrite bioleaching. The present findings agree with those of previous works [3,4, 10, 34, 35]. The hypotheses in these works were that the chalcopyrite dissolution was catalyzed by the ferrous ion according to the following reactions (1-3):

$$CuFeS_2 + 4H^+ + O_2 \rightarrow Cu^{2+} + 2S^0 + Fe^{2+} + 2H_2O$$
 (1)

$$CuFeS_2 + 3Cu^{2+} + 3Fe^{2+} \rightarrow 2Cu_2S + 4Fe^{3+}$$
 (2)

$$2Cu_{2}S + 8Fe^{3+} \rightarrow 4Cu^{2+} + 8Fe^{2+} + 2S^{0}$$
(3)

These researchers found that the inhibition of chalcopyrite bioleaching by mesophilic microorganisms is due to bacterial consumption of ferrous ion. In these reactions, the role of microorganisms such as *A. ferrooxidans* was not evident, and the copper dissolution was a purely chemical process. However, in the present study, we observed that *A. ferrooxidans* plays a fundamental role in the copper dissolution, as can be seen in the chemical controls where dissolution practically fails to occur.

Nevertheless, some researchers have found that copper release is favored at high Fe<sup>3+</sup> concentrations, where this ion contributes to the overall efficiency of the chalcopyrite leaching in which ferric ions acts as oxidizers, producing elemental sulfur according to the following reaction (4) [11, 16, 3-39].

$$CuFeS_2 + 4Fe^{3+} \rightarrow 5Fe^{2+} + Cu^{2+} + 2S^{\circ}$$
 (4)

#### 4.2. Mineralogical analysis

From the results previously outlined, it is possible to conclude that the leaching process the silicates did not present detectable changes, demonstrating refractoriness to it. Jarosite is the most abundant mineral phase as product of the bacterial leaching of chalcopyrite. There is a predominance of the ammonic component in the jarosite. The generation of jarosite in bacterial systems has been already documented in the literature [21]. [40] Produced jarosite using *A. ferrooxidans* and demonstrated the preference in the incorporation of K<sup>+</sup> and NH<sub>4</sub><sup>+</sup> in the jarosite in this system. Ammonium in the jarosite was incorporated probably from compounds used as nutrients in these processes.

Jarosite phase could be considered as the unfavorable phase because its presence apparently would passivate the copper release [5, 10, 11, 16, 34-38]. The jarosite formation was more marked from  $15^{\text{th}}$  day onward, when the system showed a lower concentration of ferrous ion, a higher concentration of ferric ion, increased redox potential, and a high concentration of SO<sub>4</sub><sup>2-</sup> in the solution. Jarosite formation was favored when redox potentials increased above the critical value (430 mV) around the  $15^{\text{th}}$  day, favoring the hydrolysis of ferric ion, promoting jarosite precipitation, and possibly generating chalcopyrite passivation [5]. The formation of jarosite was confirmed by FTIR spectra, which showed permanent increases in the typical bands.

The sharp increase of jarosite bands on the 15<sup>th</sup> day and its further slow increase was consistent with the observed chemical data. It is important to note the jarosite bands more defined with the time. It could involve a crystallinity increase in the jarosite structure. On the other hand, the increase of the band at 2935 cm<sup>-1</sup> was possibly due to an increase in bacterial population, indicating bacterial activity, which cannot detected by other characterization techniques [33]. Moreover, the NH<sub>4</sub> bands increased and were clearer with the time. It could indicate the NH<sub>4</sub> was gradually incorporating into the jarosite structure. Ammonium in the jarosite incorporated probably from compounds of ammonium, which are used as nutrients in this process, since it is the case of the ammonium sulfate added in T&K as source of energy [21]. In this way, if the microorganism did not have a NH<sub>4</sub> as source of energy they could decrease its activity.

Furthermore, SEM analysis showed that chalcopyrite dissolution, in the presence of these microorganisms, occurred on the surface due to the presence of roughening of the grains and the formation of dissolution pits, both of which increase with time. The pH reigning in the test and the high levels of  $Fe^{3+}$  and  $SO_4^{2-}$  could generate system instability, favoring the precipitation and nucleation of jarosite agglomerating on small chalcopyrite particles, increasing after the  $10^{th}$  day and forming a non-uniform film on the largest chalcopyrite grains. Jarosite precipitation, which could be mitigated by reduced levels of sulfates in the medium [1, 5, 30, 34]

On the other hand, XRD analysis (Figs. 9) indicated that jarosite formed at the expense of chalcopyrite dissolution. Moreover, XRD spectrum showed a covellita formation at the expense of chalcopyrite dissolution. In contrast, the chalcopyrite in the control reaction system remained visually unaltered. Nevertheless, the dissolution of minority phases as molybdenite,

wollastonite, and chlorite was observed. This mineralogical analysis showed the predominance of the galvanic effect, where lower-potential molybdenite dissolves in contact with chalcopyrite [41, 42].

Moreover, chlorite and wollastonite are soluble in acidic environments [5], and small quantities of the Cl<sup>-</sup> ion are not toxic to the bacterial population [43]. The increased relative abundance in the process could indicate a reduced ratio of chalcopyrite to covellite and, therefore, confirms the hypotheses raised by Hiroyoshi *et al.* [44-48], where the ferrous ions promoted chalcopyrite leaching, favoring the reduction of chalcopyrite to covellite and the simultaneously oxidation of this mineral. However, in this case, the ferrous ions apparently induced the reduction of chalcopyrite to covellite and the simultaneous oxidation. The hypothesis of this work was that the chalcopyrite dissolution was initially catalyzed by the ferrous ion according to the following reactions (5-7):

$$CuFeS_2 + 4H^+ + O_2 \rightarrow Cu^{2+} + 2S^0 + Fe^{2+} + 2H_2O$$
 (5)

$$CuFeS_2 + Cu^{2+} + Fe^{2+} \rightarrow 2CuS + 2Fe^{3+}$$
(6)

$$CuS + Fe^{3+} \rightarrow Cu^{2+} + Fe^{2+} + S^0$$
 (7)

Finally, it was possible to define the mechanisms from bacterial leaching of chalcopyrite is according figure 11:



Figure 11. Chalcopyrite bioleaching mechanism.

## 5. Conclusions

The characterization the mineral phases generated in the bioleaching process of chalcopyrite for *A. ferrooxidans* allowed understanding the transformation of these phases in the process chalcopyrite passivation. We showed that chalcopyrite bioleaching is not a typical bioprocess because faster and greater extractions resulted when the leaching was performed at low redox potential values. In this case, the ferrous ions apparently favored the reduction of chalcopyrite to CuS and the simultaneous oxidation of this newly formed phase, increasing the release of copper. A high concentration of Fe<sup>3+</sup> produces chemical instability in the process, favoring the precipitation of the jarosite principal phase formed in the processes. This phenomenon could be responsible for inhibiting chalcopyrite bioleaching. The results suggest that the mineral dissolution rate was affected by jarosite formation. This mineral may limit the diffusion of ions through the chalcopyrite surface and the access of the leaching solution. The bacteria A. ferrooxidans play an important role in the chalcopyrite bioleaching.

## Acknowledgements

The authors would like to thank the San Buenaventura University, Program of Biotechnology of Colciencias, Colombia, Laboratory of Biomineralogy of the National University of Colombia, the Laboratory of Mineralurgy, University of Antioquia, and the Laboratory of Coal, National University of Colombia, University Pascual Bravo institution by the economic support in the mineralogical characterization of samples.

# Author details

E.R. Mejía<sup>1,3\*</sup>, J.D. Ospina<sup>2</sup>, L. Osorno<sup>3</sup>, M.A. Márquez<sup>3</sup> and A.L. Morales<sup>4</sup>

\*Address all correspondence to: erika.mejia@usbmed.edu.co

1 Universidad San Buenaventura, sede Medellín, Facultad de artes integradas, Grupo de Investigación Hombre, Proyecto y Ciudad, Colombia

2 Institución Universitaria Pascual, Facultad de Ingeniería. Grupo de Investigación e Innovación Ambiental, Colombia

3 Universidad Nacional de Colombia, Medellín, Facultad de Ciencias y Facultad de Minas. Grupos de Investigación en Microbiología del Suelo y Mineralogía Aplicada y Bioprocesos, Colombia

4 Grupo de Estado Sólido, Instituto de Física, Universidad de Antioquia, Medellín, Colombia

#### References

- [1] Dutrizac, J.E. 1981. The dissolution of chalcopyrite in ferric sulfate and ferric chloride media. Met. Trans. B. 12B: 371-378.
- [2] Rivadeneira, J. 2006. Introduction. Mining innovation in Latin America Report. Publication via on-line (http://www.mininginnovation.cl/content.htm). Santiago, Chile, pp. 6–7.
- [3] Córdoba, E.M., Muñoz, J.A., Blázquez, M.L., González, F., Ballester A. 2008a. Leaching of chalcopyrite with ferric ion. Part I: General aspects Hydrometallurgy. 93 81.
- [4] Córdoba, E.M., Muñoz, J.A., Blázquez, M.L., González, F., Ballester A. 2008b. Leaching of chalcopyrite with ferric ion. Part IV: The role of redoxpotential in the presence of mesophilic and thermophilic bacteria. Hydrometallurgy. 93 88.
- [5] Marsden, J., House, I. 1992. The Chemistry of Gold Extraction. Ellis Horwood, New York, 579.
- [6] Brierley, J.A., Luinstra, L. Biooxidation-heap concept for pretreatment of refractory gold ore. In: Biohydrometallurgical Technologies, A.E. Torma, J.E. Wey & V.L. Lakshmanan Eds., The Minerals, Metals & Materials Society, pp. 437-448. 1993.
- [7] Hsu, C.H., Roger, G.H. 1995. Bacterial leaching of zinc and copper from mining wastes. Hydrometallurgy. 37 169-179
- [8] Watling, H.R. 2006. The bioleaching of sulphide minerals with emphasis on copper sulphides—a review. Hydrometallurgy. 84 81–108.
- [9] Al-Harahsheh, M., Kingman, S., Rutten, F., Briggs, D. 2006. ToF-SIMS and SEM study on the preferential oxidation of chalcopyrite. International Journal of Mineral Processing. 80 2-4.
- [10] Hiroyoshi, N., Miki, H., Hirajima, T., Tsunekawa, M. 2000. A model for ferrous-promoted chalcopyrite leaching. Hydrometallurgy. 57 31– 38.
- [11] Yin, Q., Kelsall, G.H., Vaughan, D.J., England, K.E.R. 1995. Atmospheric and electrochemical oxidation of the surface of chalcopyrite (CuFeS2). Geochimica et Cosmochimica Acta. 59 1091-1100.
- [12] Hackl, R.P. Dreisinger, D.B. Peters, E. King J.A. 1995. Passivation of chalcopyrite during oxidative leaching in sulfate media. Hydrometallurgy. 39 1-3,25-48.
- [13] Schippers A., Sand W. 1999. Bacterial leaching of metal sulfides proceeds by two indirect mechanisms via thiosulfate or via polysulfides and sulfur. Applied Environmental Microbiology. 65 1, 319-321.

- [14] Mikhlin, Y.L., Tomashevich, Y.V., Asanov, I.P., Okotrub, A.V., Varnek, V.A., Vyalikh, D.V. 2004. Spectroscopic and electrochemical characterization of the surface layers of chalcopyrite reacted in acidic solutions, Applied Surface Science 225 395–409.
- [15] Bevilaqua, D., Leite, A.L.L.C., Garcia Jr., O., Tuovinen, O.H. 2002. Oxidation of chalcopyrite by *Acidithiobacillus ferrooxidans* and *Acidithiobacillus thiooxidans* in shake flasks. Process Biochemistry. 38, 587-592.
- [16] Harmer, S.L., Thomas, J.E., Fornasiero, D., Gerson, A.R. 2006. The evolution of surface layers formed during chalcopyrite leaching. Geochimica et Cosmochimica Acta 70 4392–4402.
- [17] Klauber, C. 2008. A critical review of the surface chemistry of acidic ferric sulphate dissolution of chalcopyrite with regards to hindered dissolution. Int. J. Miner. Process. 86 1–17.
- [18] Harvey, P.I., Crundwell, F.K. 1996. The effect of As(III) on the growth of *Thiobacillus ferrooxidans* in an electrolytic cell under controlled redox potentials. Minerals Engineering. 9 10 1059-1068.
- [19] Petruk, W. 2000. Applied mineralogy in the mining industry. Elsevier. Ottawa, Ontario, Canada.
- [20] Márquez, M.A., Gaspar, J.C., Bessler, K.E., Magela G. 2006. Process mineralogy of bacterial oxidized gold ore in São Bento Mine (Brasil). Hydrometallurgy. 83 1-4 114-123.
- [21] E. Mejía, J. D. Ospina, M. A. Márquez and A. L. Morales (2012). Bioleaching of Galena (PbS), Fourier Transform-Materials Analysis, Dr Salih Salih (Ed.), ISBN: 978-953-51-0594-7, InTech, Available from: http://www.intechopen.com/books/fourier-transform-materials-analysis/bioleaching-of-galena-pbs-
- [22] Márquez, M.A., Ospina, J.D.; Mejía, E; Osorno, B.L.; Morales, A.L. (2013) Estudio µraman de la oxidación superficial de la pirita (Fes2), Calcopirita (CuFeS2) por *Acidithiobacillus ferrooxidans*. Rev. ACCEFYN. ISSN: 0370-390, Vol 14. Pp. 373-380.
- [23] Tuovinen O., Kelly D. 1973. Studies on the growth of *Thiobacillus ferrooxidans*. Arch. Microbiol. 88: p 285–298.
- [24] Fowler T.A., Holmes P.R., Crundwell F.K. 1999. Mechanism of pyrite dissolution in the presence of *Thiobacillus ferrooxidans*. Applied And Environmental Microbiology. 65: p 2987–2993.
- [25] Lenore, S., Clesceri, A. E., Greenberg Eaton, A.D. 1999. Standard Methods for the Examination of Water and Wastewater. American Public Health Association, American Water Works Association, Water Environment Federation. 20Th edition.
- [26] Chernyshova, I.V. 2003.An in situ FTIR of galena and pyrite oxidation in aqueous solution. 558. 83-98.Da Silva, G., Lastra, M. R., Budden, J. R. 2003. Electrochemical

passivation of sphalerite during bacterial oxidation in the presence of galena. Minerals Engineering. 16 199 – 203.

- [27] Gunneriusson, L., Åke Sandström, Holmgren, A., Kuzmann, E., Kovacs, K., Vértes, A. 2009. Jarosite inclusion of fluoride and its potential significance to bioleaching of sulphide minerals Hydrometallurgy. 96 108-116.
- [28] Márquez, M.A.G. 1999. Mineralogia dos processos de oxidacao sobre pressao e bacteriana do minerio de ouro da mina Sao Bento, MG. Tese de doutorado. Universidad de Brasilia.
- [29] Xuguang, S. 2005. The investigation of chemical structure of coal macerals via transmitted-light FT-IR microspectroscopy. Spectrochimica Acta Part A: Molecular and Biomolecular Spectroscopy. 62 557.
- [30] Naumann, D., Helm, D. 1995. FEMS Microbiology Letters. 126 75
- [31] Parker, A., Klauber, C., Kougianos, A., Waltling, H.R., Van Bronswijk, W. 2003. An xray photoelectron spectroscopy study of the mechanism of chalcopyrite leaching. Hydrometallurgy. 71(1–2), 265–276.
- [32] Sharma, P.K., Hanumantha, R. K. 2005. Miner. Metal. Process. 22 31
- [33] Xia L., Liu J., Xiao L., Zeng J., Li B., Geng M. and Qiu G. 2008. Single and cooperative bioleaching of sphalerite by two kinds of bacteria—*Acidithiobacillus ferriooxidans* and *Acidithiobacillus thiooxidans*. Trans. Nonferrous Met. Soc. China. 12 190
- [34] Sandström, Å., Shchukarev, A., Jan Paul. 2005. XPS characterisation of chalcopyrite chemically and bio-leached at high and low redox potential. Minerals Engineering. 18 505–515.
- [35] Mejía, E.R., Ospina, J.D., Márquez M.A., Morales, A.L. 2009. Oxidation of chalcopyrite (CuFeS2) by Acidithiobacillus ferrooxidansand a mixed culture of *Acidithiobacillus ferrooxidans andAcidithiobacillus thiooxidans* like bacterium in shake flasksAdvanced Materials Research. 71-73. 385-388.
- [36] Schippers, A. 2007. Microorganisms involved in bioleaching and nucleic acid-based molecular methods for their identification and quantification. Microbial Processing of Metal Sílfides. Chapter one. Eddited by Edgardo R. Donati & Wolfgang Sand. Springer.
- [37] Shrihari, R.K., Gandhi, K.S., Natarajan, K.A. 1991. Role of cell attachment in leaching of chalcopyrite mineral by Thiobacillus ferrooxidans. Applied Microbiology and Biotechnology. 36 278-282.
- [38] A. Akcil, H. Ciftci, H. Deveci. 2007. Mineral Engineering. 20 310
- [39] Cardona I.C. 2008. Mineralogía del proceso de biodesulfurización de carbones provenientes de la zona río Aguachinte – río Asnazú (valle del cauca y cauca). Tesis de Maestría. Universidad Nacional de Colombia, sede Medellín.

- [40] Ivarson, K.C., Ross, G.J., Miles, N.M. 1979. The microbiological formation of basic ferric sulfates: II. Crystallization in presence of potassium, ammonium, and sodiumsalts. Soil Science Society of America Journal, 43 (1979), 908–912.
- [41] Jiang, T., Li, Q., Yang Y., Li, G., Qiu, G. 2008. Bio-oxidation of arsenopyrite. Trans. Nonferrous Met. Soc. China. 18. 1433–1438.
- [42] Urbano, G., Meléndez, A.M., Reyes, V.E., Veloz, M.A., Gonzáles, I. 2007. Galvanic interactions between galena – sphalerite and their reactivity. International Journal of Mineral Processing. 82 148 – 155.
- [43] Gahana, C.S., Sundkvista, J.; Sandströma, Åke. 2009. A study on the toxic effects of chloride on the biooxidation efficiency of pyrite. Journal of Hazardous Materials. 172 1273–1281.
- [44] Hiroyoshi N., Hirota M., Hirajima T., Tsunekawa M. 1997. A case of ferrous sulfate addition enhancing chalcopyrite leaching. Hydrometallurgy. 47 37-45.
- [45] Hiroyoshi, N., Arai, M., Miki, H., Tsunekawa, M., Hirajima, T. 2002. A new reaction model for the catalytic effect of silver ions on chalcopyrite leaching in sulfuric acid solution. Hydrometallurgy. 63 257-267
- [46] Hiroyoshi, N., Kitagawa, H., Tsunekawa, M. 2008. Effect of solution composition on the optimum redox potential for chalcopyrite leaching in sulfuric acid solution. Hydrometallurgy. 91 144-149.
- [47] Hiroyoshi, N., Miki, H., Hirajima, T., Hirajima, T., Tsunekawa, M. 2001. Enhancement of chalcopyrite leaching by ferrous ion in acid ferric sulfate solution. Hydrometallurgy. 60 185-197
- [48] Shrihari, J.J.M., Kumar, R., Gandhi, K.S. 1995. Dissolution of particles of pyrite mineral by direct attachment of Thiobacillus ferrooxidans. Hydrometallurgy. 38(2) 175-187.



# Edited by Salih Mohammed Salih

The application of Fourier transform (FT) in signal processing and physical sciences has increased in the past decades. Almost all the textbooks on signal processing or physics have a section devoted to the FT theory. For this reason, this book focuses on signal processing and physical sciences. The book chapters are related to fast hybrid recursive FT based on Jacket matrix, acquisition algorithm for global navigation satellite system, determining the sensitivity of output parameters based on FFT, convergence of integrals of products based on Riemann-Lebesgue Lemma function, extending the real and complex number fields for treating the FT, nonmaterial structure, Gabor transform, and chalcopyrite bioleaching. The book provides applications oriented to signal processing and physics written primarily for engineers, mathematicians, physicians and graduate students, will also find it useful as a reference for their research activities.

Photo by DrHitch / DollarPhotoClub

IntechOpen



